## Transportation Impact Assessment

## W3 Sunset Creek



AARCADIS Prepared for W3 Lambeth Farms Inc.
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## Executive Summary

Arcadis IBI Group was retained by W3 Lambeth Farms Inc. to prepare a Transportation Impact Assessment (TIA) in support of a Draft Plan of Subdivision application for a proposed residential subdivision located east of Colonel Talbot Road in London, Ontario, on lands municipally known as 3680, $3690 \& 3700$ Colonel Talbot Road.

The proposed subdivision will include a mix of low-density, medium-density and higher density residential land uses as well as some limited neighbourhood-oriented commercial land uses. Access to the proposed development will be provided via Royal Magnolia Avenue, which has been partially constructed as part of the W3 Farms Residential Development, as well as the future Colonel Talbot \& Street ' $N$ ' intersection which aligns with Clayton Walk. Future internal connections to the Hudson Park development to the north will also eventually provide access to Pack Road, however, this is not expected to occur within the timeframe of this study. The proposed development will be built in a single phase with full buildout anticipated for 2033 and therefore a horizon year of 2038 was assumed for this study.

It is estimated that the proposed development will generate 650 and 702 two-way person-trips during the weekday morning and weekday afternoon peak hours, respectively, of which 407 and 439 will be vehicle-trips. These vehicle-trips were distributed and assigned to the adjacent road network based on the City of London 2016 Household Travel Survey and engineering judgement.

An intersection capacity analysis was completed for all study area intersections under both background and total traffic conditions. The results of the analysis indicate that the Colonel Talbot Road corridor will experience capacity issues as a two-lane roadway due to background traffic demand. Mitigation measures were proposed to address these capacity issues but without any plans for future widening, significant congestion is expected by the horizon year of the study. Capacity issues are also anticipated at the Main/Wharncliffe \& Campbell intersection as a result of high background traffic demand. It is recommended that the City review the need for capital improvements with the broader area (i.e., road widenings) to ensure that sufficient capacity is provided to accommodate projected growth.

To address background capacity issues, the following mitigation measures are recommended to be implemented:

- Colonel Talbot \& Pack: Optimize the signal timing plan and add a protected-permitted westbound left-turn phase in the weekday morning and afternoon peak hour. When reconstructing the intersection during the urbanization of Colonel Talbot Road, it is also recommended that the westbound left-turn lane be extended to provide a minimum of 160 m of storage and that northbound and westbound right-turn lanes be provided. A minimum of 40 m and 75 m of storage is required for the northbound and westbound rightturn lane, respectively. Required in approximately 5 years.
- Colonel Talbot \& Clayton/Street 'N': Give consideration to implementing peak period eastbound and westbound left-turn prohibitions or restrict the side streets to right-in/rightout only. Given the high traffic volumes on the main street, left-turn movements from the sidestreets could be hazardous and would be subject to significant delays. Required in approximately 5 years.
- Colonel Talbot \& Diane/Royal Magnolia: The Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) suggests that the intersection will remain unsignalized when Colonel Talbot Road is urbanized in 2024-2025. Based on the results of this study, however, it is recommended that the intersection be signalized and that a minimum of 100 m of storage be provided for the southbound left-turn movement
rather than the 75 m recommended in the AECOM report. It is further recommended that a combined pedestrian/bicycle crossing facility be provided on the north side of this intersection to provide system connectivity for the planned multi-use path network. Required within 5 years and prior to first occupancy of the proposed development.
- Colonel Talbot \& Kilbourne: Optimize the signal timing plan on a regular basis.
- Main/Wharncliffe \& Campbell: Optimize the signal timing plan, add a protectedpermitted southbound and eastbound left-turn phase in the weekday morning and afternoon peak hour, respectively, and add a westbound right-turn lane with a minimum of 25 m of storage capacity. Required imminently.

In addition to the above mitigation measures, the addition of site-generated traffic also triggers the need for a protected-permitted southbound left-turn phase at the Colonel Talbot \& Diane/Royal Magnolia intersection within 5 years and prior to first occupancy of the proposed development, assuming it is signalized as recommended previously.

The proposed site access on Colonel Talbot Road (Street 'N') was reviewed for conformance with the City of London Access Management Guidelines and the results of the desktop review indicate that the proposed access will meet both sightline and access spacing requirements. Furthermore, this secondary site access connection is aligned with the existing Clayton Walk intersection.

The internal transportation network of the proposed development was also reviewed. The major internal intersection of Royal Magnolia \& Campbell is located adjacent to mixed-use residential/commercial blocks and is therefore expected to experience moderate volumes of vehicular and pedestrian demand. Based on a review of anticipated volumes, it is recommended that the intersection be configured as an all-way stop-controlled intersection. Intersection capacity analysis confirms that the intersection would operate at an acceptable Level of Service (i.e., LOS ' $D$ ') in this configuration.
The existing segment of Royal Magnolia Avenue (Colonel Talbot Road to Big Leaf Trail) does not include cycling facilities but cycling facilities may be included (by others) for the remaining segment east to Bostwick Road. The City has identified the need for bicycle infrastructure on both Campbell Street North and Street 'R'. Based on Ontario Traffic Manual (OTM) Book 18: Cycling Facilities, bike lanes are warranted on Campbell Street North while mixed-traffic conditions are considered adequate for Street ' $R$ ' given the lower speeds and traffic volumes projected along this roadway.

Within the proposed development, a multi-use path (MUP) will be provided within the open space adjacent to the creek that traverses the site from west to east. This MUP will cross Campbell Street North and is therefore a candidate for a pedestrian crossover (PXO) to provide network connectivity. Based on a review of projected traffic volumes at this crossing location, a Level 2 Type D PXO is recommended. Recommendations have also been made for the realignment of the MUP so that it crosses Colonel Talbot Road at its intersection with Diane Crescent/Royal Magnolia Avenue instead of 120 m north of this intersection. If the MUP were realigned as recommended, the mid-block pedestrian signals recommended in AECOM's report would no longer be required. The proposed MUP network realignment is shown in Exhibit 11.

Based on a review of the internal roadway network, it is also recommended that traffic calming measures be provided along Campbell Street North to encourage lower operating speeds. A conceptual traffic calming plan has been provided in Exhibit 12 which includes traffic calming measures such as curb extensions and the use of a raised crosswalk at the PXO. This exhibit also illustrates potential locations for bus stops within the vicinity of the proposed development.

There is currently no transit service within reasonable walking distance of the proposed development. It is recommended that transit service be extended to the surrounding area and bus stops be provided along Colonel Talbot Road, Pack Road and Royal Magnolia Avenue to provide residents with access to transit.

The overall conclusion of this TIA is that traffic generated by the proposed W3 Sunset Creek subdivision can be safely accommodated on the adjacent road network with consideration of the mitigation measures identified above. It is recommended that the City of London review the need for capital improvements in the area to ensure that sufficient roadway capacity is provided to accommodate projected growth.

## 1 Introduction

Arcadis IBI Group has been retained by W3 Lambeth Farms Inc. to undertake a Transportation Impact Assessment (TIA) in support of Draft Plan of Subdivision application for a proposed residential subdivision located east of Colonel Talbot Road, north of Royal Magnolia Avenue, in London, Ontario.

### 1.1 Study Objectives

The key objectives of the TIA are identified below:

- Determine the impact of the proposed development on the study area intersections;
- Confirm the timing of the planned roadway modifications; and
- Identify any deficiencies in the road network and develop recommendations to mitigate these deficiencies.


### 1.2 Study Methodology

The TIA approach and methodology is based on the City of London Transportation Impact Assessment Guidelines (April 2012). City of London staff were consulted to confirm the following study parameters and assumptions:

- Study Area Intersections
- Analysis Time Periods
- Analysis Years
- Trip Generation
- Background Traffic Growth Rate
- Adjacent Developments

The above study parameters and assumptions were communicated to the City of London staff via email on May 16, 2023. City staff provided approval of these parameters on July 10, 2023, with a request for some minor modifications to the proposed study area. Approval of the proposed background traffic growth rate was provided on August 3, 2023.
Figure 1 illustrates the study area intersections that will be assessed as part of this study.

Figure 1 - Study Area Intersections


### 1.3 Reference Material

The following reference material was used in the preparation of this report:

- City of London Transportation Impact Assessment Guidelines (2012)
- City of London Access Management Guidelines (2015)
- City of London Official Plan (2016)
- City of London Transportation Master Plan (Aecom, 2013)
- City of London Cycling Master Plan (MMM Group, 2016)
- City of London 2021 Development Charges Background Study Update (2020)
- City of London 2016 Household Travel Survey Summary Report (IBI Group, 2018)
- W3 Subdivision Study (BT Engineering, 2016)
- 3493 Colonel Talbot TIS (Paradigm, 2015)
- Colonel Talbot Subdivision TIS (Stantec, 2016)
- 3080 Bostwick TIS (IBI Group, 2016 \& 2018)
- 3510-3524 Colonel Talbot Road TIA (SBM, 2021)
- Southwest Secondary Plan (2019)
- Southwest Area Plan Transportation Servicing Report (Aecom, 2010)
- Draft Colonel Talbot Road Two-Lane Upgrade Traffic Analysis Memo (Aecom, 2023)


## 2 Proposed Development

### 2.1 Land Uses

The subject site is currently occupied by agricultural land uses, including a single farmhouse and outlying farm structures. It is generally bound by Colonel Talbot Road to the west, Royal Magnolia Avenue to the south and east and agricultural land uses to the north. The property is municipally known as 3680, 3690 \& 3700 Colonel Talbot Road. Based on the zoning CityMap, the lands are currently zoned as NF (Neighbourhood Facility), OS4 (Open Space) and UR4 (Urban Reserve).

The proposed development will be composed of a mix of low-density, medium-density and higher density residential land uses as well as some limited neighbourhood-oriented commercial land uses. Access to Colonel Talbot Road will be provided via Royal Magnolia Avenue and Street ' N '. In the future, it is expected that connections with the planned Hudson Park development to the north via Campbell Street North and Street ' $R$ ' will provide residents of the development access to Pack Road, however, these connections are not expected to be completed within the horizon year of this study. The proposed development is bisected by a natural corridor along which a multiuse path (MUP) will be provided.

Table 1 presents a summary of the proposed land uses and Exhibit 1 illustrates the layout of the proposed development.

Table 1 - Proposed Land Uses

| LAND USE | SIZE |
| :--- | :---: |
| Single Family Homes | 163 units |
| Street Townhomes | 16 units |
| Cluster Housing | 522 units |
| Mid-Rise Apartments | 276 units |
| High-Rise Apartments | 338 units |

In addition to the above, the higher density blocks proposed near the Royal Magnolia \& Campbell intersection are intended to include small-scale ground level retail and services for the local community.

### 2.2 Phasing

The proposed development is expected to be built in a single phase with full buildout anticipated for 2033. This study will therefore analyze traffic conditions at the following analysis years:

- Existing Traffic
- Future (2033) Background and Total Traffic
- Future (2038) Background and Total Traffic



### 2.3 Transportation Demand Management

The City of London TMP outlines several active transportation and Transportation Demand Management (TDM) policies as the City shifts towards more sustainable modes, such as walking, cycling and transit. TDM plays a significant role in this process as it often involves low-cost, but high-benefit initiatives or improvements. The Transportation Master Plan (TMP) outlines 28 priority actions for the City to undertake in support of sustainable travel modes, ranging from short-term to long-term measures.
Within the proposed developments, sustainable transportation modes will be encouraged through the provision of active transportation facilities such as sidewalks and bicycle facilities, as discussed in Section 8 of this report.

## 3 Existing Transportation Network

### 3.1 Existing Road Network

### 3.1.1 Roadways

Table 2 provides a summary of all existing roadways within the study area. All of these roads are under the jurisdiction of the City of London.

Table 2 - Existing Road Network Details

| ROADWAY | POSTED SPEED LIMIT | CLASSIFICATION | CROSS SECTION | EXTENTS |
| :---: | :---: | :---: | :---: | :---: |
| Main Street | $50 \mathrm{~km} / \mathrm{h}$ | Civic Boulevard/ Main Street | Urban, 3-lane, undivided | Colonel Talbot to Campbell |
| Wharncliffe Road South | $60 \mathrm{~km} / \mathrm{h}$ | Civic Boulevard | Rural, 4-lane, undivided | Campbell to Riverside |
| Colonel Talbot Road | 60 km/h | Civic Boulevard | Rural, 2-lane, undivided | Byron Baseline to Southminster Bourne |
| Bostwick Road | 70 km/h | Civic Boulevard | Rural, 2-lane, undivided | Southdale to Wharncliffe |
| Pack Road | $60 \mathrm{~km} / \mathrm{h}$ | Civic Boulevard | Rural, 2-lane, undivided | Holmwood to Bostwick |
| Kilbourne Road | $60 \mathrm{~km} / \mathrm{h}$ | Neighbourhood Connector | Urban, 2-lane, undivided | Longwoods to Colonel Talbot |
| Campbell Street North | $50 \mathrm{~km} / \mathrm{h}$ | Neighbourhood Connector | Urban, 2-lane, undivided | North of Main/ Wharncliffe |
| Campbell Street | $50 \mathrm{~km} / \mathrm{h}$ | Neighbourhood Connector | Urban, 2-lane, undivided | Main/ Wharncliffe to Sunray |
| Clayton Walk | $50 \mathrm{~km} / \mathrm{h}$ | Local | Urban, 2-lane, undivided | West Graham to Colonel Talbot |
| Diane Crescent | $50 \mathrm{~km} / \mathrm{h}$ | Local | Urban, 2-lane, undivided | Malpass to Colonel Talbot |

### 3.1.2 Intersections

The following key intersections are located within the study area:

- Main Street/Wharncliffe Road South \& Campbell Street/Campbell Street North (signalized)
- Colonel Talbot Road \& Pack Road (signalized)
- Colonel Talbot Road \& Clayton Walk (unsignalized)
- Colonel Talbot Road \& Diane Crescent (unsignalized)
- Colonel Talbot Road \& Kilbourne Road (unsignalized)
- Bostwick Road \& Pack Road (unsignalized)

The existing lane configurations and parallel lane lengths are shown in Exhibit 2.


### 3.2 Existing Pedestrian and Bicycle Facilities

Within the study area, sidewalks currently exist at the following locations:

- East side of Campbell Street North and west side of Campbell Street
- West side of Colonel Talbot Road from Clayton Walk to Pack Road and east side of Colonel Talbot Road north of Pack Road
- South side of Pack Road west of Colonel Talbot Road and north side of Pack Road from Colonel Talbot Road to Frontier Avenue
- Both sides of Main Street, Clayton Walk, Kilbourne Road, Settlement Trail, and Pioneer Parkway
- South side of Diane Crescent

In addition to the above pedestrian infrastructure, there is also a network of multi-use paths (MUPs) in the northeast and southwest quadrants of the Colonel Talbot \& Pack intersection. With the exception of bike lanes on the existing segment of Campbell Street North and isolated measures at the Main/Wharncliffe \& Campbell intersection, there are otherwise no exclusive cycling facilities anywhere within the study area.

### 3.3 Existing Transit Service and Facilities

The nearest transit routes are Route \#24 on Raleigh Boulevard ( $\sim 1,200 \mathrm{~m}$ north of the proposed development) and Route \#28 on Main Street ( $\sim 1,450 \mathrm{~m}$ south of the proposed development). The details of these two transit routes are summarized below in Table 3.

Table 3 - Transit Routes

| ROUTE <br> NUMBER | TERMINI | FREQUENCY |
| :---: | :---: | :---: |
| 24 | Talbot Village to Summerside | 45-minute headways (Monday to Friday), 40- <br> to 45-minute headways (Saturday) and 40- <br> minute headways (Sunday) |
| 28 | White Oaks Mall to Lambeth | 40-minute headways (Monday to Friday), <br> peak period service only |

Figure 2 illustrates the transit routes that operate in the vicinity of the study area. The transit service maps for each of the above routes are provided in Appendix A.

Figure 2 - Transit Routes


### 3.4 Collision Analysis

Historical collision data for the period of January 2015 to May 2023 was provided by the City of London for all of the study area road segments and intersections. The subsequent sections discuss the results of the collision analysis.

Detailed collision records are provided in Appendix B.

### 3.4.1 Roadway Segments

Table 4 below summarizes the number of collisions per type that have occurred along each roadway segment. Particular collision types that have occurred eight times or more (i.e., on average once a year) along a particular roadway segment have been emphasized as these collisions warrant further review to establish if there is a repeating pattern of collisions.

Table 4 - Number of Collisions: Roadway Segments

| ROADWAY SEGMENT | COLLISION TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 患 |  | $\begin{aligned} & \text { 울 } \\ & \stackrel{\rightharpoonup}{\Phi} \end{aligned}$ | 응 |
| Colonel Talbot - Pack to Clayton | 1 | 1 |  | 1 | 8 |  | 2 | 13 |
| Colonel Talbot - Clayton to Diane |  | 1 | 1 | 1 | 4 |  |  | 7 |
| Colonel Talbot - Diane to Kilbourne | 1 | 1 | 2 | 1 | 2 |  |  | 7 |
| Pack - Bostwick to Regiment |  |  |  |  | 10 |  |  | 10 |
| Pack - Regiment to Frontier |  |  |  |  | 3 | 1 |  | 4 |
| Pack - Frontier to Pioneer |  |  |  |  | 1 |  |  | 1 |
| Pack - Pioneer to Settlement |  |  |  |  |  |  |  |  |
| Pack - Settlement to Colonel Talbot |  |  |  | 1 |  |  |  | 1 |
| Total | 2 | 3 | 3 | 4 | 28 | 1 | 2 | 43 |

Notes: SMV = Single Motor Vehicle
As shown above, animal-related collisions on Colonel Talbot Road between Pack Road and Clayton Walk and on Pack Road between Bostwick Road and Regiment Road are occurring relatively frequently. A review of these collisions indicates that approximately $50 \%$ and $60 \%$ of these collisions on Colonel Talbot Road and Pack Road, respectively, are occurring under dark conditions (i.e., before 7 am and after 9 pm ). As such, providing illumination along these roadways (if not currently provided) may help reduce the frequency of these collisions.

### 3.4.2 Intersections

Table 5 below summarizes the number of collisions per collision type that have occurred at each study area intersection. Particular collision types that have occurred eight times or more (i.e., on average once a year) along a particular roadway segment have been emphasized as these collisions warrant further review to establish if there is a repeating pattern of collisions. Additionally, the number of collisions per million vehicles entering (MVE) has also been calculated for each intersection. Generally, a rate of 1.0 or more collisions per MVE is considered significant.

