Residential Development – Apartment Building 801 Sarnia Road City of London, Ontario Stormwater Management Addendum November 2021 Revised October 2024

> **Prepared for:** Western Prestige Village 801 Sarnia Road London, Ontario



Prepared by: Eng Plus Ltd. 100-609 William Street London, ON N6N 3G1

1.0 INTRODUCTION

This Stormwater Management Addendum is to support the proposed 10 storey apartment building at 801 Sarnia Road. The proposed building has changed from the approved site plan (5-storey, 69 units) to a 10-storey building with 182 units.

This is the addendum to the approved "Stormwater Management Plan – Residential Development, 801 Sarnia Road, and Revised May 31th, 2016" by Eng Plus Ltd.

The purposes of the addendum is to provide additional design, calculations, to address the City comments dated July 26, 2021, and to address changes in the design of the site plan due to additional lands acquired.

2.0 STORMWATER MANAGEMENT

2.1 Background, Approved plan

The proposed apartment building development is part of an approved site plan number SP15-036107, comprised of medium density residential townhouses to be registered as Vacant Land Condominiums on the west portion of the subject lands and an apartment building on the east portion of the subject lands, identified as Block A (west) and Block B (east), Block A is approximately 1.65 ha. and Block B is approximately 0.94ha. as shown in Figure 1 below:

Figure 1: Site Plan illustrates the proposed development at 801 Sarnia Road, Approved Plan SP15-036107



Block A, condominium townhouse block, consists of 9 building blocks totaling 57 townhouse units had been fully developed as per the approved site plan SP15-036107.

As per the approved "Stormwater Management Plan – Residential Development, 801 Sarnia Road, Revised May 31th, 2016", the stormwater runoff of Block B, apartment building block, is divided into two post development catchment areas (B1 = 0.5 ha. and B2 = 0.16 ha.), and outlet to two separate outlets in the post-development conditions.



Low impact development, bio retention system, were proposed to address water quality and quantity for the site.

2.2 Proposed Development for Apartment Building Block

The client had acquired some additional land east of the site (approximately 0.16 ha.) and included in the development of Block B. The additional land has enable the client to have more density for the development, especially, increase the proposed apartment building to 10-storey building with total of 182 units. The site plan for Block B has changed slightly to accommodate more parking spaces for the proposal. The new proposed site plan for Block B is shown in Figure 2 below:

Figure 2: Site Plan illustrates the proposed development at 801 Sarnia Road, Apartment Building



The post-development drainage areas for Block B is attached in the appendix. The proposed new site plan lay-out has removed the bioretention/storage areas for post-development stormwater management control. Below are the new proposed stormwater management plan for the development:

2.2.1 Building Area B1a, 0.206 hectares, C=0.9

Roof top storage is proposed to control post-development flows to pre-development conditions. As per calculation attached, pre-development flows for the area B1a, 0.206 hectares, are 9.2 l/s and 21.4 l/s for 2-year and 100-year storm respectively. It is proposed to control rooftop flow to 2-year pre-development flow of 9.2 l/s. The required storage are 22 cu.m and 80.0 cu.m for 2-year and 100-year post-development conditions respectively.



The available roof top storage is approximately 82 m³ (= $(2062 \text{ m}^2 \text{ x } 0.15 \text{ m}) / 3 \text{ x } 80\%)$), at maximum 0.15m depth and 80% volume.

Therefore, there is enough capacity on the roof top to attenuate the post-development flow rates to 2-year pre-development flow rate of 9.2 l/s for all storm events up to 100-year storm. During a 250-year storm event extra stormwater over the storage requirement will overflow the rooftop.

Flow control roof drain to be specified by building mechanical engineer for the restricted flow of 9.2 l/s.

Runoff water from roof top areas are considered clean, quality treatment is not required.

2.2.2 Block B, Areas B2 (0.310 Ha.) & B3 (0.131 Ha.), C=0.8

The area B2 and B3 are the surface and parking areas, approximately 0.441 hectares at runoff coefficient of C=0.8. On-site storage is required to control peak post development discharge rates to pre-development discharge rates for the 2-year to 250-year storm events and are provided in table below:

Storm Frequency	Pre-Development Discharge (Q _{peak_pre})	Post-Development Discharge (Q _{peak_post})	Required Storage Volume (m ³)
2 year	0.020 m ³ /s	0.064 m ³ /s	40.0 m^3
100 year	0.046 m ³ /s	0.147 m ³ /s	95.5 m ³
250 year	0.054 m ³ /s	0.171 m ³ /s	110.4 m ³

To provide the required storage volume above for areas B2 & B3 in the post-development conditions, an underground storage system is proposed. Stormwater runoff is directed to the underground storage system though the catchbasins and underground sewer system.

The underground storage system is proposed to have storage volume for quantity control of 2-year design storm, or 40 cubic meters so that there will not be any surface ponding during 2-year storm events. The StormTech system attached (or approved equal) can provide 30 cu.m of storage underground, and another 10 cu.m is provided in the ~140m-300mm diameter underground sewers system.

During major storm events, excess stormwater runoff will temporary pond on top of the catchbasins in the parking areas up to the depth of 0.25m for quantity storage until capacity in the sewer system available.

Our grading plan provide approximate 125 cu.m up to the depth of 0.3m on top of the catchbasins. Total storage volume provided is 165 cu.m (= 40 + 125), meets the required storage of 110 cu.m for 250-year storm event.



Contour Elevation (m)	Contour Area (sq. m)	Depth (m)	Incremental Volume Avg. End (cu. m)	Cumulative Volume Avg. End (cu. m)
283.40		0.00	0	0
283.45	28	0.05	1	1
283.50	113	0.10	6	7
283.55	254	0.15	13	20
283.60	451	0.20	20	40
283.65	697	0.25	35	75
283.70	993	0.30	50	125

The stage/storage as per the following table:

STAGE-STORAGE VOLUME FOR AREAS B2 & B3

100-Year storage 250-Year storage

An overflow route is provide at the north boundary to safely direct overland flow for up to 250-year storm events.

An orifice of 100mm diameter is proposed at the outlet pipe to control the maximum flow from the site to 23 l/s.

For quality control, an oil/grit separator ADS model FD-4HC (or approved equal) is proposed at the outlet, before the underground storage tank. The proposed OGS is capable of remove up to 94% TSS of runoff water, archiving MOE Enhanced Protection level of 80% TSS removal. Detail calculation is attached.

2.2.1 Block B: Area B4, 0.018 hectares, C=0.25

The additional area acquired is located east of the site with the area of 0.16 hectares. The majority of this area is dedicated to the City as road widening and park land for the multi trail along the north of the site. The remainder area of approximately 0.018 hectares is added to the site development as landscape area.

Based on the topography, this area is gently draining to the north and east toward the existing railway land. We are proposing to maintain the existing drainage patterns for this area. Grading for this area is generally direct to the north match existing ground elevations. This new area will be grass/ landscape. Post development runoff coefficient for this area B3 is unchanged (C=0.25).

Since the pre- and post- development runoff coefficients are the same and approximately 1/3 of the land (road widening dedication) will be regraded to direct the drainage to the road allowance per City's standards, the stormwater runoff draining to the north will be less in the post-development conditions.

Therefore quantity control and quality control for post-development are not required.



3.0 CONCLUSIONS

This addendum is provided to address the proposed changes in the approved site plan plan number SP15-036107 due to additional land acquired east of the site. This is to supplement to the approved "Stormwater Management Plan – Residential Development, 801 Sarnia Road, Revised May 31th, 2016" by this office.

New oil/grit separator and underground storage system, together with roof top storage are proposed to address quality and quantity post-development conditions for drainage areas B1-B3. Additional landscape area B4 is graded following the existing drainage pattern of the site and match into existing ground along the boundary.

We trust the information presented in this addendum address your concerns on stormwater management and meets your current requirements. Please do not hesitate to contact us should you have any questions or concerns.

All of which is respectfully submitted,



Vinh Pham, P.Eng.

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APPENDIX A

CALCULATIONS - ATTACHMENTS



DATA SHEET BLOCK B1 Areas - A = 0.206 Ha. Pre-development Flow Calculation

2-Year Pre-development Flow

- Q= 2.78CIA C= 0.25 Pre-development Run-off Coefficient |= 64.03 mm/h Rainfall intensity, Time to Peak = 15 minutes A= 0.206 ha Proposed Building area 9.2 l/sec Q = **100-Year Pre-development Flow** Q= 2.78CIA 149.56 mm/h |= Rainfall intensity, Time to Peak = 15 minutes **Q** = 21.4 l/sec **250-Year Pre-development Flow** Q= 2.78CIA |= 174.67 mm/h Rainfall intensity, Time to Peak = 15 minutes
 - Q = 25.0 l/sec