Table 5 - Number of Collisions: Intersections

| INTERSECTION | COLLISION TYPE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\begin{gathered} \stackrel{\rightharpoonup}{0} \\ \frac{0}{\infty} \end{gathered}$ |  | $\begin{aligned} & \stackrel{\mathrm{O}}{\stackrel{\rightharpoonup}{\top}} \end{aligned}$ | $\begin{aligned} & \stackrel{-1}{\stackrel{-}{2}} \end{aligned}$ |  |
| Colonel Talbot \& Pack |  | 4 | 3 | 1 | 14 | 2 | 3 | 27 | 0.72 |
| Colonel Talbot \& Clayton |  |  |  |  |  |  | 1 | 1 | 0.03 |
| Colonel Talbot \& Diane |  | 1 |  |  |  |  |  | 1 | 0.04 |
| Colonel Talbot \& Kilbourne |  | 2 |  |  |  | 1 |  | 3 | 0.10 |
| Bostwick \& Pack |  | 2 | 2 | 3 | 6 | 1 | 2 | 16 | 0.83 |
| Main/Wharncliffe \& Campbell | 1 | 12 | 4 | 1 | 6 |  | 1 | 25 | 0.60 |
| Total | 1 | 21 | 9 | 5 | 26 | 4 | 7 | 73 | - |

Notes: SMV = Single Motor Vehicle, MVE = Million Vehicles Entering
As illustrated above, there is a high frequency of angle collisions at three of the intersections and a high frequency of rear end collisions at the Main/Wharncliffe \& Campbell intersection. None of the intersections experience a collision rate per MVE higher than 1.0 indicating that the rate of collisions observed at these intersections is normal for the volume of traffic passing through.

It is noteworthy that the Colonel Talbot \& Pack intersection was signalized in 2021 but this doesn't appear to have had any impact on the rate at which angle collisions occur at the intersection.
A detailed review of these collisions indicates that improper driver behaviour accounts for $50 \%$ of angle collisions at all three intersections and $58 \%$ of rear end collisions at the Main/Wharncliffe \& Campbell intersection. For angle collisions, drivers generally failed to yield the right of way, failed to stop at the red light or stop sign, or performed improper turns. For rear end collisions, following too close was a frequent cause of collisions.

Poor roadway conditions were also a major contributing factor to many of these collisions, as summarized below:

- Colonel Talbot \& Pack (Angle): 14\% of collisions
- Bostwick \& Pack (Angle): 50\% of collisions
- Main/Wharncliffe \& Campbell (Angle): 33\% of collisions
- Main/Wharncliffe \& Campbell (Rear End): $17 \%$ of collisions

A number of collisions had no obvious cause (i.e., neither weather, road condition nor driver behaviour contributed to these collisions).
With respect to the travel direction of vehicles involved in the collisions, collisions at the Main/Wharncliffe \& Campbell intersection were generally caused by vehicles travelling in the eastbound and westbound directions which corresponds with the movements with the highest traffic volumes. This may indicate that congestion and/or high speeds at the intersection could be contributing to these collisions. No obvious directional patterns were observed at the other two intersections.

## 4 Future Transportation Network

The City of London is currently in the midst of developing its Mobility Master Plan which will establish how the City will prioritize transportation and mobility infrastructure until 2050. The development of the Plan is currently at Phase 1 of 3. As such, this study has referenced the 2013 City of London Transportation Master Plan (TMP) to determine how the transportation network will change within the timeframe of this study. The TMP projections have been supplemented by the more recent 2021 Development Charges (DC) Background Study Update (October 2020), which allocates funds and assigns expected completion dates to specific capital projects.

### 4.1 Future Road Network

The TMP and 2021 DC study outline future capital projects throughout the City. Projects that may impact traffic patterns near the proposed development have been documented below:

## Southdale Road West \& Colonel Talbot Road Intersection

The Southdale Road West \& Colonel Talbot Road intersection is currently being replaced with a two-lane roundabout.

## Colonel Talbot Road

The 2021 DC study indicates that Colonel Talbot Road will undergo an upgrade from a rural to an urban cross-section from 300m south of Southdale Road West to James Street in 2023. The City of London webpage for this project suggests that the timeline for this project has recently been revised to 2024-2025. The Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) was provided by City staff and recommends the following traffic controls and lane configurations:

- Colonel Talbot \& Pack: It was recommended that the existing lane configuration be maintained but that optimized signal timings and a protected-permitted southbound left-turn phase during the weekday afternoon peak hour be implemented.
- Colonel Talbot \& Clayton Walk: Two-way stop-controlled intersection with left-turn and shared through-right lanes on the northbound and southbound approaches, leftturn and shared through-right lanes on the eastbound approach and shared allmovements lane on the westbound approach. The memorandum recommends a minimum of 45 m of storage for the southbound left-turn lane.
- Colonel Talbot \& Diane/Royal Magnolia: Two-way stop-controlled intersection with left-turn and shared through-right lanes on the northbound and southbound approaches, a shared all-movements lane on the eastbound approach and right-turn and shared through-left lane on the westbound approach.
- Colonel Talbot \& Kilbourne/Hayward: Signalized intersection with left-turn lanes on all approaches, separate through and right-turn lanes on the northbound approach and shared through-right lanes on all other approaches.

The memorandum further recommends that mid-block pedestrian signals be installed on Colonel Talbot Road approximately 120m north of Diane Crescent/Royal Magnolia Avenue. As noted in Section 8.2, this report recommends that pedestrian/bicycle crossing facilities be provided at the Colonel Talbot \& Diane/Royal Magnolia intersection instead to avoid having two closely spaced traffic signals.

The City project webpage indicates that, in addition to these intersection modifications, the urbanization of Colonel Talbot Road will include the addition of concrete curbs and gutters, new streetlights, boulevard bike paths, sidewalks and localized medians.

## Southdale Road West

The TMP indicates that Southdale Road West will be widened to 4 lanes between Colonel Talbot Road and Wharncliffe Road South. Southdale Road West has since been widened to 4 lanes from west of Pine Valley Boulevard to Wharncliffe Road South and the segment from Bostwick Road/Farnham Road to west of Pine Valley Boulevard has recently been widened to four lanes with substantial completion planned for end of 2023. The remainder will be widened in 2031.

## Bostwick Road

The TMP does not identify any widenings for Bostwick Road, however, the 2021 DC study indicates that the segment between Southdale Road West and Pack Road will be urbanized in 2025 and the segment between Pack Road and Wharncliffe Road South will be widened to four lanes and realigned in 2026. The Bostwick Road Realignment Municipal Class Environmental Assessment Study Report (Parsons, March 2019) outlines the planned roadway configuration for Bostwick Road and indicates that both the two-lane and four-lane roadway cross-sections will feature a centre median as well as concrete sidewalks and cycle tracks on both side of the roadway.

## Bradley Avenue

Based on the TMP, Bradley Avenue is planned to be extended from White Oak Road to Bostwick Road. Since the TMP was completed, the segment of Bradley Avenue between Wharncliffe Road South and Wonderland Road South has been constructed. The 2021 DC study indicates that the segment between White Oak Road and Wharncliffe Road South was originally planned to be constructed in 2023, followed by the segment between Bostwick Road and Wonderland Road South in 2028, however there is no indication that the works between White Oak and Wharncliffe have started at the time of this study. The existing segment of Bradley Avenue between Wonderland Road and Wharncliffe Road has a centre median, sidewalks on both sides of the road and a two-way cycle track on the south side of the road. It is assumed that this roadway cross-section configuration will be maintained as the road is extended west to Bostwick Road.

## Pack Road

The 2021 DC study indicates that Pack Road is anticipated to be urbanized between Colonel Talbot Road and Bostwick Road in 2032.

## Bostwick Road \& Pack Road/Bradley Avenue Intersection

The Bostwick Road Realignment Municipal Class Environmental Assessment Study Report (Parsons, March 2019) indicates that the Bostwick \& Pack/Bradley intersection will be configured as a two-lane roundabout with dual entry and exit lanes on all approaches. The cycle tracks on Bostwick Road and Bradley Avenue will transition to MUPs at the roundabout in order to allow bicyclists to cross together with pedestrians.

Overall, the above roadway network improvements will facilitate travel to/from the east, particularly the Bradley Avenue extension which will provide an alternative east-west route in this part of the city.

Exhibit 3 illustrates the future planned intersection lane configuration and traffic controls based on the above City projects.


### 4.2 Future Pedestrian and Bicycle Facilities

The City of London TMP has identified active transportation (i.e., walking and cycling) as a critical element of the future transportation network. In September 2016, the City approved the Cycling Master Plan (CMP), which provides details regarding the planning, design and staging of cycling infrastructure in the City. The CMP indicates that a buffered bike lane will be provided on the portion of Pack Road east of Colonel Talbot Road and a buffered paved shoulder will be provided on the portion west of Colonel Talbot Road. The CMP indicates that the proposed cycling facilities on Pack Road are planned to be implemented by 2031.
A recent technical amendment to the CMP has also identified the need for cycling facilities along Campbell Street North (Pack Road to James Street), Street 'R' (Pack Road to Royal Magnolia Avenue) and Royal Magnolia Avenue (Colonel Talbot Road to Bostwick Road). It should be noted that cycling facilities are not included in the design of the existing section of Royal Magnolia Avenue from Colonel Talbot Road to Big Leaf Trail but cycling facilities may be included (by others) for the remaining segment east to Bostwick Road. The portions of Campbell Street North and Street ' $R$ ' within the proposed development have been reviewed as part of this study to determine the recommended type of cycling facility for each of these roads. The results of this review are provided in Section 8.2.

A number of multi-use paths are planned within the surrounding area and cycling desire lines have been identified that pass through the proposed development.
Figure 3 illustrates the planned cycling network within the study area.
Figure 3 - Future Cycling Network


```
Existing Cycling Routes
-_Multi Use Pathway
—— In-Boulevard Facility
- Bike Lane
- Signed Bike Route with Sharrow
-_Signed Bike Route
Proposed Facility Types
- = Multi-Use Pathway
-=. In-Boulevard Facility
- - - Cycle Track
- Buffered Bike Lane
==" Bike Lane
■ Buffered Paved Shoulder
- =- Paved Shoulder
- =- Signed Route with Edgeline
- =- Signed Bike Route with Sharrow
- =- : Signed Bike Route
.... Desired Connection \({ }^{1}\)
```

Source: City of London Cycling Master Plan (September 2016)
The Official Plan (OP) and Southwest Area Plan (SWAP) also identify the planned multi-use path (MUP) network within the study area which generally conforms to the MUP network outlined in the TMP.
Figure 4 illustrates the future multi-use path (MUP) network within the study area.

Figure 4 - Future Multi-Use Path Network

Multi-Use Pathways
Existing Route
On-Road Route
Planned Route

Source: City of London Southwest Area Plan (December 2019)

### 4.3 Future Transit Service and Facilities

The TMP does not identify any transit service improvements which will have a direct impact on the study area. The Southwest Area Plan (SWAP) Transportation Servicing Report (TSR), however, recommended future transit routes in the study area, including a route along Pack Road, as illustrated in Figure 5.

Figure 5 - Potential Transit Routes


Source: City of London Southwest Area Plan Transportation Servicing Report (May 2010)

### 4.4 Future Adjacent Developments

The City of London noted that the following adjacent developments are anticipated to contribute traffic volumes to the study area intersections:

Table 6 - Adjacent Developments

| ADJACENT <br> DEVELOPMENT | BUILDOUT YEAR | LAND USES |
| :--- | :--- | :--- |
|  |  | 16 townhomes |
| 3080 Bostwick Road | Prior to 2033 ${ }^{1}$ | 48 stacked townhomes |
|  |  | 2,464 high-rise residential units |
|  |  | $21,528 \mathrm{ft}^{2}$ of commercial space |
|  |  | $43,056 \mathrm{ft}^{2}$ of office space |
|  |  | 376 single family homes |
| W3 Farms Residential | Prior to 238 street townhomes <br> Development | 113 cluster townhomes |
|  |  | 476 apartment units with convenience |
|  |  | commercial and small-scale offices |
|  |  | 32 mixed-use residential/commercial units |
|  |  | 2.0 -hectare elementary school |


| ADJACENT DEVELOPMENT | BUILDOUT YEAR | LAND USES |
| :---: | :---: | :---: |
| Colonel Talbot Subdivision ${ }^{2}$ | Prior to $2033{ }^{1}$ | 538 single family homes <br> 776 condominium/townhome units |
| 3493 Colonel Talbot Road | 2024 | 177 single family homes <br> 314 condominium/townhome units $10,765 \mathrm{ft}^{2}$ of group floor auxiliary commercial space |
| Westwinds Subdivision | 2024 to 2030 | 46 single family homes <br> 37 street townhomes <br> 56 cluster townhomes <br> 610 mid-rise apartment units |
| Kilbourne Subdivision | 2024 to 2035 | 488 single family homes <br> 213 street townhomes <br> 602 cluster housing units <br> 762 mid-rise apartment units <br> 1,076 high-rise apartment units |
| Foxwood Development | 2024 to 2028 | 462 mid-rise apartment units |
| 3510-3524 Colonel Talbot Road | Imminently | 37 mid-rise apartment units $434 \mathrm{~m}^{2}$ of ground floor commercial space |
| Hudson Park Subdivision ${ }^{3}$ | Prior to $2033{ }^{1}$ | 192 single family homes 339 multi-family housing units |

Notes:
${ }^{1}$ - The stated buildout years for these developments are no longer expected to be accurate. It is assumed that these developments will be fully built-out prior to 2033.
${ }^{2}$ - The traffic generation for this development has been based on the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) as the 2015 Paradigm TIA used outdated land use statistics for the site.
${ }^{3}$ - A TIA has yet not been prepared for this development. The land use statistics and trip generation for this development are based on the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023).

The buildout dates identified above are conservative estimates based on the latest information available, however, market conditions will ultimately dictate when these future adjacent developments will be built out.
Exhibit 4 illustrates the locations of the future adjacent developments identified above.


IBI GROUP

W3 Sunset Creek
Transportation Impact Assessment

Exhibit 4:
Adjacent Developments

PROJECT No.
SCALE:


## 5 Traffic Volumes

### 5.1 Existing Traffic Volumes

Weekday morning and afternoon peak hour traffic counts were obtained for the following intersections:

- Main/Wharncliffe \& Campbell (City of London, November 2021)
- Bostwick \& Pack (Arcadis IBI Group c/o Horizon Data Services, November 2021)
- Colonel Talbot \& Pack (City of London, September 2022)
- Colonel Talbot \& Clayton (City of London, November 2022)
- Colonel Talbot \& Diane (City of London, November 2022)
- Colonel Talbot \& Kilbourne (City of London, September 2022)

Given that two of the traffic counts were completed in 2021 during the COVID-19 pandemic, supplementary traffic counts were obtained for nearby adjacent intersections to determine whether any adjustment factors are required to account for the impact of the pandemic on traffic volumes. The supplementary traffic counts obtained were:

- Colonel Talbot \& Main (City of London, September 2022)
- Wharncliffe \& Exeter (City of London, March 2023)
- Southdale \& Bostwick (City of London, May 2019)

Compared to the adjacent intersection volumes, traffic volumes at the Bostwick \& Pack intersection did not appear to have been notably impacted by the COVID-19 pandemic. As such, no adjustment factors were applied to the traffic volumes at that intersection.

Traffic volumes and travel patterns at the Main/Wharncliffe \& Campbell intersection appear to have been impacted by the COVID-19 pandemic with weekday morning peak hour volumes $30 \%$ higher and weekday afternoon peak hour volumes $8 \%$ lower than would be expected. As such, an adjustment factor has been conservatively applied to the weekday afternoon peak hour volumes to better estimate typical conditions. No adjustment factor has been applied to weekday morning peak hour volumes as a conservative measure.

Traffic volumes representative of Existing Traffic conditions are provided in Exhibit 5. The turning movement counts collected for this study have been provided in Appendix C.


### 5.2 Future Background Traffic Volumes

As agreed with City of London staff ${ }^{1}$, a $1.5 \%$ linear annual growth rate has been applied to the study area intersections in order to account for regional traffic growth passing through the study area. The background traffic growth rate has not been applied to Clayton Walk, Diane Crescent, Campbell Street or Campbell Street North as these streets are not expected to experience growth in regional traffic. All traffic growth along these streets has been accounted for explicitly through the inclusion of adjacent development traffic projections.
The extension of Bradley Avenue to Bostwick Road is expected to result in a significant shift in traffic in the study area as it will provide an alternative east-west route. Consistent with the City of London's future traffic model projections, approximately $20 \%$ of traffic on Southdale Road east of Bostwick Road is expected to reroute to the Bradley Avenue extension. Figure 6 and Figure 7 illustrates how this diversion of eastbound and westbound traffic on Southdale Road to the Bradley Avenue extension will impact the study area intersections.

Figure 6 - Eastbound Traffic Rerouting


[^0]Figure 7 - Westbound Traffic Rerouting


The background traffic volumes were calculated by applying the growth rates to the existing traffic volumes, superimposing these volumes with adjacent development traffic, and adjusting the volumes to account for the projected rerouting of traffic due to the Bradley Avenue extension. The resulting Future (2033 \& 2038) Background Traffic volumes are presented in Exhibit 6 and Exhibit 7.



### 5.3 Trip Generation

The baseline traffic generation of the proposed developments was estimated using peak hour trip generation rates from the Institute of Transportation Engineers (ITE) Trip Generation Manual (11 ${ }^{\text {th }}$ Edition). These baseline vehicle-trips were subsequently converted into person-trips using the methodology outlined in the ITE Trip Generation Handbook ( $3^{\text {rd }}$ Edition) and were then subdivided into auto driver, auto passenger, transit, pedestrian, bicycle, and 'other' trips based on existing mode share distributions.