DATA SHEET

BLOCK B1 - Building Area, A = 0.206Ha. STORAGE REQUIREMENT

Design C	riteria:				
•		Lot Are	a A=	0.206	ha
	Post	t-Developmen	t C=	0.90	
		Flow	· 0=	2 78CIA	m ³
		1100	v Q -	2.7001/(
Storm	2 Year				
а	754.36		Q _{pre_2} =	9.2	l/s
b	6.01				
С	0.81				
Duration	Intensity	Peak Runoff	Storm runoff	Release Flow	Req'd Storage
(minute)	mm/hr	m³/s	m³	m³	m³
5	108.1	0.056	16.71	2.75	13.96
10	79.8	0.041	24.68	5.50	19.18
15	64.0	0.033	29.70	8.25	21.45
20	53.9	0.028	33.31	11.00	22.31
25	46.7	0.024	36.12	13.75	22.36
30	41.4	0.021	38.40	16.50	21.90
Storm	100 Year				
а	2619.36		$Q_{pre_2} =$	9.2	l/s
b	10.50				
С	0.88				
Duration	Intensity	Peak Runoff	Storm runoff	Release Flow	Req'd Storage
(minute)	mm/hr	m³/s	m³	m³	m³
5	232.2	0.120	35.91	2.75	33.16
10	181.4	0.093	56.09	5.50	50.59
15	149.6	0.077	69.38	8.25	61.13
30	99.4	0.051	92.18	16.50	75.68
40	81.7	0.042	101.12	22.00	79.12
50	69.7	0.036	107.75	27.50	80.24
55	65.0	0.033	110.49	30.25	80.23
Storm	250 Year				
а	3048.22		Q _{pre_250} =	25.0	l/s
b	10.03				
С	0.89				
Duration	Intensity	Peak Runoff	Storm runoff	Release Flow	Req'd Storage
(minute)	mm/hr	m³/s	m³	m³	m³
5	274.7	0.142	42.48	7.50	34.98
10	212.9	0.110	65.84	15.00	50.83
15	174.7	0.090	81.02	22.51	58.52
30	115.1	0.059	106.80	45.01	61.78
40	94.4	0.049	116.81	60.02	56.80
50	80.3	0.041	124.20	75.02	49.18

DATA SHEET

Block B2 & Block B3 Parking Area - A = 0.310 + 0.131 Ha. **Pre-development Flow Calculation**

2-Year Pre-development Flow

Q= 2.78CIA		
C= I= A=	0.25 65.07 mm/h 0.441 ha	Pre-development Run-off Coefficient Rainfall intensity, Time to Peak = 15 minutes Drainage area
Q =	19.9 l/sec	
100-Year Pre	-development Flo	ow .
Q= 2.78CIA		
I=	149.56 mm/h	Rainfall intensity, Time to Peak = 15 minutes
Q =	45.8 l/sec	
250-Year Pre	-development Flo	ow .
Q= 2.78CIA		
I=	174.67 mm/h	Rainfall intensity, Time to Peak = 15 minutes

Q = 53.5 l/sec

DATA SHEET BLOCK B2 (0.310 Ha.) & BLOCK B3 (-.131Ha.) Parking Areas STORAGE REQUIREMENT