### 5.3.1 Baseline Vehicle Trip Generation

Based on the ITE Trip Generation Manual, the baseline vehicle trip generation of the proposed development has been calculated and is summarized below in Table 7.
Extracts from the ITE Trip Generation Manual have been provided in Appendix D.
Table 7 - Baseline Vehicle Trip Generation

| LAND USE | SIZE | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |  |  |  |  |  |  |  |  |
| Single Family Homes | 163 units | 29 | 87 | 116 | 99 | 58 | 157 |  |  |  |  |  |  |  |  |
| Street Townhomes | 16 units | 2 | 6 | 8 | 5 | 4 | 9 |  |  |  |  |  |  |  |  |
| Cluster Housing | 522 units | 50 | 168 | 218 | 124 | 80 | 204 |  |  |  |  |  |  |  |  |
| Mid-Rise Apartments | 276 units | 25 | 85 | 110 | 66 | 42 | 108 |  |  |  |  |  |  |  |  |
| High-Rise Apartments | 338 units | 24 | 69 | 93 | 69 | 42 | 111 |  |  |  |  |  |  |  |  |
| Total |  |  |  |  |  |  |  |  |  | $\mathbf{1 3 0}$ | $\mathbf{4 1 5}$ | $\mathbf{5 4 5}$ | $\mathbf{3 6 3}$ | $\mathbf{2 2 6}$ | $\mathbf{5 8 9}$ |

### 5.3.2 Person Trip Generation

The ITE trip generation rates for residential land uses are based on data collected from traffic surveys conducted across North America over the past 20-30 years in mostly suburban areas where transit usage is traditionally very low. The ITE Trip Generation Handbook (3 $3^{\text {rd }}$ Edition) provides the mode share distribution of several survey sites that were used for developing the trip generation rates. Based on these surveys, approximately $97 \%$ of trips generated by these developments were via private automobile (either as a driver or passenger) with an average vehicle occupancy of 1.15. Of the $3 \%$ of trips via sustainable modes of transportation (i.e., transit, walk or bike), only $0.1 \%$ of trips were transit trips. This indicates that these developments generate approximately 1.19 person-trips per baseline vehicle-trip.
Assuming 1.19 person-trips are generated per baseline vehicle-trip, the proposed development is expected to generate the following number of person-trips:

Table 8 - Person Trip Generation

| LAND USE | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
| Single Family Homes | 35 | 104 | 139 | 118 | 69 | 187 |
| Street Townhomes | 2 | 7 | 9 | 6 | 5 | 11 |
| Cluster Housing | 60 | 200 | 260 | 148 | 95 | 243 |
| Mid-Rise Apartments | 30 | 101 | 131 | 79 | 50 | 129 |
| High-Rise Apartments |  | 29 | 82 | 111 | 82 | 50 |
|  | Total | $\mathbf{1 5 6}$ | $\mathbf{4 9 4}$ | $\mathbf{6 5 0}$ | $\mathbf{4 3 3}$ | $\mathbf{2 6 9}$ |

### 5.3.3 Mode Share

The 2016 Household Travel Survey Summary Report (IBI Group, July 2016) indicates that within the City of London, the current mode share distribution is as follows:

- Auto Driver: 62.5\%
- Auto Passenger: $14.1 \%$
- Transit: 7.6\%
- Walk: $11.3 \%$
- Bicycle: 1.4\%
- Other: 3.2\%

As the surrounding area becomes more developed, it is anticipated that transit service will be extended to the area. Additionally, the adjacent W3 Farms Residential Development will include an elementary school and some mixed-use commercial land uses. As such, future internal and adjacent land uses will provide amenities within walking/biking distance of the site. It is, therefore, expected that the mode share distribution described above will be achievable for the proposed development. The largely car-oriented nature of the surrounding area is unlikely to support higher non-auto mode shares, however.

### 5.3.4 Summary of Trip Generation

Applying the mode share distribution from Section 5.3 .3 to the person-trip estimates from Table 8, the number of person-trips per mode was calculated and is summarized below in Table 9.

Table 9 - Person-Trips per Mode

| TRAVEL MODE | AM PEAK HOUR |  |  | PM PEAK HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN | OUT | TOTAL | IN | OUT | TOTAL |
| Auto Driver | 97 | 309 | 407 | 270 | 168 | 439 |
| Auto Passenger | 22 | 69 | 92 | 61 | 38 | 99 |
| Transit | 12 | 37 | 50 | 33 | 20 | 53 |
| Walk | 18 | 56 | 74 | 49 | 30 | 79 |
| Bicycle | 2 | 7 | 9 | 6 | 4 | 10 |
| Other | 5 | 16 | $\mathbf{2 1}$ | 14 | 9 | 23 |
| Total | $\mathbf{1 5 6}$ | $\mathbf{4 9 4}$ | $\mathbf{6 5 0}$ | $\mathbf{4 3 3}$ | $\mathbf{2 6 9}$ | $\mathbf{7 0 2}$ |

### 5.4 Trip Distribution and Assignment

The distribution of development-generated traffic was based primarily on the City of London 2016 Household Travel Survey. It is estimated that site-generated traffic will distribute as follows:

- $35 \%$ to/from the North via Colonel Talbot Road
- $15 \%$ to/from the South
- $10 \%$ via Colonel Talbot Road
- $5 \%$ via Campbell Street North
- $50 \%$ to/from the East
- $35 \%$ via Pack Road/Bradley Avenue
- $10 \%$ via Royal Magnolia Avenue
- 5\% via Campbell Street North

Using the above distribution, development-generated traffic was assigned to the adjacent road network based on engineering judgement. Based on the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023), it is understood that left turns from side streets on Colonel Talbot Road will experience very high delays due to significant volumes of mainline traffic. As such, it is anticipated that all left-turns onto Colonel Talbot Road will be completed at the Colonel Talbot \& Diane/Royal Magnolia intersection as this arterial-to-collector intersection is expected to ultimately be signalized in the future. Exhibit 8 illustrates the projected development-generated traffic volumes.

### 5.5 Future Total Traffic Volumes

The future background traffic volumes were superimposed with the site-generated traffic volumes to estimate the future total traffic volumes, as presented in Exhibit 9 and Exhibit 10.




## 6 Intersection Capacity Analysis

Traffic operations at all study area intersections were evaluated using Synchro v11 and SIDRA Intersections v9.0 for the weekday morning and afternoon peak hours under the following traffic conditions:

- Existing Traffic
- Future (2033) Background and Total Traffic
- Future (2038) Background and Total Traffic


### 6.1 Intersection Capacity Analysis Criteria

In qualitative terms, Level of Service (LOS) describes a user's perception of the operational conditions of a transportation facility. For vehicular LOS, these conditions are generally defined in terms of delay, speed and travel time, freedom to manoeuvre, traffic interruptions, safety, comfort and convenience. The two key metrics used to evaluate vehicular LOS are as follows:

- Volume to Capacity (v/c) Ratio: The ratio of traffic volume (either measured or forecast) to the capacity of the intersection or roadway.
- Average Delay: The average elapsed time from when a vehicle stops at the end of the queue until the vehicle departs from the stop line, including the time required for a vehicle to travel from the last-in-queue position to the first-in-queue position.

LOS is given a letter designation from ' $A$ ' to ' $F$ '. LOS ' $A$ ' represents the best operating conditions and LOS ' $E$ ' represents the level at which the intersection, or an approach to the intersection, is carrying the maximum traffic volume that can, practicably, be accommodated. LOS ' $F$ ' indicates that the facility is operating beyond its theoretical capacity.

The Highway Capacity Manual (HCM) 2010, prepared by the Transportation Research Board, includes the following Levels of Service criteria for signalized and unsignalized intersections, as indicated in Table 10.

Table 10 - Level of Service Thresholds

| LEVEL OF <br> SERVICE | SIGNALIZED | UNSIGNALIZED |
| :---: | :---: | :---: |
|  | Delay (Seconds per Vehicle) |  |

The TIA Guidelines indicate that intersections and turning movements that exceed the following thresholds should be identified:

- LOS 'E’ or worse.
- $\quad$ v/c ratio greater than 0.90 .
- $95^{\text {th }}$ percentile queues greater than the available storage capacity


### 6.2 Intersection Capacity Analysis Results

Based on the established intersection capacity analysis criteria described above, existing and future traffic conditions were analysed using the weekday morning and weekday afternoon peak hour traffic volumes derived in the previous sections of this report. The analysis results are progressive, in that any roadway modification required by a preceding traffic condition was assumed for future conditions. This format helps identify which modifications were triggered by the proposed development in each analysis year and which were triggered by background traffic.
Given the number of intersections within the study area, the following tables only illustrate the intersection capacity analysis results for movements which meet one or more of the thresholds described above.
For intersections where none of the movements meet any of the above criteria, only the overall intersection delay and LOS is shown.

The full intersection capacity analysis results have been provided in Appendix E.

### 6.2.1 Existing Traffic

The results of the intersection capacity analysis of Existing Traffic conditions are presented in Table 11.
Table 11 - Intersection Capacity Analysis: Existing Traffic

| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. DELAY <br> (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{aligned} & \text { 95TH } \\ & \text { PERCENTLLE } \\ & \text { QUEUE (m) } \\ & \hline \end{aligned}$ |  |
| Colonel Talbot \& Pack (signalized) | 9.2 (12.7) | A (B) | - | - (-) | - (-) | - (-) | - (-) | - |
| Colonel Talbot \& Clayton (unsignalized) | $\begin{gathered} 30.6 \\ (36.6) \end{gathered}$ | D (E) | EBL | 30.6 (36.6) | D (E) | 0.30 (0.22) | 8.4 (5.6) | 30 |
| Colonel Talbot \& Diane (unsignalized) | $\begin{gathered} 20.9 \\ (27.3) \end{gathered}$ | C (D) | - | - (-) | - (-) | - (-) | - (-) | - |
| Colonel Talbot \& Kilbourne (unsignalized) | $\begin{gathered} 28.7 \\ (47.1) \end{gathered}$ | D (E) | EBL | 28.7 (47.1) | D (E) | 0.21 (0.30) | 4.9 (8.4) | 45 |
| Bostwick \& Pack (unsignalized) | $\begin{gathered} 14.1 \\ (33.7) \\ \hline \end{gathered}$ | B (D) | - | - (-) | - (-) | - (-) | - (-) | - |
| Main/Wharncliffe |  |  | NBL | 21.2 (38.1) | C (D) | 0.21 (0.17) | 13.9 (12.3) | 5 |
| \& Campbell (signalized) | (12.3) | B (B) | SBL | 106.0 (59.7) | F (E) | 0.96 (0.66) | \#35.6 (34.5) | 45 |

Notes: Int. stands for Intersection. Only intersection capacity analysis results for critical movements are shown above.
As shown above, eastbound left movements at the intersections of Colonel Talbot \& Clayton and Colonel Talbot \& Kilbourne are currently approaching their theoretical capacity (i.e., LOS 'E'). At the Main/Wharncliffe \& Campbell intersection, northbound left-turn queues are exceeding the storage capacity and the southbound left-turn movement is experiencing high delays during both peak hours and is approaching its theoretical capacity in the weekday morning peak hour.

### 6.2.2 Future (2033) Background Traffic

As noted in Section 4.1, Colonel Talbot Road is expected to be urbanized in 2024-2025 which will result in the reconstruction of all the study area intersections along this corridor. It is assumed that by 2033, the roadway configurations, traffic controls and signal timing plans outlined in the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) will be implemented and therefore represent the baseline roadway configuration at this analysis year. The results of the intersection capacity analysis of Future (2033) Background Traffic conditions are presented in Table 12.

Table 12 - Intersection Capacity Analysis: Future (2033) Background Traffic

| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. DELAY (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{aligned} & \text { 95TH } \\ & \text { PERCENTILE } \\ & \text { QUEUE (m) } \end{aligned}$ |  |
| Colonel Talbot \& Pack $\left(\right.$ signalized) ${ }^{1}$ | $\begin{gathered} 26.0 \\ (59.3) \end{gathered}$ | C (E) | EBL | 101.9 (118.7) | F (F) | 0.73 (0.85) | \#35.0 (\#36.5) | 55 |
|  |  |  | WBL | 112.3 (96.2) | F (F) | 0.94 (0.98) | \#76.1 (\#105.5) | 55 |
|  |  |  | WBTR | 54.5 (69.1) | D (E) | 0.80 (0.98) | \#74.0 (\#134.1) | - |
|  |  |  | NBTR | 13.5 (64.9) | B (E) | 0.77 (1.05) | 175.5 (\#351.1) | - |
|  |  |  | SBL | 33.8 (166.1) | C (F) | 0.79 (1.22) | \#87.3 (\#76.6) | 120 |
| Colonel Talbot \& Pack (signalized) ${ }^{2}$ | $\begin{gathered} 16.9 \\ (30.6) \end{gathered}$ | B (C) | WBL | 53.5 (68.1) | D (E) | 0.65 (0.88) | 45.5 (\#86.4) | 55 |
| Colonel Talbot \& Clayton (unsignalized) | $\begin{gathered} 339.8 \\ (367.8) \end{gathered}$ | F (F) | EBL | 339.8 (367.8) | F (F) | 1.23 (1.05) | 38.5 (25.2) | 30 |
| Colonel Talbot \& Diane/Royal Magnolia (unsignalized) ${ }^{1}$ | $\begin{gathered} 259.4 \\ (506.1) \end{gathered}$ | F (F) | EBTRL | 259.4 (506.1) | F (F) | 0.96 (1.05) | 28.0 (19.6) | - |
|  |  |  | WBTL | 201.3 (298.7) | F (F) | 0.91 (0.74) | 29.4 (16.1) | - |
| Colonel Talbot \& Diane/Royal Magnolia (signalized) | 10.9 (8.3) | B (A) | - | - (-) | - (-) | - (-) | - (-) | - |
| Colonel Talbot \& Kilbourne (signalized) ${ }^{1}$ | $\begin{gathered} 19.1 \\ (15.3) \end{gathered}$ | B (B) | WBL | 57.8 (70.8) | E (E) | 0.85 (0.77) | \#68.7 (\#55.9) | - |


| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. DELAY <br> (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{gathered} \text { 95TH } \\ \text { PERCENTILE } \\ \text { QUEUE }(\mathrm{m}) \end{gathered}$ |  |
| Colonel Talbot \& Kilbourne (signalized) $^{3}$ | $\begin{gathered} 19.2 \\ (16.7) \end{gathered}$ | B (B) | - | - (-) | - (-) | - (-) | - (-) | - |
| Bostwick \& Pack (roundabout) | 8.1 (12.7) | A (B) | - | - (-) | - (-) | - (-) | - (-) | - |
| Main/Wharncliffe \& Campbell (signalized) | $\begin{gathered} 30.0 \\ (22.7) \end{gathered}$ | C (C) | EBL | 34.7 (90.1) | C (F) | 0.53 (1.01) | \#30.3 (\#50.4) | 45 |
|  |  |  | NBL | 19.3 (42.4) | B (D) | 0.20 (0.33) | 14.6 (17.1) | 5 |
|  |  |  | SBL | 93.4 (60.5) | F (E) | 0.98 (0.71) | \#49.0 (39.5) | 45 |
| Main/Wharncliffe \& Campbell (signalized) ${ }^{4}$ | $\begin{gathered} 26.6 \\ (20.8) \end{gathered}$ | C (C) | NBL | 32.7 (42.3) | C (D) | 0.28 (0.33) | 20.8 (17.1) | 5 |
|  |  |  | SBL | 45.1 (60.3) | D (E) | 0.74 (0.71) | \#41.1 (39.5) | 45 |

Notes: Int. stands for Intersection. Only intersection capacity analysis results for critical movements are shown above.
${ }^{1}$ Lane configuration and traffic signal timing plan based on the preferred design of the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023).
${ }^{2}$ Optimized signal timings in AM peak hour, increased cycle length from 110s to 130s in PM peak hour, added a protected-permitted westbound left-turn phase in the $A M$ and PM peak hour and added a northbound and westbound right-turn lane to the intersection.
${ }^{3}$ Optimized signal timings in AM and PM peak hour.
${ }^{4}$ Added a protected-permitted southbound left-turn phase and changed cycle length to 90s in AM peak hour, added a protected-permitted eastbound left-turn phase in the PM peak hour, added a westbound right-turn lane to the intersection.
As noted above, the analysis of the four Colonel Talbot Road intersections assumed that the baseline roadway configuration and traffic signal timing plans in 2033 would adhere to the preferred design of the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023). This memorandum had noted that in 2030:

- The Colonel Talbot \& Pack intersection would be operating at capacity;
- The intersections of Colonel Talbot \& Clayton and Colonel Talbot \& Diane/Royal Magnolia would be experiencing very high delays (LOS ' $F$ ') on the side street approaches; and
- Some left-turn movements at the Colonel Talbot \& Kilbourne intersection would be operating at LOS ' E '.

The results in Table 12 are therefore consistent with the above results.
It should be noted that the traffic projections developed for both this study and the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) indicate that Colonel Talbot Road will be exceeding the theoretical capacity of a two-lane road (i.e., over a 1,000 vehicles per hour in the peak direction) in the near future. This therefore indicates that Colonel Talbot Road will likely require four-lane widening if it is to accommodate the projected traffic demand.

As the Colonel Talbot \& Pack intersection was expected to be at capacity by 2030, it is not unexpected that its capacity would be exceeded after three years of background traffic growth. Adjustments to the signal timing plan may partially alleviate some of the capacity issues at the intersection, however, the addition of a protected-permitted westbound left-turn phase during both peak hours as well as the introduction of a northbound and westbound right-turn lane would ultimately be required in order to address the significant capacity issues anticipated under AECOM's preferred design. Consideration should be given to implementing these mitigation measures when Colonel Talbot Road is urbanized.

At the Colonel Talbot \& Clayton intersection, delays on the side street are expected to be significant due to the volume of traffic travelling along Colonel Talbot Road. It is expected that background traffic demand on the eastbound approach will gradually decrease over time due to the high delays through changes to travel behaviour and the use alternative routes to travel northbound on Colonel Talbot. The City should give consideration to implementing a peak period eastbound left-turn prohibition at this intersection or to physically restricting Clayton Walk to right-in/right-out only.

Royal Magnolia Avenue is classified as a neighbourhood connector. The purpose of such streets is to connect neighbourhood streets (i.e., local roads) to the arterial road network. In order to do this effectively and minimize cut through traffic along neighbourhood streets, delays at intersections between neighbourhood connectors and the arterial road network must be reasonable. Excessive delays will cause drivers to seek alternative routes, thereby undermining this road's role within the hierarchy of the road network. Were the Colonel Talbot \& Diane/Royal Magnolia intersection to remain unsignalized, it is expected that side street delays would be unacceptable and lead to unsafe driver behaviour. As such, there is a need to signalize this intersection when Colonel Talbot Road is urbanized rather than remain unsignalized as is recommended in the AECOM memorandum.
At the Colonel Talbot \& Kilbourne intersection, some minor traffic signal timing optimization is required in order to reduce delays on the westbound left-turn movement.

The Main/Wharncliffe \& Campbell intersection is expected to have some movements operate near or at capacity during both the weekday morning and afternoon peak hour in 2033. Although the intersection was only recently rebuilt, future traffic demand associated with adjacent developments will result in the need for a westbound right-turn lane to be introduced at this intersection, as well as protected-permitted southbound and eastbound left-turn phases in the weekday morning and afternoon peak hour, respectively, in order to address these capacity issues. Even with these mitigation measures, the southbound left-turn movement is still expected to operate at LOS ' E ' during the weekday morning peak hour but as the intersection as a whole is expected to operate at LOS 'C' no further mitigation measures are necessary.

The Bostwick \& Pack intersection is expected to have been reconstructed as a two-lane roundabout by 2033. The results of the intersection capacity analysis indicate that the intersection will operate at an acceptable Level of Service under this configuration.

### 6.2.3 Future (2038) Background Traffic

The results of the intersection capacity analysis of Future (2038) Background Traffic conditions are presented in Table 13. The analysis assumes that the required mitigation measures from the Future (2033) Background Traffic conditions analysis are implemented, and that signal timing optimization will occur on a regular basis.

Table 13 - Intersection Capacity Analysis: Future (2038) Background Traffic

| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. DELAY <br> (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{gathered} \text { 95TH } \\ \text { PERCENTILE } \\ \text { QUEUE (m) } \end{gathered}$ |  |
| Colonel Talbot \& Pack (signalized) | $\begin{gathered} 18.5 \\ (37.3) \end{gathered}$ | $B$ (D) | EBL | 53.4 (59.5) | D (E) | 0.39 (0.41) | 23.5 (28.1) | 55 |
|  |  |  | EBTR | 54.4 (63.5) | D (E) | 0.61 (0.70) | 41.8 (53.7) | - |
|  |  |  | WBL | 51.0 (81.7) | D (F) | 0.65 (0.93) | 47.1 (\#105.9) | 55 |
|  |  |  | WBR | 8.7 (22.3) | A (C) | 0.42 (0.67) | 16.7 (60.8) | 60 |
|  |  |  | NBT | 13.6 (41.4) | B (D) | 0.67 (0.93) | 148.1 (\#334.8) | - |
|  |  |  | SBL | 26.6 (83.5) | C (F) | 0.71 (0.95) | \#79.8 (\#83.1) | 120 |
| Colonel Talbot \& Clayton (unsignalized) | $\begin{gathered} 445.2 \\ (486.3) \end{gathered}$ | $F(F)$ | EBL | 445.2 (486.3) | F (F) | 1.44 (1.26) | 42.7 (27.3) | 30 |
| Colonel Talbot \& Diane/Royal Magnolia (signalized) | 12.2 (9.5) | B (A) | - | - (-) | - (-) | - (-) | - (-) | - |
| Colonel Talbot \& Kilbourne (signalized) | $\begin{gathered} 20.8 \\ (18.7) \end{gathered}$ | C (B) | WBL | 53.8 (60.0) | D (E) | 0.83 (0.71) | \#66.3 (48.4) | - |
| Bostwick \& Pack (roundabout) | 8.5 (14.2) | A (B) | - | - (-) | - (-) | - (-) | - (-) | - |
| Main/Wharncliffe \& Campbell (signalized) | $\begin{gathered} 28.0 \\ (23.9) \end{gathered}$ | C (C) | EBL | 18.8 (34.6) | B (C) | 0.38 (0.69) | 17.9 (\#65.4) | 45 |
|  |  |  | WBL | 58.2 (24.3) | E (C) | 0.89 (0.58) | \#74.1 (39.8) | - |
|  |  |  | NBL | 32.7 (42.9) | C (D) | 0.28 (0.34) | 20.8 (17.4) | 5 |
|  |  |  | SBL | 57.0 (61.3) | E (E) | 0.81 (0.71) | \#45.5 (40.0) | 45 |

Notes: Int. stands for Intersection. Only intersection capacity analysis results for critical movements are shown above.

Under Future (2038) Background Traffic conditions, the study area intersections are expected to operate at an acceptable overall Level of Service, although some turning movements are expected to experience high delays and/or begin to approach their theoretical capacity.
At the Colonel Talbot \& Pack intersection, the volume of traffic on the northbound through lane during the weekday afternoon peak hour is expected to approach the limit of a single lane, indicating that Colonel Talbot Road will likely require four-lane widening beyond 2038. A significant portion of the available green time is dedicated to the northbound through movement as a result of the heavy traffic demand, limiting the green time that can be allocated to the other turning movements. It is expected that increasing the northbound through capacity would allow additional green time to be allocated to other movements, thereby mitigating the capacity issues anticipated in 2038.

At the Colonel Talbot \& Clayton intersection, the continued increase in background traffic is expected to further increase traffic delays for eastbound left-turning traffic. As noted previously, it is expected that vehicles will seek alternative travel routes in order to avoid these high delays, although the City should consider measures to restrict left-turns from Clayton Walk.
The intersections of Colonel Talbot \& Diane/Royal Magnolia, Colonel Talbot \& Kilbourne and Main/Wharncliffe \& Campbell are all expected to operate at an acceptable Level of Service under Future (2038) Background Traffic conditions, assuming the required modifications previously identified as are in place. Some left-turn movements at the latter two intersections will begin to experience slightly high delays (i.e., LOS ' $E$ ') but as the intersections as a whole are operating well no mitigation measures are necessary.

The Bostwick \& Pack roundabout is expected to continue operating at an acceptable Level of Service (i.e., LOS 'D’ or better).

### 6.2.4 Future (2033) Total Traffic

The results of the intersection capacity analysis of Future (2033) Total Traffic conditions are presented in Table 14. To identify the direct impact of the subject development, the analysis assumes that the required mitigation measures from the Future (2033) Background Traffic conditions analysis are implemented, and that signal timing optimization will occur on a regular basis.

Table 14 - Intersection Capacity Analysis: Future (2033) Total Traffic

| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. <br> (s) <br> (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{aligned} & \text { 95TH } \\ & \text { PERCENTLLE } \\ & \text { QUEUE (m) } \end{aligned}$ |  |
| Colonel Talbot \& Pack (signalized) | $\begin{gathered} 21.7 \\ (43.7) \end{gathered}$ | C (D) | EBL | 53.9 (59.2) | D (E) | 0.38 (0.40) | 22.8 (26.5) | 55 |
|  |  |  | EBTR | 54.4 (62.0) | D (E) | 0.60 (0.68) | 40.3 (50.9) | - |
|  |  |  | WBL | 50.9 (81.7) | D (F) | 0.69 (0.98) | 54.4 (\#137.8) | 55 |
|  |  |  | NBT | 17.6 (57.1) | B (E) | 0.76 (1.00) | 193.4 (\#358.7) | - |
|  |  |  | SBL | 53.8 (87.5) | D (F) | 0.88 (0.97) | \#90.5 (\#80.6) | 120 |
| Colonel Talbot \& Clayton (unsignalized) | $\begin{gathered} 1312.6 \\ (1276.1) \end{gathered}$ | F (F) | EBL | 1312.6 (1276.1) | F (F) | 3.02 (2.51) | 55.3 (34.3) | 30 |
| Colonel Talbot \& Diane/Royal Magnolia (signalized) | $\begin{gathered} 19.6 \\ (36.0) \end{gathered}$ | B (D) | SBL | 15.5 (247.4) | B (F) | 0.41 (1.44) | 23.5 (\#88.7) | 75 |
| Colonel Talbot \& Diane/Royal Magnolia (signalized) ${ }^{1}$ | $\begin{gathered} 19.6 \\ (28.7) \end{gathered}$ | B (C) | WBTL | 23.2 (63.7) | C (E) | 0.30 (0.38) | 19.2 (19.9) | - |
|  |  |  | NBTR | 16.8 (34.5) | B (C) | 0.73 (0.95) | \#150.8 (\#391.8) | - |
|  |  |  | SBL | 15.5 (82.7) | B (F) | 0.41 (0.96) | 23.5 (\#100.0) | 75 |
| Colonel Talbot \& Kilbourne (signalized) | $\begin{gathered} 20.1 \\ (17.9) \end{gathered}$ | C (B) | - | - (-) | - (-) | - (-) | - (-) | - |
| Bostwick \& Pack (roundabout) | 9.3 (15.5) | A (C) | - | - (-) | -(-) | - (-) | - (-) | - |
| Main/Wharncliffe \& Campbell (signalized) | $\begin{gathered} 27.1 \\ (24.0) \end{gathered}$ | C (C) | EBL | 18.2 (30.9) | B (C) | 0.36 (0.64) | 18.5 (\#68.5) | 45 |
|  |  |  | NBL | 32.8 (41.6) | C (D) | 0.28 (0.33) | 20.8 (17.0) | 5 |
|  |  |  | SBL | 54.2 (59.9) | D (E) | 0.82 (0.72) | \#48.7 (41.3) | 45 |

Notes: Int. stands for Intersection. Only intersection capacity analysis results for critical movements are shown above.
${ }^{1}$ Added a protected-permitted southbound left-turn phase and increased cycle length to 130s in PM peak hour.

The addition of site-generated traffic to the Colonel Talbot \& Pack intersection is expected to result in a number of movements approaching their theoretical capacity during the weekday afternoon peak hour, despite the required modifications identified under Future (2033) Background Traffic conditions. This is similar to what was observed under Future (2038) Background Traffic conditions and can be attributed to a lack of through lane capacity in the northbound and southbound directions on Colonel Talbot Road. Although site-generated traffic will contribute between $12 \%$ to $13 \%$ of northbound and southbound through traffic at this intersection, the issue is largely due to background traffic demand and insufficient gaps to safely perform turning movements.

At the intersections of Colonel Talbot \& Clayton, Colonel Talbot \& Kilbourne and Main/Wharncliffe \& Campbell, the addition of sitegenerated traffic is not expected to have a significant impact on traffic operations relative to background traffic conditions. The Colonel Talbot \& Clayton intersection is expected to continue experiencing excessive delays on its eastbound approach due to heavy traffic in the north-south directions. As noted previously, it is expected that some drivers will choose alternate routes rather than attempt to turn left at this intersection. The assignment of site-generated traffic has already considered the excessive delays that westbound leftturning traffic would experience at this intersection and has therefore assigned the traffic to turn left at the Colonel Talbot \& Diane/Royal Magnolia intersection instead. Given the high delays that eastbound and westbound left-turning traffic is expected to experience at the Colonel Talbot \& Clayton intersection, the City should give consideration to implementing peak period eastbound and westbound leftturn restrictions at the intersection or physically restricting the side streets to right-in/right-out only.

During the weekday afternoon peak hour, the southbound left-turn movement at the Colonel Talbot \& Diane/Royal Magnolia intersection is expected to exceed its theoretical capacity. Providing a protected-permitted phase for this movement is expected to improve traffic operations but at the expense of the northbound through movement. As noted previously for the Colonel Talbot \& Pack intersection, these capacity issues can largely be attributed to a lack of north-south through lane capacity indicating that Colonel Talbot Road will require four-lane widening in the near future.

The Bostwick \& Pack roundabout is expected to continue operating at an acceptable Level of Service (i.e., LOS 'D' or better).

### 6.2.5 Future (2038) Total Traffic

The results of the intersection capacity analysis of Future (2038) Total Traffic conditions are presented in Table 15. The analysis assumes that the required mitigation measures from the Future (2033) Total Traffic and Future (2038) Background Traffic conditions analyses are implemented, and that signal timing optimization will occur on a regular basis.

Table 15 - Intersection Capacity Analysis: Future (2038) Total Traffic

| INTERSECTION | AM PEAK HOUR (PM PEAK HOUR) |  |  |  |  |  |  | PARALLEL LANE LENGTH (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INT. DELAY <br> (s) | $\begin{aligned} & \text { INT. } \\ & \text { LOS } \end{aligned}$ | LANE GROUP | DELAY (s) | LOS | V/C RATIO | $\begin{aligned} & \text { 95TH } \\ & \text { PERCENTLLE } \\ & \text { QUEUE (m) } \end{aligned}$ |  |
| Colonel Talbot \& Pack (signalized) | $\begin{gathered} 23.0 \\ (50.6) \end{gathered}$ | C (D) | EBL | 55.5 (59.5) | E (E) | 0.40 (0.41) | 24.2 (28.1) | 55 |
|  |  |  | EBTR | 57.1 (63.5) | $E$ (E) | 0.62 (0.70) | 43.4 (53.7) | - |
|  |  |  | WBL | 71.5 (106.1) | $E(F)$ | 0.84 (1.06) | \#66.4 (\#160.0) | 55 |
|  |  |  | WBR | 12.9 (23.3) | B (C) | 0.44 (0.64) | 22.7 (65.4) | 60 |
|  |  |  | NBT | 16.7 (66.3) | B (E) | 0.76 (1.03) | 199.4 (\#381.0) | - |
|  |  |  | SBL | 56.3 (104.1) | E (F) | 0.90 (1.03) | \#97.6 (\#87.3) | 120 |
| Colonel Talbot \& Clayton (unsignalized) | $\begin{gathered} 1610.5 \\ (1570.1) \end{gathered}$ | F (F) | EBL | 1610.5 (1570.1) | F (F) | 3.56 (2.97) | 57.4 (35.7) | 30 |
| Colonel Talbot \& Diane/Royal Magnolia (signalized) | $\begin{gathered} 22.2 \\ (33.7) \end{gathered}$ | C (C) | WBTL | 22.8 (63.7) | C (E) | 0.29 (0.38) | 19.2 (19.9) | - |
|  |  |  | NBTR | 18.9 (45.1) | B (D) | 0.77 (1.00) | \#165.9 (\#423.9) | - |
|  |  |  | SBL | 19.4 (82.7) | B (F) | 0.47 (0.96) | 27.1 (\#100.0) | 75 |
| Colonel Talbot \& Kilbourne (signalized) | $\begin{gathered} 22.3 \\ (18.4) \end{gathered}$ | C (B) | WBL | 53.8 (70.4) | D (E) | 0.83 (0.77) | \#66.3 (\#55.3) | - |
| Bostwick \& Pack (roundabout) | 9.8 (17.6) | A (C) | - | - (-) | - (-) | - (-) | - (-) | - |
| Main/Wharncliffe \& Campbell (signalized) | $\begin{gathered} 28.9 \\ (24.2) \end{gathered}$ | C (C) | EBL | 19.8 (43.0) | B (D) | 0.40 (0.77) | 19.7 (\#70.8) | 45 |
|  |  |  | WBL | 58.2 (24.5) | E (C) | 0.89 (0.59) | \#74.1 (39.9) | - |
|  |  |  | NBL | 32.8 (43.5) | C (D) | 0.28 (0.35) | 20.8 (17.7) | 5 |
|  |  |  | SBL | 71.6 (63.9) | E (E) | 0.90 (0.74) | \#53.2 (43.2) | 45 |

Notes: Int. stands for Intersection. Only intersection capacity analysis results for critical movements are shown above.
As shown above, the intersections of Colonel Talbot \& Pack and Colonel Talbot \& Diane/Royal Magnolia are both expected to operate at or above their theoretical capacity as a result of insufficient road capacity. The City should consider reviewing the need for additional
road network capacity in the area as the results of this study suggest that Colonel Talbot Road will not be sufficiently wide to accommodate the traffic demand associated with the development of the surrounding area.

The Colonel Talbot \& Clayton intersection is expected to continue operating with significant delays on the eastbound approach. As a result of these delays, it is expected that drivers will instead choose to turn left at alternate locations with lower delays (e.g., Colonel Talbot \& Diane/Royal Magnolia), however, without restriction of this movement, unsafe turning movements would still be possible.

Traffic operations at the intersections of Colonel Talbot \& Kilbourne and Main/Wharncliffe \& Campbell under Future (2038) Total Traffic conditions are largely the same as observed under background traffic conditions, indicating that site-generated traffic has a minimal impact on these intersections. Some left-turn movements at both intersection operate at LOS ' $E$ ' but as the intersections as a whole operate at an acceptable Level of Service (i.e., intersection LOS of 'D' or better) no mitigation measures are required.

The Bostwick \& Pack roundabout is expected to continue operating at an acceptable Level of Service (i.e., LOS ‘D’ or better).

### 6.2.6 Summary of Results

Overall, the results of the intersection capacity analysis indicates that all study area intersections, with the exception of the Bostwick \& Pack/Bradley roundabout, are expected to experience capacity issues under future background traffic conditions. Colonel Talbot Road in particular is expected to experience significant capacity issues due to heavy background traffic demand. The findings of the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) indicated that side street approaches would experience very high delays and key study area intersections would be operating at capacity by 2030. As such, the findings of this study are to be expected. These results suggest that Colonel Talbot Road will require four-lane widening in the future, although the City has not identified if or when this will occur. Until this widening is undertaken, it can be expected that significant congestion will occur along Colonel Talbot Road. Table 16 summarizes the interim mitigation measures required to address some of the capacity issues identified

Table 16 - Required Operational Improvements

| YEAR | REQUIRED OPERATIONAL IMPROVEMENTS |
| :--- | :--- |
| 2033 | Background Traffic <br> - Colonel Talbot \& Pack: Optimize the signal timing plan, add a protected- <br> permitted westbound left-turn phase in the weekday morning and afternoon peak <br> hour and add a northbound and westbound right-turn lane. Required in <br> approximately 5 years. <br> - Colonel Talbot \& Clayton Walk: Consider implementing peak period eastbound <br> and westbound left-turn prohibitions or physically restricting the side streets to <br> right-in/right-out only. Given the high traffic volumes on the main street, left-turn <br> movements from the sidestreets could be hazardous and would be subject to <br> significant delays. Required in approximately 5 years. <br> - Colonel Talbot \& Diane/Royal Magnolia: Signalize the intersection. Required <br> within 5 years and prior to first occupancy of the proposed development. <br> - Colonel Talbot \& Kilbourne: Optimize the signal timing plan on a regular basis. <br> - Main/Wharncliffe \& Campbell: Optimize the signal timing plan, add a protected- <br> permitted southbound and eastbound left-turn phase in the weekday morning and <br> afternoon peak hour, respectively, and add a westbound right-turn lane. Required <br> imminently. |
| Total Traffic |  |
| - Colonel Talbot \& Diane/Royal Magnolia: Add a protected-permitted southbound |  |
| left-turn phase in the weekday afternoon peak hour. Required within 5 years. |  |

As shown above, the majority of the above mitigation measures are required as a result of background traffic demand rather than site-generated traffic. The City should consider reviewing the need for the four-lane widening of Colonel Talbot Road given the significant capacity issues anticipated along this corridor.

### 6.3 Traffic Signal Warrants

Traffic signal warrant analysis was completed for both the Colonel Talbot \& Clayton intersection and Colonel Talbot \& Diane/Royal Magnolia intersection in accordance with the methodology outlined in Ontario Traffic Manual (OTM) Book 12: Traffic Signals. The results of the warrant
analysis are provided in Appendix F and indicate that neither intersection warrants signalization under Future (2038) Total Traffic conditions. Although not warranted, traffic signals are required at the Colonel Talbot \& Diane/Royal Magnolia intersection in order to ensure that Royal Magnolia Avenue can fulfill its role as a neighbourhood connector road and alleviate projected side street delays that do not meet acceptable operating conditions.