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Design Criteria:					
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45 75.2 0.074 199.15 123.77 75.36 Storm 250 Year Qpre_250 = 53.5 l/s b 10.03 C 0.89 C Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s m³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 30 35	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 0	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 92.91
Storm 250 Year a 3048.22 b 10.03 c 0.89 Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s m³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 40	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 422.77	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.29
Storm 250 Year a 3048.22 b 10.03 c 0.89 Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s m³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 40 40 45	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2	Peak Runoff m³/s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
a 3048.22 a 3048.22 a 30.3.3 //s b 10.03 c 0.89 c 30.3.3 //s c 30.3.3 //s c c 0.89 c c 0.89 c <thc< th=""> <thc< th=""> c <</thc<></thc<>	c Duration (minute) 5 15 25 30 35 40 45	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2	Peak Runoff m³/s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
b 10.03 c 0.89 Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s 0 M³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 30 35 40 45 Storm	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year	Peak Runoff m³/s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
c 0.89 Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s m³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 30 35 40 45 Storm	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22	Peak Runoff m³/s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} =	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
Duration Intensity Peak Runoff Storm runoff Release Flow Req'd Storage (minute) mm/hr m³/s m³ m³ m³ 5 274.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 40 45 Storm a b	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03	Peak Runoff m³/s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} =	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
(minute)mm/hrm /smmm5274.70.26980.8416.0664.7715174.70.171154.1848.18106.0025129.60.127190.6580.30110.3530115.10.113203.2296.36106.8635103.70.102213.56112.42101.144094.40.093222.29128.4893.80	c Duration (minute) 5 15 25 30 30 35 40 45 Storm a b c c	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} =	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38
5 2/4.7 0.269 80.84 16.06 64.77 15 174.7 0.171 154.18 48.18 106.00 25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 30 35 40 45 Storm a b c Duration	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} =	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s
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25 129.6 0.127 190.65 80.30 110.35 30 115.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 30 35 40 45 Storm Storm a b c Duration (minute) 5	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Qpre_250 = Storm runoff m ³ 80.84	Release Flow m³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m³ 16.06	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Req'd Storage m ³ 64.77
30 113.1 0.113 203.22 96.36 106.86 35 103.7 0.102 213.56 112.42 101.14 40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 40 45 Storm a b c Duration (minute) 5 15	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7 174.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Qpre_250 = Storm runoff m ³ 80.84 154.18	Release Flow m³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m³ 16.06 48.18 09.20	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Req'd Storage m ³ 64.77 1060.02
40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 30 35 40 45 Storm a b c Duration (minute) 5 15 25 20	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7 174.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171 0.127	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} = Storm runoff m ³ 80.84 154.18 190.65	Release Flow m³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m³ 16.06 48.18 80.00 06.26	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Req'd Storage m ³ 64.77 106.00 110.35
ער אין אייע איין איין איין דער אין דער א	c Duration (minute) 5 15 25 30 35 40 45 Storm a b c Duration (minute) 5 15 25 25 30 0	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7 174.7 129.6 115.1	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171 0.127 0.113 0.113	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} = Storm runoff m ³ 80.84 154.18 190.65 203.22	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m ³ 16.06 48.18 80.30 96.63	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s I/s Req'd Storage m ³ 64.77 106.00 110.35 106.86
45 86.8 0.085 229.79 144.54 85.25	c Duration (minute) 5 15 25 30 35 40 45 Storm a b c Duration (minute) 5 15 25 30 35 40	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7 174.7 129.6 115.1 103.7 94.4	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171 0.127 0.113 0.102 0.093	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Qpre_250 = Storm runoff m ³ 80.84 154.18 190.65 203.22 213.56 222.20	Release Flow m ³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m ³ 16.06 48.18 80.30 96.36 112.42 128.48	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Keq'd Storage m ³ 64.77 106.00 110.35 106.86 101.14 93.80
40 94.4 0.093 222.29 128.48 93.80	c Duration (minute) 5 15 25 30 35 40 45 Storm a b c Duration (minute) 5	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Qpre_250 = Storm runoff m ³ 80.84	Release Flow m³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m³ 16.06 48.18	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Req'd Storage m ³ 64.77 106.00
	c Duration (minute) 5 15 25 30 35 40 45 Storm a b c Duration (minute) 5 15 25 30 30 35	0.88 Intensity mm/hr 232.2 149.6 111.6 99.4 89.6 81.7 75.2 250 Year 3048.22 10.03 0.89 Intensity mm/hr 274.7 174.7 129.6 115.1 103.7	Peak Runoff m ³ /s 0.228 0.147 0.109 0.097 0.088 0.080 0.074 0.074 Peak Runoff m ³ /s 0.269 0.171 0.127 0.113 0.102	Storm runoff m ³ 68.33 132.02 164.23 175.41 184.63 192.43 199.15 Q _{pre_250} = Storm runoff m ³ 80.84 154.18 190.65 203.22 213.56	Release Flow m³ 13.75 41.26 68.76 82.51 96.26 110.01 123.77 53.5 Release Flow m³ 16.06 48.18 80.30 96.36 1122.42	Req'd Storage m ³ 54.58 90.76 95.47 92.90 88.37 82.41 75.38 I/s Req'd Storage m ³ 64.77 106.00 110.35 106.86 101.14