## 7 Geometric Analyses

### 7.1 Site Access Review

The Colonel Talbot \& Clayton Walk/Street ' N ' intersection is the proposed development's only direct access intersection to the existing public roadway network. All other access points to the subject site will be provided via internal connections to other adjacent developments. As such, only this intersection requires geometric review of sightlines and access spacing. The City of London Access Management Guidelines classify access intersections, such as the Street ' N ' access, as major access connections.

### 7.1.1 Sightlines

The Access Management Guidelines indicate that sightlines at a major access connection must meet the desirable decision sight distance requirements. For an assumed design speed of 70 $\mathrm{km} / \mathrm{h}$ (posted speed limit plus $10 \mathrm{~km} / \mathrm{h}$ ), the desirable decision sight distance is 275 m . Based on a desktop review of sightlines at the proposed access location, this sight distance requirement has been met.

### 7.1.2 Access Spacing

Colonel Talbot Road is classified as a Civic Boulevard (i.e., Urban Arterial) and, therefore, a minimum spacing of 150 m is required between adjacent full movement unsignalized access intersections. Additionally, 400 m of spacing is desirable between the Street ' N ' access and any adjacent signalized intersection, although 300 m of spacing is the minimum requirement.

The proposed Street ' N ' access is approximately 485 m south of Pack Road (signalized), 315 m north of Diane Crescent/Royal Magnolia Avenue (future signalized) and 260 m south of a potential future major access connection to the Hudson Park Subdivision (unsignalized). As such, the proposed access location meets the minimum spacing requirements outlined above. Furthermore, Street ' $N$ ' has been aligned with the existing Clayton Walk intersection.

### 7.2 Auxiliary Lane Analysis

The auxiliary lane analyses below have been completed in accordance with the City of London Access Management Guidelines and the Transportation Association of Canada (TAC) Geometric Design Guide for Canadian Roads.

### 7.2.1 Left-Turn Auxiliary Lane Analysis: Unsignalized Intersections

Auxiliary left-turn lane warrant analysis was completed for the Colonel Talbot \& Clayton intersection under Future (2038) Total Traffic conditions and the results are provided in Appendix G. The results of the analysis indicate that a southbound left-turn lane with 35 m of storage is warranted at the intersection. The northbound left-turn volume at this intersection is well below $5 \%$ and therefore does not meet the minimum threshold for a left-turn lane. As a southbound left-turn lane with 45 m of storage is already planned for this intersection as part of the urbanization of Colonel Talbot Road, no auxiliary lane extensions are required to accommodate the developmentgenerated demand.

### 7.2.2 Right-Turn Auxiliary Lane Analysis: Unsignalized Intersections

The Transportation Association of Canada (TAC) Geometric Design Guide for Canadian Roads indicates that auxiliary right-turn lanes should be considered at unsignalized intersections when "the volume of decelerating or accelerating vehicles compared with the through traffic volume causes undue hazard". The City of London Access Management Guidelines (April 2012) further
suggest that right-turn lanes be considered when right-turn volumes exceed 60 vehicles per hour and represent $10 \%$ to $20 \%$ of approaching traffic.
Northbound and southbound right-turn volumes at the Colonel Talbot \& Clayton intersection are expected to be relatively low ( 5 to 55 vehicles per hour) and represent a small proportion of approaching traffic ( $1 \%$ to $4 \%$ ). As such, it is not expected that auxiliary right-turn lanes will be required at this intersection.

### 7.2.3 Left-Turn Auxiliary Lane Analysis: Signalized Intersections

The auxiliary left-turn lane storage requirements for all left-turn movements at signalized intersections that site-generated traffic will contribute to are shown below in Table 17. The maximum $95^{\text {th }}$ percentile queue under Future (2038) Total Traffic conditions was compared with the existing or expected future storage lengths. Any deficiencies were identified, and additional storage recommendations were noted. The results do not consider taper length or deceleration requirements.

Table 17 - Auxiliary Left-Turn Lane Storage Requirements: Signalized Intersections

| INTERSECTION | MOVEMENT | PARALLEL <br> LANE LENGTH <br> $(\mathrm{m})$ | 95TH <br> PERCENTILE <br> QUEUE <br> (m) | DEFICIENCY <br> $(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: |
| Colonel Talbot <br> \& Pack | WBL | 55 | 160 | 105 |
| Colonel Talbot <br> \& Diane/Royal <br> Magnolia | SBL | 75 | 100 | 25 |
| Main/ <br>  <br> Campbell | SBL | 45 | 55 | $-{ }^{2}$ |
|  | EBL | 45 | 75 | -3 |

Notes:
${ }^{1}-95^{\text {th }}$ percentile queue lengths have been rounded up to nearest multiple of 5 m .
${ }^{2}$ - As this on a side street approach to the intersection, a small amount of queue spillback is not considered critical and therefore it is not recommended that the auxiliary lane be lengthened.
${ }^{3}$ - It is expected that the queue would spillback into the two-way left-turn lane rather than into the through lane and therefore would not impact through traffic on Main Street. As such, no auxiliary lane extension is recommended.

As illustrated above, additional auxiliary left-turn lane storage is required at two of the study area intersections. Consideration should be given to providing this additional storage when these intersections are reconstructed as part of the urbanization of Colonel Talbot Road.

### 7.2.4 Right-Turn Auxiliary Lane Analysis: Signalized Intersections

The City of London Access Management Guidelines indicate that auxiliary right-turn lanes should be considered when the volume of right-turning traffic represents between $10 \%$ and $20 \%$ of approaching traffic and exceeds 60 vehicles per hour during the peak hour. Table 18 summarizes the right-turn movements which meet the right-turn warrants. Only movements to which sitegenerated traffic will contribute to were evaluated.

Table 18 - Auxiliary Right-Turn Lane Storage Requirements

| INTERSECTION | MOVEMENT | RIGHT TURN WARRANTED? |  | PARALLEL LANE LENGTH (M) | 95TH \%ILE QUEUE ${ }^{1}$ <br> (M) | DEFICIENCY <br> (M) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FUTURE <br> (2038) <br> BACK GROUND TRAFFIC | FUTURE <br> (2038) <br> TOTAL <br> TRAFFIC |  |  |  |
| Colonel Talbot \& Pack | NBR | Yes |  | TBD ${ }^{2}$ | 40 | - |
| Colonel Talbot | NBR |  |  | - | - | - |
| \& Diane/Royal Magnolia | WBR | Yes |  | 60 | 50 | - |
| Main/ | SBR | Yes ${ }^{3}$ |  | - | - | - |
| Wharncliffe \& Campbell | WBR | Yes |  | TBD ${ }^{2}$ | 25 | - |

Notes:
${ }^{1}$ - Maximum $95^{\text {th }}$ percentile queue length under Future (2038) Total Traffic. Queue lengths have been rounded up to nearest multiple of 5m. Queue lengths are only reported for locations that currently have, or are proposed to have, auxiliary right-turn lanes.
${ }^{2}$ - These are proposed auxiliary right-turn lanes and therefore do not have an existing or planned parallel lane length.
${ }^{3}$ - Although warranted, an auxiliary southbound right-turn lane is not operationally required and therefore not recommended.

Based on the above, there are a number of locations that warrant a right-turn lane as a result of background traffic demand. The addition of site-generated traffic does not trigger the need for additional right-turn lanes.

At the Colonel Talbot \& Pack intersection, the results of the intersection capacity analysis suggest that a minimum of 40 m storage is required for the auxiliary northbound right-turn lane, however, insufficient property is currently available.

At the Main/Wharncliffe \& Campbell intersection, a minimum of 25 m of storage is required for the auxiliary westbound right-turn lane. This right-turn lane is required to provide additional capacity to the westbound approach. With this additional capacity, additional green time can be provided to the side street approaches which are expected to be nearing capacity (i.e., v/c ratio near 1.0) under Future (2033) Background Traffic conditions. There is the potential, however, that there may be insufficient property to implement this measure.

Note that the above measures are simply noted for future consideration by the City of London and are not required to accommodate the proposed development.

The westbound auxiliary right-turn lane at the Colonel Talbot \& Diane/Royal Magnolia intersection is expected to have sufficient storage to accommodate the projected demand.

## 8 Internal Transportation Network Review

The internal transportation network has been reviewed to ensure that sufficient transit, pedestrian and cycling facilities will be provided to support the target mode share distribution. Additionally, the need for traffic calming measures has been assessed to ensure that the potential for cutthrough traffic has been minimized to the greatest extent possible.

### 8.1 Royal Magnolia \& Campbell Intersection

Both Royal Magnolia Avenue and Campbell Street North are classified as Neighbourhood Connectors and therefore the intersection of these two streets is expected to experience a moderate volume of traffic. The presence of mixed-use residential/commercial land uses on the northeast and southeast corners of this intersection is expected to contribute additional vehicular and pedestrian demand by attracting local residents from the surrounding neighbourhoods. The traffic control at this intersection has therefore been reviewed to ensure that the intersection can accommodate the projected vehicular and pedestrian demand.
Figure 8 illustrates the projected vehicle and pedestrian demand at the intersection based on the anticipated trip generation of the commercial land uses adjacent to the intersection and through traffic generated by both the proposed development and the adjacent W3 Farms Residential Development.

Figure 8 - Future (2038) Total Traffic Volumes at Royal Magnolia \& Campbell Intersection


Ontario Traffic Manual (OTM) Book 5: Regulatory Signs indicates that all-way stop-control is warranted if a minimum of $30 \%$ of traffic at the intersection is from the minor street. Based on projected traffic volumes at this intersection, approximately $30 \%$ of total traffic at the intersection
during the weekday peak hours is expected to be from Campbell Street North and therefore the intersection warrants all-way stop-control.

Intersection capacity analysis was completed for this intersection and the results are shown below in Table 19. The intersection is expected to operate at an acceptable Level of Service (i.e., LOS ' $D$ ' or better) as an all-way stop-controlled intersection.

Table 19 - Intersection Capacity Analysis Results: Royal Magnolia \& Campbell Intersection

| INTERSECTION | TRAFFIC <br> CONTROL | PEAK <br> PERIOD | OVERALL LOS <br> (DELAY) | CRITICAL <br> MOVEMENT <br> (DELAY) |
| :---: | :---: | :---: | :---: | :---: |
|  <br> Campbell | Unsignalized | AM | $\mathrm{A}(8.2 \mathrm{~s})$ | WBTRL (8.2s) |
|  | PM | $\mathrm{A}(8.7 \mathrm{~s})$ | WBTRL (8.7s) |  |

### 8.2 Pedestrian and Cycling Facilities

Concrete sidewalks will be provided on both sides of all internal streets. A multi-use path (MUP) will bisect the proposed development and follow the creek, crossing Campbell Street North approximately 250 m north of Royal Magnolia Avenue. This crossing location is a potential candidate for implementation of a PXO and the results of the PXO warrant analysis are summarized in Section 8.3.

As previously discussed in Section 4.1, the Draft Colonel Talbot Road Two Lane Upgrade Traffic Analysis Memo (AECOM, April 2023) recommended the implementation of a mid-block pedestrian signal on Colonel Talbot Road approximately 120m north of Diane Crescent/Royal Magnolia Avenue to provide connectivity for the MUP network. Instead of providing mid-block pedestrian signals at this location, however, it is recommended that instead the MUP be realigned so that it crosses Colonel Talbot Road at its intersection with Diane Crescent and Royal Magnolia Avenue. This would eliminate the need for two closely spaced traffic signals on Colonel Talbot Road while still maintaining connectivity for active modes. The proposed realignment of the MUP network is illustrated in Exhibit 11.

As discussed previously in Section 4.2, a recent technical amendment to the Cycling Master Plan (CMP) indicates that both Campbell Street North and Street ' $R$ ' will require cycle facilities. OTM Book 18: Cycling Facilities provides a nomograph for selecting appropriate cycling facilities for a roadway based on the posted speed limit and average daily traffic (ADT) volumes.

Using equations from OTM Book 12, the future ADT volumes along Campbell Street North are estimated to range between 680 to 1,330 vehicles per day. Based on an assumed posted speed limit of $50 \mathrm{~km} / \mathrm{h}$, a dedicated cycling facility such as a bike lane is warranted along Campbell Street North. The speed limit and future ADT volumes on Street 'R' are expected to be lower than on Campbell Street North and therefore a shared street or neighbourhood bikeway is appropriate for this street.



W3 Sunset Creek
IBI GROUP

Exhibit 11:
Multi-Use Path Network

PROJECT No.
SCALE:

## 143384



### 8.3 Pedestrian Crossovers (PXOs)

There is one location within the proposed development that has been identified as a potential candidate for the implementation of a PXO:

- Campbell Street North, 250m North of Royal Magnolia Avenue: A PXO may be required at this location in order to provide system connectivity for the MUP network.

OTM Book 15: Pedestrian Crossing Treatments, Figure 2 illustrates the process for determining whether a PXO is warranted at a given location. Based on this warrant, a PXO is warranted on Campbell Street North due to the need for system connectivity and the lack of another signalcontrolled pedestrian crossing within 200 m .

OTM Book 15 provides further guidance on the selection of the appropriate PXO type for a location based on two-way traffic volumes and the posted speed limit. Based on equations from OTM Book 12 and OTM Book 15, 8-hour two-way traffic volumes can be estimated by taking the sum of the weekday morning and afternoon peak hour traffic volumes and multiplying it by two. Using the traffic volume projections outlined above in Figure 8, it can be estimated that future 8-hour twoway volumes on Campbell Street North at the crossing location will be approximately 340 vehicles. Assuming a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$ or less, a Level 2 Type D PXO is recommended on Campbell Street North. It is further recommended that curb extensions be implemented at the crossing to narrow the roadway width to 7.5 m or less. As PXOs are intended for pedestrians only, dismount and walk signs (Rb-70) should be installed to instruct cyclists to cross the street as a pedestrian.
Figure 9 illustrates the recommended PXO configuration.

Figure 9 - Recommended PXO on Campbell Street North, 250m North of Royal Magnolia Avenue


### 8.4 Transit Service and Facilities

As noted previously in Section 3.3, there is currently no transit service within walking distance of the proposed development. It is recommended that the City of London extend transit service along Colonel Talbot Road, Pack Road and Royal Magnolia Avenue in order to provide residents of the proposed development, and residents of adjacent developments, access to transit service and support the TMP's objective of encouraging more trips via transit. Transit stops should be provided at regular intervals along these routes in order to ensure that residents live within a short walking
distance of transit. Exhibit 12 identifies potential locations for transit stops in the vicinity of the proposed development.

### 8.5 Traffic Calming Measures

Given the short length of the majority of internal roadways, it is not expected that operating speeds will warrant the implementation of traffic calming measures. The exception is Campbell Street North which will ultimately extend to Pack Road and will be of sufficient length for higher operating speeds to occur. A conceptual traffic calming plan has therefore been developed for this street and is illustrated in Exhibit 12. It is recommended that curb extensions and a raised PXO be utilized to narrow the street at key locations and create vertical deflection to encourage lower operating speeds. In addition, the following curb radii are recommended to reduce high turning speeds and shorten pedestrian crossing distances while still accommodating heavy vehicles:

- As low as 5 m at local-local and local-collector road intersections
- No less than 9 m at collector-collector intersections or on arterial roads


W3 Sunset Creek
Transportation Impact Assessment

Exhibit 12:
Conceptual Traffic Calming \& Transit Plan

PROJECT No
SCALE:

## 143384



## 9 Conclusions and Recommendations

Based on the trip generation rates from the ITE Trip Generation Manual and the mode share data from the 2016 Household Travel Survey, it is expected that the proposed development will generate between 650 to 702 two-way person-trips during the weekday peak hours, of which 407 to 439 will be vehicle-trips. These vehicle-trips were distributed and assigned to the adjacent road network based on origin-destination data from the 2016 Household Travel Survey.
The results of the intersection capacity analysis indicate that the Colonel Talbot Road corridor is expected to experience significant congestion under background traffic conditions. Without fourlane widening, it is expected that the majority of study area intersections on Colonel Talbot Road will experience capacity issues at the horizon year of the study as a result of background traffic growth. The Main/Wharncliffe \& Campbell intersection is also expected to experience capacity issues. Only the Bostwick \& Pack roundabout is expected to operate at an acceptable Level of Service (i.e., LOS ‘D’ or better).

The following mitigation measures are recommended to be implemented to address background traffic capacity issues:

- Colonel Talbot \& Pack: Optimize the signal timing plan, add a protected-permitted westbound left-turn phase in the weekday morning and afternoon peak hour, and add a northbound and westbound right-turn lane with a minimum of 40 m and 70 m of storage, respectively. Required in approximately 5 years.
- Colonel Talbot \& Clayton/Street ' $\mathbf{N}$ ': Give consideration to implementing peak period eastbound and westbound left-turn prohibitions or restricting the side streets to right-in/right-out only. Given the high traffic volumes on the main street, left-turn movements from the sidestreets could be hazardous and would be subject to significant delays. Required in approximately 5 years.
- Colonel Talbot \& Diane/Royal Magnolia: Signalize the intersection and provide combined bicycle/pedestrian crossing facilities on the north leg. Required within 5 years and prior to first occupancy of the proposed development.
- Colonel Talbot \& Kilbourne: Optimize the signal timing plan on a regular basis.
- Main/Wharncliffe \& Campbell: Optimize the signal timing plan, add a protectedpermitted southbound and eastbound left-turn phase in the weekday morning and afternoon peak hour, respectively, and add a westbound right-turn lane with a minimum of 25 m of storage. Required imminently.

In addition to the above mitigation measures, the following is also recommended to be implemented prior to 2033 in order to accommodate site-generated traffic:

- Colonel Talbot \& Pack: Extend the westbound left-turn lane to provide a minimum of 160m of storage. Required in approximately 5 years.
- Colonel Talbot \& Diane/Royal Magnolia: Add a protected-permitted southbound leftturn phase in the weekday afternoon peak hour (assuming the intersection is signalized) and ensure that a minimum of 100 m of storage is provided for the southbound left-turn movement when this intersection is constructed. Required within 5 years and prior to first occupancy of the proposed development.
Based on projected traffic volumes at the Royal Magnolia \& Campbell intersection, all-way stopcontrol is warranted, and intersection capacity analysis results suggest that this intersection would operate at an acceptable Level of Service (i.e., LOS 'D' or better) in this configuration.

Given the capacity issues projected within the study area as a result of Colonel Talbot Road exceeding its theoretical capacity as a two-lane road, it is recommended that the City of London review roadway network capacity needs in the area as it is expected that this road will require fourlane widening within the timeframe of this study.
The review of the proposed Colonel Talbot \& Street ' $N$ ' intersection has confirmed that the intersection complies with the sightline and access spacing requirements outlined in the Access Management Guidelines.

The internal transportation network was analyzed to ensure that sufficient facilities will be provided to support the pedestrian, cycling and transit mode share of the proposed development.

Bicycle lanes are recommended on Campbell Street North to support this street's role as a cycle route. Although Street ' $R$ ' is also expected to be part of a cycle route, no dedicated facilities are expected to be required due to the low speed and traffic volume projected on this roadway.
To ensure a continuous multi-use path (MUP) network through the proposed development, a Level 2 Type D pedestrian crossover (PXO) is recommended where the MUP crosses Campbell Street North. It is also recommended that the MUP network be realigned to cross Colonel Talbot Road at its intersection with Diane Crescent/Royal Magnolia Avenue, rather than 120 m to the north.

Within the proposed development, only Campbell Street North is expected to be sufficiently long to warrant traffic calming measures. In order to encourage appropriate operating speeds, curb extensions and a raised crosswalk for the PXO are recommended.

To minimize the vehicular impact on the surrounding road network, it is recommended that transit service be extended to the area with bus stops on Colonel Talbot Road, Pack Road and Royal Magnolia Avenue to ensure future residents have access to public transportation as an alternative mode of travel.

The overall conclusion of this TIA is that traffic generated by the proposed W3 Sunset Creek subdivision can be safely accommodated on the adjacent road network with consideration of the mitigation measures identified above. It is recommended that the City of London review the need for capital improvements in the area to ensure that sufficient roadway capacity is provided to accommodate projected growth.

## 10 Professional Authorization



Eric McLaren, P.Eng.


David Hook, P.Eng.

## Appendix A - Transit Service Maps



Map Legend
Effective: September 3, 2023
(A) Timepoint $\quad$ 單 Shopping Centre $\rightarrow$ Route Direction
(H) Hospital

ROUTE 24 - MONDAY TO FRIDAY

| WESTBOUND |  |  |  |  |  |  | EASTBOUND |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A | B | B | C | D | E | E |  | E | E | D | ) | B | B | A |
| LVS | ARR | LVS |  |  | ARR | LVS |  | ARR | LVS |  |  | ARR | LVS | ARR |
| - | - |  |  |  |  |  |  |  |  |  |  |  |  | 5:58 |
| - | - | - | - | - |  |  | 6:03 | 6:10 | 6:13 | 6:20 | 6:28 | 6:36 | 6:38 | 6:43 |
| 5:58 | 6:05 | 6:06 | 6:12 | 6:19 | 6:27 | 6:37 | 6:48 | 6:55 | 6:58 | 7:05 | 7:13 | 7:21 | 7:23 | 7:28 |
| 6:43 | 6:50 | 6:51 | 6:57 | 7:04 | 7:12 | 7:22 | 7:33 | 7:40 | 7:41 | 7:50 | 7:58 | 8:05 | 8:07 | 8:12 |
| 7:28 | 7:36 | 7:37 | 7:44 | 7:52 | 8:01 | 8:08 | 8:19 | 8:26 | 8:27 | 8:36 | 8:44 | 8:51 | 8:53 | 8:58 |
| 8:12 | 8:20 | 8:21 | 8:28 | 8:36 | 8:45 | 8:52 | 9:03 | 9:09 | 9:12 | 9:19 | 9:27 | 9:35 | 9:37 | 9:42 |
| 8:58 | 9:06 | 9:07 | 9:14 | 9:22 | 9:31 | 9:38 | 9:49 | 9:55 | 9:58 | 10:05 | 10:13 | 10:21 | 10:23 | 10:28 |
| 9:42 | 9:49 | 9:51 | 9:57 | 10:05 | 10:13 | 10:23 | 10:33 | 10:39 | 10:42 | 10:49 | 10:57 | 11:05 | 11:07 | 11:12 |
| 10:28 | 10:35 | 10:37 | 10:43 | 10:51 | 10:59 | 11:09 | 11:19 | 11:25 | 11:28 | 11:35 | 11:43 | 11:51 | 11:53 | 11:58 |
| 11:12 | 11:19 | 11:21 | 11:27 | 11:35 | 11:43 | 11:53 | 12:03 | 12:09 | 12:12 | 12:19 | 12:27 | 12:34 | 12:37 | 12:42 |
| 11:58 | 12:05 | 12:07 | 12:13 | 12:21 | 12:29 | 12:39 | 12:49 | 12:55 | 12:58 | 1:05 | 1:13 | 1:20 | 1:23 | 1:28 |
| 12:42 | 12:49 | 12:50 | 12:57 | 1:05 | 1:13 | 1:23 | 1:33 | 1:39 | 1:42 | 1:49 | 1:57 | 2:04 | 2:07 | 2:12 |
| 1:28 | 1:35 | 1:36 | 1:43 | 1:51 | 1:59 | 2:09 | 2:19 | 2:25 | 2:25 | 2:33 | 2:43 | 2:51 | 2:52 | 2:57 |
| 2:12 | 2:20 | 2:20 | 2:28 | 2:40 | 2:49 | 2:53 | 3:04 | 3:10 | 3:10 | 3:18 | 3:28 | 3:36 | 3:37 | 3:42 |
| 2:57 | 3:05 | 3:05 | 3:13 | 3:25 | 3:34 | 3:38 | 3:49 | 3:55 | 3:55 | 4:03 | 4:13 | 4:21 | 4:22 | 4:27 |
| 3:42 | 3:50 | 3:50 | 3:58 | 4:10 | 4:19 | 4:23 | 4:34 | 4:41 | 4:42 | 4:50 | 4:59 | 5:06 | 5:08 | 5:12 |
| 4:27 | 4:35 | 4:36 | 4:45 | 5:00 | 5:09 | 5:18 | 5:29 | 5:36 | 5:37 | 5:45 | 5:54 | 6:01 | 6:03 | 6:07 |
| 5:12 | 5:20 | 5:21 | 5:30 | 5:45 | 5:54 | 6:03 | 6:14 | 6:21 | 6:24 | 6:30 | 6:37 | 6:44 | 6:46 | 6:51 |
| 6:07 | 6:17 | 6:19 | 6:25 | 6:33 | 6:40 | 6:50 | 7:00 | 7:07 | 7:10 | 7:16 | 7:23 | 7:30 | 7:32 | 7:37 |
| 6:51 | 7:01 | 7:03 | 7:09 | 7:17 | 7:24 | 7:34 | 7:44 | 7:51 | 7:54 | 8:00 | 8:07 | 8:14 | 8:16 | 8:21 |
| 7:37 | 7:47 | 7:49 | 7:55 | 8:03 | 8:10 | 8:20 | 8:30 | 8:37 | 8:40 | 8:46 | 8:53 | 9:00 | 9:02 | 9:07 |
| 8:21* |  |  |  |  |  |  | To G | arage |  |  |  |  |  |  |
| 9:07* |  |  |  |  |  |  | To | age |  |  |  |  |  |  |

## LEGEND

| * | Bus into Garage | + | Route Change |
| :---: | :--- | :---: | :--- |
| 5:58 | Bus goes into service at Commissioners and Meadowlilly 2min earlier |  |  |
| 6:03 | Bus goes into service at Tillman and Southdale 3min earlier |  |  |

ROUTE 24 - SATURDAY

| WESTBOUND |  |  |  |  |  |  | EASTBOUND |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\left\lvert\, \begin{aligned} & \\ & \hline \end{aligned}\right.$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A | B | B | C | D | 란 | E | F) | 를 | E | D | C | B | $B$ | A |
| LVS | ARR | LVS |  |  | ARR | LVS |  | ARR | LVS |  |  | ARR | LVS | ARR |
| - | - |  |  |  |  |  |  |  |  |  |  |  |  | 6:37 |
| - | - | 6:15 | 6:21 | 6:28 | 6:35 | 6:35 | 6:42 | 6:47 | 6:51 | 6:57 | 7:04 | 7:13 | 7:13 | 7:17 |
| 6:37 | 6:43 | 6:48 | 6:53 | 7:00 | 7:06 | 7:13 | 7:22 | 7:27 | 7:31 | 7:37 | 7:44 | 7:53 | 7:53 | 7:57 |
| 7:17 | 7:23 | 7:28 | 7:33 | 7:40 | 7:46 | 7:53 | 8:02 | 8:07 | 8:11 | 8:17 | 8:24 | 8:33 | 8:33 | 8:37 |
| 7:57 | 8:03 | 8:08 | 8:13 | 8:20 | 8:26 | 8:33 | 8:42 | 8:47 | 8:51 | 8:57 | 9:04 | 9:13 | 9:13 | 9:17 |
| 8:37 | 8:43 | 8:48 | 8:53 | 9:00 | 9:06 | 9:13 | 9:22 | 9:27 | 9:31 | 9:37 | 9:44 | 9:53 | 9:53 | 9:57 |
| 9:17 | 9:23 | 9:28 | 9:33 | 9:40 | 9:46 | 9:53 | 10:02 | 10:08 | 10:11 | 10:18 | 10:25 | 10:32 | 10:32 | 10:37 |
| 9:57 | 10:03 | 10:08 | 10:13 | 10:20 | 10:26 | 10:33 | 10:42 | 10:48 | 10:49 | 10:56 | 11:03 | 11:10 | 11:10 | 11:15 |
| 10:37 | 10:44 | 10:48 | 10:54 | 11:01 | 11:08 | 11:13 | 11:24 | 11:30 | 11:31 | 11:38 | 11:45 | 11:52 | 11:52 | 11:57 |
| 11:15 | 11:22 | 11:25 | 11:31 | 11:38 | 11:45 | 11:49 | 12:00 | 12:06 | 12:06 | 12:13 | 12:22 | 12:30 | 12:30 | 12:35 |
| 11:57 | 12:04 | 12:08 | 12:14 | 12:21 | 12:28 | 12:33 | 12:44 | 12:50 | 12:50 | 12:57 | 1:06 | 1:14 | 1:15 | 1:20 |
| 12:35 | 12:42 | 12:47 | 12:52 | 1:00 | 1:09 | 1:20 | 1:30 | 1:36 | 1:36 | 1:43 | 1:52 | 2:00 | 2:00 | 2:05 |
| 1:20 | 1:27 | 1:32 | 1:37 | 1:45 | 1:54 | 2:05 | 2:15 | 2:21 | 2:23 | 2:30 | 2:37 | 2:44 | 2:44 | 2:49 |
| 2:05 | 2:13 | 2:18 | 2:23 | 2:30 | 2:38 | 2:50 | 3:00 | 3:06 | 3:08 | 3:15 | 3:22 | 3:29 | 3:30 | 3:35 |
| 2:49 | 2:57 | 3:02 | 3:07 | 3:14 | 3:22 | 3:34 | 3:44 | 3:50 | 3:52 | 3:59 | 4:06 | 4:13 | 4:14 | 4:19 |
| 3:35 | 3:43 | 3:48 | 3:53 | 4:00 | 4:08 | 4:20 | 4:30 | 4:36 | 4:38 | 4:45 | 4:52 | 4:59 | 5:00 | 5:05 |
| 4:19 | 4:27 | 4:32 | 4:37 | 4:44 | 4:52 | 5:04 | 5:14 | 5:20 | 5:22 | 5:29 | 5:36 | 5:43 | 5:44 | 5:49 |
| 5:05 | 5:13 | 5:18 | 5:23 | 5:30 | 5:38 | 5:44 | 5:54 | 6:00 | 6:02 | 6:09 | 6:16 | 6:23 | 6:24 | 6:29 |
| 5:49 | 5:57 | 6:02 | 6:07 | 6:14 | 6:22 | 6:28 | 6:38 | 6:44 | 6:46 | 6:53 | 7:00 | 7:07 | 7:08 | 7:13 |
| 6:29 | 6:37 | 6:42 | 6:47 | 6:54 | 7:02 | 7:08 | 7:18 | 7:24 | 7:26 | 7:33 | 7:40 | 7:47 | 7:48 | 7:53 |
| 7:13 | 7:21 | 7:26 | 7:31 | 7:38 | 7:46 | 7:52 | 8:02 | 8:08 | 8:11 | 8:18 | 8:25 | 8:32* | To Ga | Grage |
| 7:53 | 8:01 | 8:06 | 8:11 | 8:18 | 8:26 | 8:32* |  |  |  | To | rage |  |  |  |

ROUTE 24 - SUNDAY / HOLIDAY

| WESTBOUND |  |  |  |  |  |  | EASTBOUND |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| A | B | B | C | (D) | E |  | F | E | E | (D) | C | B | B | A |
| LVS | ARR | LVS |  |  | ARR | LVS |  | ARR | LVS |  |  | ARR | LVS | ARR |
| - | - | - | - | - | - | - | - | - | - | - | - | - | - | 10:02 |
| - | - | 9:38 | 9:44 | 9:51 | 9:58 | 10:00 | 10:07 | 10:13 | 10:13 | 10:20 | 10:27 | 10:35 | 10:38 | 10:42 |
| 10:02 | 10:09 | 10:09 | 10:14 | 10:21 | 10:28 | 10:35 | 10:47 | 10:53 | 10:53 | 11:00 | 11:07 | 11:15 | 11:18 | 11:22 |
| 10:42 | 10:49 | 10:49 | 10:54 | 11:01 | 11:08 | 11:15 | 11:27 | 11:33 | 11:33 | 11:40 | 11:47 | 11:55 | 11:58 | 12:02 |
| 11:22 | 11:29 | 11:29 | 11:34 | 11:41 | 11:48 | 11:55 | 12:07 | 12:13 | 12:13 | 12:19 | 12:26 | 12:34 | 12:37 | 12:41 |
| 12:02 | 12:09 | 12:09 | 12:15 | 12:23 | 12:31 | 12:38 | 12:48 | 12:54 | 12:54 | 1:00 | 1:07 | 1:15 | 1:18 | 1:22 |
| 12:41 | 12:48 | 12:48 | 12:54 | 1:02 | 1:10 | 1:17 | 1:27 | 1:33 | 1:33 | 1:39 | 1:46 | 1:54 | 1:57 | 2:01 |
| 1:22 | 1:29 | 1:29 | 1:35 | 1:43 | 1:51 | 1:58 | 2:08 | 2:14 | 2:14 | 2:20 | 2:27 | 2:35 | 2:38 | 2:42 |
| 2:01 | 2:08 | 2:08 | 2:14 | 2:22 | 2:30 | 2:37 | 2:47 | 2:53 | 2:53 | 2:59 | 3:06 | 3:14 | 3:17 | 3:21 |
| 2:42 | 2:49 | 2:49 | 2:55 | 3:03 | 3:11 | 3:18 | 3:28 | 3:34 | 3:34 | 3:40 | 3:47 | 3:55 | 3:58 | 4:02 |
| 3:21 | 3:28 | 3:28 | 3:34 | 3:42 | 3:50 | 3:57 | 4:07 | 4:13 | 4:13 | 4:19 | 4:26 | 4:34 | 4:37 | 4:41 |
| 4:02 | 4:09 | 4:09 | 4:15 | 4:23 | 4:31 | 4:38 | 4:48 | 4:54 | 4:54 | 5:00 | 5:07 | 5:15 | 5:18 | 5:22 |
| 4:41 | 4:48 | 4:48 | 4:54 | 5:02 | 5:10 | 5:17 | 5:27 | 5:32 | 5:32 | 5:38 | 5:45 | 5:53* | To G | arage |
| 5:22* |  |  |  |  |  |  | To G | arage |  |  |  |  |  |  |

## LEGEND

| $*$ | Bus into Garage | $\boldsymbol{+}$ | Route Change |
| :---: | :--- | :---: | :--- |
| $\mathbf{0 : 0 0}$ | Bus goes into service at Commissioners and Meadowlilly 2min earlier |  |  |

## 0 O WHITE OAKS MALLLAMBETH



## $\int 0$ WHITE OAKS MALLLAMBETH



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SOUTHBOUND


## LEGEND

| $\boldsymbol{+}$ | Route Change | * |
| :---: | :--- | :---: |
| $\mathbf{0 : 0 0}$ | Bus goes into service at White Oak and Bradley 6 minutes earlier | Bus into Garage |

## SERVICE NOTE:

Route 28 operates on a modified weekday peak period service only from 6:30AM - 10:30AM and 2:30PM - 7:00PM.