Orifice Calculation

BLOCK B1a and Block B1b

Orifice Size required - 2 year pre-development, = 7.7 l/s + 14.8 l/s = 22.5 l/s

Q=KA(2gh)^{1/2}

Q= K= A= h= g=	0.0225 0.6 ? 1.2 9.81	m ³ /sec m m/sec ²	Restricted Flow Coefficient Orifice Size Max. height from top of ponding to orifice Gravity
A=	0.007728428 A=3.14d ² /4	m ²	
d=	0.099222632	m	
or	99.22	mm	
say	100	mm	
A= Q= Q=	0.00785 KA(2gh) ^{1/2} <u>0.023</u>	0.022853937 m ³ /sec	m ³ /sec



ADS OGS Sizing Summary

Project Name:	801 Sarnia Road		
Consulting Engineer:	Eng Plus Ltd.		
Location:	London, Ontario		
Sizing Completed By:	Haider Nasrullah	Email:	haider.nasrullah@adspipe.com

Treatment Requirements				
Treatment Goal: Enhanced (MOE)				
Selected Parameters: 80% TSS 90% Volume				
Selected Unit: FD-4HC				

Summary of Results				
Model TSS Removal Volume 1				
FD-4HC	92.0%	>90%		
FD-5HC	95.0%	>90%		
FD-6HC	96.0%	>90%		
FD-8HC	98.0%	>90%		
FD-10HC	99.0%	>90%		

FD-4HC Specification				
Unit Diameter (A):	1,200 mm			
Inlet Pipe Diameter (B):	300 mm			
Outlet Pipe Diameter (C):	300 mm			
Height, T/G to Outlet Invert (D):	1320 mm			
Height, Outlet Invert to Sump (E):	1515 mm			
Sediment Storage Capacity (F):	0.78 m³			
Oil Storage Capacity (G):	723 L			
Recommended Sediment Depth for Maintenance:	440 mm			
Max. Pipe Diameter:	600 mm			
Peak Flow Capacity:	510 L/s			

Site Elevations:			
Rim Elevation:	283.40		
Inlet Pipe Elevation:	282.13, 282.13		
Outlet Pipe Elevation:	282.08		

Site DetailsSite Area:0.441 ha% Impervious:-Rational C:0.80Rainfall Station:London Intl Airport, ONParticle Size Distribution:FinePeak Flowrate:---



Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



Consulting Engineer: Eng Plus Ltd.

Location:

London, Ontario

Net Annual Removal Efficiency Summary: FD-4HC

Rainfall Intensity ⁽¹⁾	Fraction of Rainfall ⁽¹⁾	FD-4HC Removal Efficiency ⁽²⁾	Weighted Net-Annual Removal Efficiency
mm/hr	%	%	%
0.50	0.2%	100.0%	0.2%
1.00	13.7%	100.0%	13.7%
1.50	17.3%	100.0%	17.3%
2.00	13.5%	97.7%	13.2%
2.50	2.7%	95.7%	2.6%
3.00	2.3%	94.1%	2.1%
3.50	8.5%	92.7%	7.9%
4.00	4.7%	91.6%	4.3%
4.50	1.5%	90.6%	1.3%
5.00	5.2%	89.7%	4.7%
6.00	4.1%	88.2%	3.6%
7.00	4.4%	86.9%	3.9%
8.00	3.3%	85.9%	2.8%
9.00	2.4%	84.9%	2.0%
10.00	2.3%	84.1%	2.0%
20.00	9.2%	78.9%	7.2%
30.00	2.5%	75.9%	1.9%
40.00	1.1%	73.9%	0.8%
50.00	0.4%	72.4%	0.3%
100.00	0.6%	67.9%	0.4%
	92%		
	>90%		

Notes:

- (1) Rainfall Data: 1960:2002, HLY03, London AP, ONT, 6144475.
- (2) Based on third party verified data and appoximating the removal of a PSD similar to the STC Fine distribution
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.

PROJECT INFORMATION

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO.	



801 SARNIA ROAD LONDON, ON, CANADA

SC-310 STORMTECH CHAMBER SPECIFICATIONS

- 1 CHAMBERS SHALL BE STORMTECH SC-310.
- 2 CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE OR POLYETHYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184. "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES". AND MEET 3 THE REQUIREMENTS OF ASTM F2922 (POLETHYLENE) OR ASTM F2418 (POLYPROPYLENE), "STANDARD SPECIFICATION FOR CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE ELOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE 5 THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2").
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2922 SHALL BE GREATER THAN OR EQUAL TO 400 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD. THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2922 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. Q
- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE. DUE TO THE 10. ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS. TO MINIMIZE THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE 11. LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGEABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310 SYSTEM

- STORMTECH SC-310 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH SC-310 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE". 2
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. 3. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS 4
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- 6 MAINTAIN MINIMUM - 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.
- 7. 467. 5. 56. OR 57
- 8. THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH SC-310 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE". 1
- 2 THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE"
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-800-821-6710 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.





EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE; AASHTO M43 #3, 357, 4,

NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE



ACCEPTABLE FILL MATERIALS: STORMTECH SC-310 CHAMBER SYSTEMS

MATERIAL LOCATION		MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMF
	D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER.	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPA INSTA
с		INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN CC THE CHAM 6" (150 mr WELL GI PROC VEHICLE
	в	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE5	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	
	Α	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE5	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE C

PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".

2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.

3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.

4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION

5. WHERE RECYCLED CONCRETE AGGREGATE IS USED IN LAYERS 'A' OR 'B' THE MATERIAL SHOULD ALSO MEET THE ACCEPTABILITY CRITERIA OUTLINED IN TECHNICAL NOTE 6.20 "RECYCLED CONCRETE STRUCTURAL BACKFILL".



NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2922 (POLETHYLENE) OR ASTM F2418 (POLYPROPYLENE), "STANDARD SPECIFICATION FOR CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. SC-310 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS. REFERENCE STORMTECH DESIGN MANUAL FOR BEARING CAPACITY GUIDANCE.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 400 LBS/FT/%. THE ASC IS DEFINED IN SECTION
 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.





SC-310 ISOLATOR ROW PLUS DETAIL

NTS

INSPECTION & MAINTENANCE

STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- A. INSPECTION PORTS (IF PRESENT)
- A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
- A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
- i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- 1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

VOVEN GEOTEXTILE BETWEEN MABERS OUS FABRIC WITHOUT SEAMS	4640 TRUEMAN BLVD 801 SARNIA ROAD	StormTech® London, on, canada	Chamber System Date: 09/24/2024 DRAWN: HN	1-800-821-6710 WWW.STORMTECH.COM DATE DRW CHK DRW CHK DESCRIPTION PROJECT #: CHECKED: N/A THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADSISTORMTECH UNDER THE PROJECT'S ENGINEER OF RECORD FEOR) OR OTHER PROJECT REPRESENTATIVE. THIS DRAWING IS NOT INTENDED FOR USE IN BIDDING OR CONSTRUCTION WITHOUT FILE OR SOUND FOR CONSTRUCTION IF IS THE ULTMATE RESPONSIBILITY OF THE EOR TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL REVIEWT THE PRODUCT FOR DEALLS MEET ALL APPLICABLE
	4	s⊦ 1 C	DF	5



SHEET

5 OF 5





IZE (W X H X INSTALLED LENGTH)	34.0" X 16.0" X 85.4"	(864
HAMBER STORAGE	14.7 CUBIC FEET	(0.4
INIMUM INSTALLED STORAGE*	31.0 CUBIC FEET	(0.8
VEIGHT	35.0 lbs.	(16.

			<u> </u>
PART #	STUB	A	
SC310EPE06T / SC310EPE06TPC	6" (150 mm)	9.6" (244 mm)	
SC310EPE06B / SC310EPE06BPC	0 (130 mm)	3.0 (244 mm)	
SC310EPE08T / SC310EPE08TPC	8" (200 mm)	11.9" (302 mm)	
SC310EPE08B / SC310EPE08BPC	0 (200 mm)	11.9 (302 1111)	
SC310EPE10T / SC310EPE10TPC	10" (250 mm)	12 7" (222 mm)	
SC310EPE10B / SC310EPE10BPC	10 (230 11111)	12.1 (32311111)	
SC310ECEZ*	12" (300 mm)	13.5" (343 mm)	

* FOR THE SC310ECEZ THE 12" (300 mm) STUB LIES BELOW THE BOTTOM OF THE END CAP APPROXIMATELY 0.25" (6 mm). BACKFILL MATERIAL SHOULD BE REMOVED FROM BELOW THE N-12 STUB SO THAT THE FITTING SITS LEVEL.

NOTE: ALL DIMENSIONS ARE NOMINAL

ORIFICE TO BE INSTALLED AT THE OUTLET PIPE.

10/9/-/3/05/5/