## Appendix B - Collision Data

Collision Details Report
From: January 1, 2015 To: May 16, 2023

| Location .......... BOSTWICK RD @ PACK RD |  |  |  |  |  | Municipality....... LONDON |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Control.... Stop sign |  |  |  |  |  | Total Collisions.... 16 |  |  |  |  |
| Collision ID | Date/Day/Time | Environment | Impact Type | Classification Direction | Surface Cond'n | Vehicle Manoeuver | Vehicle type | First Event | Driver Action | No. Ped |
| 15-76081 | 2015-Jul-15, Wed, 16:57 | Clear | Turning movement | Non-fatal injury North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Improper lane change |  |
| Comments: |  |  |  | South | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 16-24227s | 2016-Mar-10, Thu,07:10 | Rain | Rear end | Non-reportable East | Wet | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Other |  |
| Comments: |  |  |  | East | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 16-113727s | 2016-Oct-25, Tue, 16:30 | Clear | Angle | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  | East | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |  |
| $17300$ | 2016-Dec-31, Sat, 19:00 | Clear | SMV other | P.D. only South | Dry | Going ahead | Automobile, station wagon | Animal - wild | Driving properly |  |
| Comments: 48: Deer |  |  |  |  |  |  |  |  |  |  |
| 17-855922s | 2017-Dec-24, Sun,19:20 | Snow | Angle | Non-reportable South | Packed snow | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  | East | Packed snow | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 18-854747s | 2018-Jun-19, Tue,08:05 | Clear | Turning movement | Non-reportable South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  | North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 18-855163s | 2018-Jul-05, Thu,07:30 | Clear | Rear end | Non-reportable East | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 19-851639s | 2019-Feb-17, Sun,00:00 | Snow | Angle | Non-reportable East | Packed snow | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  | North | Packed snow | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 19-61729 | 2019-Jun-27, Thu,14:27 | Clear | Turning movement | Non-fatal injury North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |  |
| Comments: |  |  |  | South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |



| 15-117090s | 2015-Oct-28, Wed,14:45 | Rain | Angle | Non-reportable West | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  | South | Wet | Stopped | Pick-up truck | Other motor vehicle | Driving properly |
| 15-124520s | 2015-Nov-16, Mon,13:20 | Clear | Sideswipe | Non-reportable North | Dry | Changing lanes | Automobile, station wagon | Other motor vehicle | Improper lane change |
| Comments: |  |  |  | North |  | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-14351 | 2016-Feb-10, Wed, 16:55 | Clear | Angle | Non-fatal injury East | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Disobeyed traffic control |
| Comments: |  |  |  | South | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-68094s | 2016-Jul-02, Sat, 11:30 | Clear | Angle | Non-reportable West | Dry | Turning right | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-83316s | 2016-Aug-08, Mon,15:50 | Clear | Rear end | Non-reportable West | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Dry | Slowing or stopping | Delivery van | Other motor vehicle | Driving properly |
| 16-97445 | 2016-Sep-13, Tue, 13:30 | Clear | Rear end | P.D. only East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Following too close |
| Comments: |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-121543s | 2016-Nov-15, Tue,16:45 | Clear | Sideswipe | Non-reportable West | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West |  | Turning left | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |
| 17-34383s | 2017-Apr-06, Thu,17:30 | Rain | Turning movement | Non-reportable East | Wet | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 17-850034s | 2017-May-02, Tue,10:45 | Rain | Angle | Non-reportable West | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | South | Wet | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| 17-850105s | 2017-May-04, Thu,16:15 | Rain | Rear end | Non-reportable West | Wet | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 17-855242s | 2017-Dec-06, Wed, 17:10 | Clear | Rear end | Non-reportable East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |


| 18-3232 | 2018-Jan-04, Thu,17:15 | Snow | Sideswipe | P.D. only | East | Packed snow | Changing lanes | Pick-up truck | Other motor vehicle |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  |  | East | Packed snow | Going ahead | Tow truck | Other motor vehicle | Driving properly |
| 19-850784s | 2019-Jan-25, Fri,00:00 | Clear | Rear end | Non-repo | South | Ice | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  |  | South | Wet |  |  |  |  |
| 1921434 | 2019-Mar-08, Fri,09:24 | Clear | Other | Non-fata | West | Dry | Going ahead | Automobile, station wagon | Pole (utility, power) | Lost control |
| Comments: |  |  |  |  | East | Dry | Going ahead | Truck - dump | Pole (utility, power) | Driving properly |
| 19-853211s | 2019-Apr-13, Sat,00:00 | Clear | Rear end | Non-repo | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  |  | East |  | Stopped | Passenger van | Other motor vehicle | Driving properly |
| 20-850135s | 2020-Jan-06, Mon,11:00 | Clear | Rear end | Non-rep | North | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Following too close |
| 20857176 | 2020-Dec-09, Wed, 16:30 | Clear | Approaching | P.D. only | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | West | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |
| 21856101 | 2021-Nov-07, Sun,18:00 | Clear | Rear end | P.D. only | North | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  |  | North | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |
| 21857553 | 2021-Dec-23, Thu,22:15 | Snow | Angle | P.D. only | North | Loose snow | Turning right | Automobile, station wagon | Other motor vehicle | Speed too fast for condition |
| Comments: |  |  |  |  | West | Loose snow | Stopped | Passenger van | Other motor vehicle | Driving properly |
| 22853660 | 2022-May-17, Tue,15:00 | Clear | Rear end | Non-repo | West | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | West | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle |  |
| 22854786 | 2022-Jun-29, Wed, 17:45 | Clear | Sideswipe | P.D. only | North | Dry | Changing lanes | Automobile, station wagon | Other motor vehicle | Improper lane change |
| Comments: |  |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22857252 | 2022-Sep-29, Thu, 19:20 | Clear | Rear end | P.D. only | West | Dry | Going ahead | Automobile, station wagon | Other motor vehicle |  |
| Comments: |  |  |  |  | West | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |



| 16-58101s | 2016-Jun-08, Wed, 16:50 | Clear | Rear end | Non-reportable North | Dry | Stopped | Automobile, | Other motor | Driving properly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  | North | Dry |  |  |  |  |
| 16-62232s | 2016-Jun-18, Sat, 14:00 | Clear | Rear end | Non-reportable East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | East | Dry | Slowing or stopping | Pick-up truck | Other motor vehicle | Following too close |
| 16-66986 | 2016-Jun-29, Wed, 21:52 | Clear | SMV other | P.D. only West | Dry | Going ahead | Pick-up truck | Animal - wild | Driving properly |
| Comments: Deer |  |  |  |  |  |  |  |  |  |
| 16-67415s | 2016-Jun-30, Thu,19:20 | Clear | Turning movement | Non-reportable West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-87619 | 2016-Aug-19, Fri, 19:23 | Clear | SMV other | Non-fatal injury West | Dry | Going ahead | Automobile, station wagon | Ran off road | Other |
| Comments: |  |  |  |  |  |  |  |  |  |
| 16-91259 | 2016-Aug-29, Mon, 12:30 | Clear | Angle | Non-fatal injury North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  | West | Dry | Stopped | Pick-up truck | Other motor vehicle | Driving properly |
| 16-109983s | 2016-Oct-15, Sat,16:15 | Clear | Rear end | Non-reportable West | Dry | Slowing or stopping | Pick-up truck | Other motor vehicle |  |
| Comments: |  |  |  | West | Dry | Other | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-116887s | 2016-Nov-02, Wed, 17:30 | Rain | Angle | Non-reportable North | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Wet | Turning left | Passenger van | Other motor vehicle |  |
| 16-120124s | 2016-Nov-10, Thu,18:00 | Clear | Turning movement | Non-reportable East | Dry | Turning right | Pick-up truck | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| 17-852359s | 2017-Aug-19, Sat,12:38 | Clear | Rear end | Non-reportable North | Dry | Stopped | Passenger van | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry |  |  |  |  |
| 17-103596 | 2017-Oct-06, Fri, 15:15 | Clear | Angle | Non-fatal injury North | Dry | Going ahead | Pick-up truck | Other motor vehicle | Driving properly |
| Comments: |  |  |  | East | Dry | Going ahead | Bicycle | Cyclist | Other |
| 17-854504s | 2017-Nov-10, Fri, 11:00 | Clear | Other | Non-reportable North | Dry | Reversing | Truck-other | Other motor vehicle | Driving properly |
| Comments: |  |  |  | South | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |


| 17-855016s | 2017-Nov-28, Tue,21:10 | Clear | Turning movement | Non-reportable South | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  | North | Dry | Going ahead | Pick-up truck | Other motor vehicle | Driving properly |
| 18-850123s | 2018-Jan-05, Fri,09:30 | Other | Sideswipe | Non-reportable North | Slush | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Slush |  |  |  |  |
| 18-852332s | 2018-Mar-09, Fri, 17:00 | Clear | Turning movement | Non-reportable South | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 18-853080s | 2018-Apr-12, Thu,10:00 | Clear | Rear end | Non-reportable East | Wet | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Following too close |
| Comments: |  |  |  | East | Wet | Stopped | Passenger van | Other motor vehicle | Driving properly |
| 18-853321s | 2018-Apr-21, Sat, 16:45 | Clear | Sideswipe | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry | Changing lanes | Automobile, station wagon | Other motor vehicle | Improper lane change |
| 18-60138 | 2018-Jun-11, Mon,23:57 | Clear | SMV other | P.D. only East | Dry | Going ahead | Pick-up truck | Ran off road | Wrong way on one-way road |
| Comments: |  |  |  |  |  |  |  |  |  |
| 18-93193 | 2018-Aug-31, Fri, 14:00 | Clear | Rear end | P.D. only West | Dry |  | Automobile, station wagon | Other motor vehicle | Following too close |
| Comments: |  |  |  | West | Dry | Going ahead | Delivery van | Other motor vehicle | Driving properly |
| 18-859255s | 2018-Nov-26, Mon,14:00 | Rain | Angle | Non-reportable North | Wet | Turning left | Pick-up truck | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Wet |  |  |  |  |
| 19-852335s | 2019-Mar-11, Mon,00:00 | Clear | Turning movement | Non-reportable East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| 19852335 | 2019-Mar-11, Mon,20:40 | Clear | Turning movement | P.D. only West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 19-854506s | 2019-May-31, Fri,00:00 | Clear | Sideswipe | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North |  |  |  |  |  |
| 19-856999s | 2019-Sep-01, Sun,00:00 | Rain | Rear end | Non-reportable North | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |




| 22851353 | 2022-Feb-18, Fri,22:00 | Clear | Rear end | P.D. only | North | Dry | Going ahead | Passenger van | Other motor vehicle | Driving properly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  |  | North | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22852145 | 2022-Mar-13, Sun, 20:25 | Clear | SMV other | Non-reportable | South | Slush | Going ahead | Truck - tractor | Pole (utility, power) | Driving properly |
| Comments: |  |  |  |  |  | Slush |  |  |  |  |
| 22854047 | 2022-Jun-02, Thu,15:00 | Clear | Sideswipe | P.D. only | North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | North | Dry | Turning left | Pick-up truck | Other motor vehicle | Driving properly |
| 22854217 | 2022-Jun-08, Wed, 22:50 | Clear | Rear end | Non-reportable | South | Dry | Stopped | Delivery van | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | South | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle |  |
| 22854791 | 2022-Jun-29, Wed, 14:00 | Rain | Rear end | P.D. only | South | Wet | Going ahead | Truck - open | Other motor vehicle | Disobeyed traffic control |
| Comments: |  |  |  |  | South | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22855457 | 2022-Jul-25, Mon,21:15 | Clear | Rear end | Non-reportable | South | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle |  |
| 22855632 | 2022-Aug-03, Wed,21:00 | Clear | Rear end | P.D. only | East | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Other |
| 2281888 | 2022-Aug-30, Tue,03:41 | Clear | Angle | P.D. only | East | Wet | Turning right | Automobile, station wagon | Other motor vehicle | Other |
| Comments: | Charged Driver \#1 on pa | age 1: | 14 (A) (NA) |  | North | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22856906 | 2022-Sep-20, Tue,20:30 | Clear | Sideswipe | P.D. only | West | Dry | Turning left | Pick-up truck | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22857488 | 2022-Oct-07, Fri,23:20 | Clear | Sideswipe | P.D. only | North | Dry | Changing lanes | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 22105868 | 2022-Nov-04, Fri, 15:15 | Clear | SMV other | Non-fatal injury | North | Dry | Going ahead | Automobile, station wagon | Other | Driving properly |
| Comments: 48: Other |  |  |  |  |  | Dry |  |  |  |  |
| 22858449 | 2022-Nov-08, Tue,23:30 | Clear | Rear end | P.D. only | East | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Following too close |
| Comments: |  |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |



| 18-855759s | 2018-Jul-28, Sat, 15:52 | Clear | Angle | Non-reportable South | Dry | Going ahead | Pick-up truck | Other motor vehicle | Driving properly |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  | West | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 18-99085 | 2018-Sep-14, Fri, 10:31 | Clear | Angle | Non-fatal injury West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |
| Comments: |  |  |  | South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 18-857727s | 2018-Oct-13, Sat, 15:15 | Clear | Rear end | Non-reportable West | Dry | Stopped | Pick-up truck | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Dry | Going ahead | Passenger van | Other motor vehicle | Driving properly |
| 18-857742s | 2018-Oct-14, Sun, 14:55 | Clear | Angle | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | East | Dry | Stopped | Pick-up truck | Other motor vehicle | Driving properly |
| 19-851528s | 2019-Feb-13, Wed,00:00 | Snow | Rear end | Non-reportable South | Slush | Slowing or stopping | Passenger van | Other motor vehicle | Driving properly |
| Comments: |  |  |  | South | Slush | Slowing or stopping | Pick-up truck | Other motor vehicle | Driving properly |
| 19-852062s | 2019-Mar-01, Fri,00:00 | Clear | Sideswipe | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |
| 20-850794s | 2020-Jan-23, Thu,07:05 | Clear | Angle | Non-reportable West | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 20-851188s | 2020-Feb-01, Sat,05:40 | Snow | Angle | Non-reportable North | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | West | Wet | Slowing or stopping | Automobile, station wagon | Other motor vehicle | Driving properly |
| 20-853992s | 2020-Jul-06, Mon,09:10 | Clear | Sideswipe | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North | Dry | Stopped | Truck - tractor | Other motor vehicle | Driving properly |
| 20855706 | 2020-Oct-01, Thu, 10:30 | Rain | Sideswipe | P.D. only West | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  | West | Wet | Turning right | Automobile, station wagon | Other motor vehicle | Driving properly |
| 20128184 | 2020-Dec-30, Wed, 16:51 | Rain | Angle | Non-fatal injury East | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |
| Comments: |  |  |  | North | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |


| 2167076 | 2021-Jul-04, Sun, 14:00 | Clear | Angle | P.D. only | West | Dry | Going ahead | Pick-up truck | Other motor vehicle | Failed to yield right-ofway |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: | Charged Driver \#1 on page 1: HTA 144 (8) (NA) |  |  |  | North | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 21855761 | 2021-Oct-28, Thu, 16:00 | Clear | Turning movement | P.D. only | North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  |  | South | Dry | Turning right | Pick-up truck | Other motor vehicle | Driving properly |  |
| 22852487 | 2022-Apr-01, Fri, 19:30 | Clear | Angle | P.D. only | South | Dry | Going ahead | Pick-up truck | Other motor vehicle |  |  |
| Comments: |  |  |  |  | West | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 22852868 | 2022-Apr-18, Mon, 15:00 | Clear | Angle | P.D. only | East | Dry | Turning right | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  |  | South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 22854158 | 2022-Jun-07, Tue,13:10 | Rain | Rear end | P.D. only | North | Wet | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  |  | North | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 22855713 | 2022-Aug-06, Sat, 23:30 | Clear | Angle | P.D. only | North | Dry | Turning left | Automobile, station wagon | Other motor vehicle | Improper turn |  |
| Comments: |  |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| 22856493 | 2022-Sep-06, Tue,20:00 | Clear | Other | P.D. only | West | Dry | Reversing |  | Other motor vehicle |  |  |
| Comments: |  |  |  |  | West | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Other |  |
| 23852769 | 2023-Mar-31, Fri, 15:15 | Rain | Angle | P.D. only | East | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Comments: |  |  |  |  | South | Wet | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Location .......... COLONEL TALBOT RD@CLAYTON WALKTraffic Control.... |  |  |  |  |  |  |  | Municipality........ LONDON |  |  |  |
|  |  |  |  |  |  |  | Traffic Control.... | Total Collisions.... 1 |  |  |  |
| Collision ID | Date/Day/Time | Enviro | Impact Type | Classification | Direction | Surface Cond'n | Vehicle Manoeuver | Vehicle type | First Event | Driver Action | No. Ped |
| 22851839 | 2022-Mar-08, Tue,21:30 | Clear | Other | P.D. only | West | Wet | Reversing | Automobile, station wagon | Other motor vehicle | Other |  |
| Comments: |  |  |  |  | East | Dry | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |  |
| Location .......... COLONEL TALBOT RD@DIANE CRES |  |  |  |  |  |  |  | Municipality....... LONDON |  |  |  |
| Traffic Control.... Stop sign |  |  |  |  |  |  |  | Total Collisions.... 1 |  |  |  |
| Collision ID | Date/Day/Time | Enviro | Impact Type | Classification | Direction | Surface Cond'n | Vehicle Manoeuver | Vehicle type | First Event | Driver Action | No. Ped |

Collision Details Report
From: January 1, 2015 To: May 16, 2023

| Location $\qquad$ COLONEL Traffic Control.... No control |  | TALBOT RD btwn CLAYTON WALK \& DIANE CRES |  |  |  | Municipality |  |  | LONDON 7 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Total Collisions.... |  |  |  |  |  |
| Collision ID | Date/Day/Time | Environment | Impact Type | Classification Direction | Surface Cond'n | Vehicle Manoeuver | Vehicle type | First Event |  | Driver Action | No. Ped |
| 16-75220 | 2016-Jul-19, Tue,13:58 | Clear | Rear end | Non-fatal injury South | Dry | Going ahead | Motorcycle | Other motor vehicle |  | Speed too fast for condition |  |
| Comments: |  |  |  | South | Dry | Slowing or stopping | Automobile, station wagon | Other motor vehicle |  | Driving properly |  |
| 18-854037s | 2018-May-23, Wed,00:20 | Clear | SMV other | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Animal - wild |  | Driving properly |  |
| Comments: Deer |  |  |  |  |  |  |  |  |  |  |  |
| 18-859081s | 2018-Nov-21, Wed,00:00 | Snow | SMV other | Non-reportable South | Loose snow | Going ahead | Passenger van | Animal - wild |  | Driving properly |  |
| Comments: Deer |  |  |  |  |  |  |  |  |  |  |  |
| 19-850966s | 2019-Jan-25, Fri,00:00 | Snow | SMV other | Non-reportable South | Ice | Turning right | Automobile, station wagon | Ran off road |  | Lost control |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |  |
| 20852421 | 2020-Mar-09, Mon,10:30 | Clear | SMV other | P.D. only South | Dry | Going ahead | Automobile, station wagon | Animal - wild |  | Driving properly |  |
| Comments: 48: Wild animal |  |  |  |  |  |  |  |  |  |  |  |
| 20856667 | 2020-Nov-17, Tue, 11:50 | Snow | Sideswipe | P.D. only South | Wet | Going ahead | Automobile, station wagon | Other motor vehicle |  | Driving properly |  |
| Comments: |  |  |  | South |  | Turning left | Automobile, station wagon | Other motor vehicle |  | Driving properly |  |
| 230334081 | 2023-Mar-21, Tue,12:00 | Clear | SMV other | P.D. only South | Dry | Going ahead | Automobile, station wagon | Animal - wild |  | Driving properly |  |
| Comments: Statement \#1: V1, SB COLONEL TALBOT ROAD, A DEER RUNS OUT <br> OF THE WEST DITCH INTO THE RIGHT FRONT SIDE OF V1. V1 <br> DRIVER HAD NO TIME TO AVOID DEER. DRIVER NOT INJURED. |  |  |  |  |  |  |  |  |  |  |  |
| Location .......... COLONEL TALBOT RD btwn CLAYTON WALK \& PACK RD |  |  |  |  |  | Municipality....... LONDON |  |  |  |  |  |
| Traffic Control.... No control |  |  |  |  |  | Total Collisions.... 13 |  |  |  |  |  |
| Collision ID | Date/Day/Time | Environment | Impact Type | Classification Direction | Surface Cond'n | Vehicle Manoeuver | Vehicle type | First Event |  | Driver Action | No. Ped |
| 15-97903s | 2015-Sep-09, Wed,05:40 | Clear | SMV other | Non-reportable South | Wet | Going ahead | Pick-up truck | Animal - wild |  | Driving properly |  |
| Comments: Deer |  |  |  |  |  |  |  |  |  |  |  |


| 16-24277s | 2016-Mar-09, Wed, 13:20 | Clear | Other | Non-reportable West | Dry | Reversing | Automobile, station wagon | Other motor vehicle | Failed to yield right-ofway |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments: |  |  |  | North |  | Stopped | Automobile, station wagon | Other motor vehicle | Driving properly |
| 16-128275s | 2016-Dec-03, Sat, 19:00 | Clear | SMV other | Non-reportable North | Dry | Going ahead | Automobile, station wagon | Animal - wild | Driving properly |
| Comments: | DEER |  |  |  | Dry |  |  |  |  |
| 17-1917s | 2017-Jan-06, Fri,07:05 | Clear | SMV other | Non-reportable North | Dry | Going ahead | Pick-up truck | Animal - wild | Driving properly |
| Comments: Deer |  |  |  |  |  |  |  |  |  |
| 17-852630s | 2017-Sep-01, Fri, 11:30 | Clear | SMV other | Non-reportable North | Dry | Going ahead | Pick-up truck | Animal - wild | Driving properly |
| Comments: DEER |  |  |  |  |  |  |  |  |  |
| 18-854943s | 2018-Jun-27, Wed,05:30 | Clear | SMV other | Non-reportable South | Dry | Going ahead | Automobile, station wagon | Animal - wild | Driving properly |
| Comments: Deer |  |  |  |  |  |  |  |  |  |
| 19-854464s | 2019-May-30, Thu,00:00 | Clear | Rear end | Non-reportable North | Dry | Turning right | Automobile, station wagon | Other motor vehicle | Other |
| Comments: |  |  |  | North |  | Stopped | Pick-up truck | Other motor vehicle | Driving properly |
| 19-856674s | 2019-Aug-20, Tue,00:00 | Clear | Approaching | Non-reportable South | Dry | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| Comments: |  |  |  | North |  | Going ahead | Automobile, station wagon | Other motor vehicle | Driving properly |
| 19-856785s | 2019-Aug-23, Fri,00:00 | Clear | SMV other | Non-reportable North | Dry | Going ahead | Passenger van | Animal - wild | Driving properly |
| Comments: Deer |  |  |  |  |  |  |  |  |  |
| 21852693 | 2021-Jun-11, Fri, 11:15 | Clear | SMV other | P.D. only South | Dry | Going ahead | Automobile, station wagon | Animal - wild | Driving properly |
| Comments: 48: Wild animal |  |  |  |  |  |  |  |  |  |
| 2198912 | 2021-Sep-28, Tue,04:30 | Clear | SMV other | P.D. only North | Dry | Going ahead | Automobile, station wagon | Ran off road | Exceeding speed limit |
| Comments: Charged Driver \#1 on page 1: HTA $130(1)$ (NA) |  |  |  |  |  |  |  |  |  |
| 22851985 | 2022-Mar-14, Mon,19:35 | Clear | Other | Non-reportable North | Wet | Going ahead | Automobile, station wagon | Debris falling off vehicle | Driving properly |
| Comments: |  |  |  | South |  | Going ahead | Pick-up truck | Debris falling off vehicle |  |
| 22859471 | 2022-Dec-12, Mon,23:20 | Clear | SMV other | P.D. only North | Dry | Going ahead | Automobile, station wagon | Animal - wild | Driving properly |
| Comments: | 48: Wild animal |  |  |  |  |  |  |  |  |





## Appendix C - Traffic Count Data

## H orizon D ata Services Ltd

318 Simonston Blvd
Thornhill, ON L3T 4T5
"we always count...never estimated"
File Name : Bostwick Road \& Pack Road
Site Code : 00000000
Start Date : 11/17/2021
Page No
: 5


## H orizon D ata Services Ltd

318 Simonston Blvd
Thornhill, ON L3T 4T5
"we always count...never estimated"
File Name : Bostwick Road \& Pack Road
Site Code : 00000000
Start Date : 11/17/2021
Page No : 11


## Turning Movements Report - AM Period

Location. $\qquad$ CAMPBELL ST @ MAIN ST
Municipality LONDON
GeolD....... INT6172
Count Date.......
Tuesday, 02 November, 2021
Peak Hour...... 08:00 AM —09:00 AM


## Turning Movements Report - PM Period

Location. $\qquad$ CAMPBELL ST @ MAIN ST
Municipality LONDON
GeolD....... INT6172
Count Date.......
Tuesday, 02 November, 2021
Peak Hour......
04:15 PM —05:15 PM








## Turning Movements Report - AM Period

Location $\qquad$ COLONEL TALBOT RD@CLAYTON WALK
Municipality LONDON
GeolD....... INT6076
Count Date.......
Tuesday, 08 November, 2022
Peak Hour......
07:45 AM —08:45 AM


## Turning Movements Report - PM Period

Location. $\qquad$ COLONEL TALBOT RD@CLAYTON WALK
Municipality LONDON
GeolD....... INT6076
Count Date.......
Tuesday, 08 November, 2022
Peak Hour......
04:45 PM — 05:45 PM




## Turning Movements Report - AM Period

Location $\qquad$ EXETER RD @ WHARNCLIFFE RD S
Municipality LONDON
GeolD....... INT6088
Count Date.......
Wednesday, 22 March, 2023
Peak Hour......
07:45 AM — 08:45 AM


## Turning Movements Report - PM Period

Location $\qquad$ EXETER RD @ WHARNCLIFFE RD S
Municipality LONDON
GeolD....... INT6088
Count Date.... Wednesday, 22 March, 2023 Peak Hour......
04:15 PM —05:15 PM


## Turning Movements Report - AM Period

Location. $\qquad$ BOSTWICK RD @ SOUTHDALE RD W
Municipality LONDON
GeoID....... INT5739
Count Date...
Tuesday, 21 May, 2019
Peak Hour...... 08:00 AM — 09:00 AM


## Turning Movements Report - PM Period

Location $\qquad$ BOSTWICK RD @ SOUTHDALE RD W
Municipality LONDON
GeoID....... INT5739
Count Date...
Tuesday, 21 May, 2019
Peak Hour...... 04:45 PM —05:45 PM


## Appendix D - Trip Generation Data

# Single-Family Detached Housing <br> (210) 

Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban
Number of Studies: 192
Avg. Num. of Dwelling Units: 226
Directional Distribution: $25 \%$ entering, $75 \%$ exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.70 | $0.27-2.27$ | 0.24 |

Data Plot and Equation


## Single-Family Detached Housing

 (210)Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic,<br>One Hour Between 4 and 6 p.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 208<br>Avg. Num. of Dwelling Units: 248<br>Directional Distribution: 63\% entering, 37\% exiting

## Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.94 | $0.35-2.98$ | 0.31 |

## Data Plot and Equation



# Single-Family Attached Housing (215) 

Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban
Number of Studies: 46
Avg. Num. of Dwelling Units: 135
Directional Distribution: 25\% entering, 75\% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate
0.48

Range of Rates
0.12-0.74

Standard Deviation
0.14

## Data Plot and Equation



## Single-Family Attached Housing (215)

Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic,<br>One Hour Between 4 and 6 p.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 51<br>Avg. Num. of Dwelling Units: 136<br>Directional Distribution: 59\% entering, $41 \%$ exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate
0.57

Range of Rates
0.17-1.25

Standard Deviation
0.18

Data Plot and Equation


# Multifamily Housing (Mid-Rise) <br> Not Close to Rail Transit (221) 



- Institute of Transportation Engineers


# Multifamily Housing (Mid-Rise) <br> Not Close to Rail Transit (221) 

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Studies: 31
Avg. Num. of Dweiling Units: 169
Directional Distribution: 61\% entering, 39\% exiting
Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.39 | $0.19-0.57$ | 0.08 |

## Data Plot and Equation



# Multifamily Housing (High-Rise) <br> Not Close to Rail Transit (222) 

## Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.
Setting/Location: General Urban/Suburban
Number of Studies:
45
Avg. Num. of Dwelling Units: 372
Directional Distribution: 26\% entering, 74\% exiting

## Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.27 | $0.09-0.67$ | 0.11 |

## Data Plot and Equation



# Multifamily Housing (High-Rise) <br> Not Close to Rail Transit (222) 

Vehicle Trip Ends vs: Dwelling Units
On a: Weekday,
Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Studies: 45
Avg. Num. of Dwelling Units: 372
Directional Distribution: 62\% entering, 38\% exiting

\section*{Vehicle Trip Generation per Dwelling Unit <br> | Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.32 | $0.09-0.80$ | 0.13 |}

## Data Plot and Equation



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## Appendix E - Intersection Capacity Analysis

|  | 4 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\dagger$ |  | ( | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 54 | 49 | 22 | 35 | 33 | 85 | 46 | 428 | 32 | 125 | 517 | 49 |
| Future Volume (vph) | 54 | 49 | 22 | 35 | 33 | 85 | 46 | 428 | 32 | 125 | 517 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 0.0 | 80.0 |  | 0.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |  |  |
| Frt |  | 0.953 |  |  | 0.892 |  |  | 0.990 |  |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1674 | 0 | 1674 | 1500 | 0 | 1615 | 1749 | 0 | 1674 | 1789 | 0 |
| Flt Permitted | 0.672 |  |  | 0.705 |  |  | 0.380 |  |  | 0.452 |  |  |
| Satd. Flow (perm) | 1184 | 1674 | 0 | 1238 | 1500 | 0 | 646 | 1749 | 0 | 796 | 1789 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 25 |  |  | 96 |  |  | 8 |  |  | 10 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 61 | 55 | 25 | 39 | 37 | 96 | 52 | 481 | 36 | 140 | 581 | 55 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 61 | 80 | 0 | 39 | 133 | 0 | 52 | 517 | 0 | 140 | 636 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 25.2 | 25.2 |  | 45.9 | 45.9 |  | 45.9 | 45.9 |  |
| Total Split (s) | 29.0 | 29.0 |  | 29.0 | 29.0 |  | 51.0 | 51.0 |  | 51.0 | 51.0 |  |
| Total Split (\%) | 36.3\% | 36.3\% |  | 36.3\% | 36.3\% |  | 63.8\% | 63.8\% |  | 63.8\% | 63.8\% |  |
| Maximum Green (s) | 22.8 | 22.8 |  | 22.8 | 22.8 |  | 45.1 | 45.1 |  | 45.1 | 45.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 4.3 | 4.3 |  | 3.8 | 3.8 |  | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 1.9 | 1.9 |  | 2.1 | 2.1 |  | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 6.2 | 6.2 |  | 5.9 | 5.9 |  | 5.9 | 5.9 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 28.0 | 28.0 |  | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 9.1 | 9.1 |  | 9.1 | 9.1 |  | 49.3 | 49.3 |  | 49.3 | 49.3 |  |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.14 | 0.14 |  | 0.74 | 0.74 |  | 0.74 | 0.74 |  |
| v/c Ratio | 0.38 | 0.32 |  | 0.23 | 0.46 |  | 0.11 | 0.40 |  | 0.24 | 0.48 |  |


|  | $\rangle$ |  |  | $\checkmark$ |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 32.9 | 22.5 |  | 28.7 | 15.5 |  | 5.0 | 5.8 |  | 5.8 | 6.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 32.9 | 22.5 |  | 28.7 | 15.5 |  | 5.0 | 5.8 |  | 5.8 | 6.7 |  |
| LOS | C | C |  | C | B |  | A | A |  | A | A |  |
| Approach Delay |  | 27.0 |  |  | 18.5 |  |  | 5.8 |  |  | 6.5 |  |
| Approach LOS |  | C |  |  | B |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 7.0 | 6.2 |  | 4.4 | 4.1 |  | 1.8 | 22.4 |  | 5.3 | 30.1 |  |
| Queue Length 95th (m) | 16.6 | 16.7 |  | 11.9 | 17.1 |  | 6.0 | 45.7 |  | 14.4 | 60.8 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  |  | 80.0 |  |  | 120.0 |  |  |
| Base Capacity (vph) | 404 | 588 |  | 423 | 576 |  | 477 | 1295 |  | 588 | 1325 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.14 |  | 0.09 | 0.23 |  | 0.11 | 0.40 |  | 0.24 | 0.48 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 66.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.48 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 9.2 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 65.3\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road






| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | $\mathbf{1}$ | $\mathbf{7}$ | $\mathbf{1}$ | 4 | 个 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 35 | 77 | 49 | 407 | 565 | 28 |
| Future Vol, veh/h | 35 | 77 | 49 | 407 | 565 | 28 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 45 | 0 | 55 | - | - | 45 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, \% | 3 | 7 | 8 | 10 | 6 | 19 |
| Mvmt Flow | 39 | 87 | 55 | 457 | 635 | 31 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road SouthExisting Traffic W3 Sunset Creek

|  | 4 |  |  | 7 | - |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  | \% | $\uparrow$ |  | 7 | $\uparrow$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 31 | 418 | 33 | 187 | 548 | 88 | 55 | 88 | 270 | 96 | 30 | 34 |
| Future Volume (vph) | 31 | 418 | 33 | 187 | 548 | 88 | 55 | 88 | 270 | 96 | 30 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  | 1.00 |  | 0.98 | 0.98 |  | 1.00 | 0.98 |  |
| Frt |  | 0.989 |  |  | 0.979 |  |  | 0.887 |  |  | 0.921 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1808 | 0 | 1738 | 1769 | 0 | 1789 | 1570 | 0 | 1674 | 1553 | 0 |
| Flt Permitted | 0.292 |  |  | 0.436 |  |  | 0.711 |  |  | 0.276 |  |  |
| Satd. Flow (perm) | 529 | 1808 | 0 | 798 | 1769 | 0 | 1308 | 1570 | 0 | 486 | 1553 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  | 13 |  |  | 219 |  |  | 37 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 34 | 454 | 36 | 203 | 596 | 96 | 60 | 96 | 293 | 104 | 33 | 37 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 34 | 490 | 0 | 203 | 692 | 0 | 60 | 389 | 0 | 104 | 70 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 40.0 | 40.0 |  | 40.0 | 40.0 |  |
| Total Split (\%) | 52.4\% | 52.4\% |  | 52.4\% | 52.4\% |  | 47.6\% | 47.6\% |  | 47.6\% | 47.6\% |  |
| Maximum Green (s) | 38.0 | 38.0 |  | 38.0 | 38.0 |  | 34.0 | 34.0 |  | 34.0 | 34.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 |  | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 38.3 | 38.3 |  | 38.3 | 38.3 |  | 14.5 | 14.5 |  | 14.5 | 14.5 |  |
| Actuated g/C Ratio | 0.59 | 0.59 |  | 0.59 | 0.59 |  | 0.22 | 0.22 |  | 0.22 | 0.22 |  |
| v/c Ratio | 0.11 | 0.46 |  | 0.43 | 0.66 |  | 0.21 | 0.75 |  | 0.96 | 0.19 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road SouthExisting Traffic W3 Sunset Creek

|  | 4 |  |  | $\dagger$ |  |  |  | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 9.1 | 10.5 |  | 12.9 | 14.4 |  | 21.2 | 19.5 |  | 106.0 | 12.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 9.1 | 10.5 |  | 12.9 | 14.4 |  | 21.2 | 19.5 |  | 106.0 | 12.1 |  |
| LOS | A | B |  | B | B |  | C | B |  | F | B |  |
| Approach Delay |  | 10.4 |  |  | 14.0 |  |  | 19.7 |  |  | 68.2 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | E |  |
| Queue Length 50th (m) | 1.6 | 28.5 |  | 11.8 | 47.9 |  | 5.9 | 17.8 |  | 12.3 | 3.1 |  |
| Queue Length 95th (m) | 7.0 | 67.3 |  | 35.9 | 113.9 |  | 13.9 | 44.0 |  | \#35.6 | 11.3 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 312 | 1068 |  | 470 | 1048 |  | 689 | 931 |  | 256 | 836 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.11 | 0.46 |  | 0.43 | 0.66 |  | 0.09 | 0.42 |  | 0.41 | 0.08 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 84.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 65 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.96 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 19.0 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 87.4\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | \% | f |  | \% | F |  | ${ }^{7}$ | ¢ |  |
| Traffic Volume (vph) | 56 | 48 | 36 | 40 | 60 | 207 | 47 | 709 | 45 | 82 | 495 | 64 |
| Future Volume (vph) | 56 | 48 | 36 | 40 | 60 | 207 | 47 | 709 | 45 | 82 | 495 | 64 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 0.0 | 80.0 |  | 0.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 0.99 |  | 0.99 | 0.98 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt |  | 0.936 |  |  | 0.884 |  |  | 0.991 |  |  | 0.983 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1676 | 0 | 1825 | 1626 | 0 | 1789 | 1864 | 0 | 1789 | 1813 | 0 |
| Flt Permitted | 0.364 |  |  | 0.699 |  |  | 0.386 |  |  | 0.261 |  |  |
| Satd. Flow (perm) | 670 | 1676 | 0 | 1333 | 1626 | 0 | 726 | 1864 | 0 | 491 | 1813 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 38 |  |  | 185 |  |  | 7 |  |  | 13 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 60 | 51 | 38 | 43 | 64 | 220 | 50 | 754 | 48 | 87 | 527 | 68 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 60 | 89 | 0 | 43 | 284 | 0 | 50 | 802 | 0 | 87 | 595 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 25.2 | 25.2 |  | 45.9 | 45.9 |  | 45.9 | 45.9 |  |
| Total Split (s) | 29.0 | 29.0 |  | 29.0 | 29.0 |  | 51.0 | 51.0 |  | 51.0 | 51.0 |  |
| Total Split (\%) | 36.3\% | 36.3\% |  | 36.3\% | 36.3\% |  | 63.8\% | 63.8\% |  | 63.8\% | 63.8\% |  |
| Maximum Green (s) | 22.8 | 22.8 |  | 22.8 | 22.8 |  | 45.1 | 45.1 |  | 45.1 | 45.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 4.3 | 4.3 |  | 3.8 | 3.8 |  | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 1.9 | 1.9 |  | 2.1 | 2.1 |  | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 6.2 | 6.2 |  | 5.9 | 5.9 |  | 5.9 | 5.9 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 28.0 | 28.0 |  | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effit Green (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 45.3 | 45.3 |  | 45.3 | 45.3 |  |
| Actuated g/C Ratio | 0.16 | 0.16 |  | 0.16 | 0.16 |  | 0.66 | 0.66 |  | 0.66 | 0.66 |  |
| v/c Ratio | 0.56 | 0.30 |  | 0.20 | 0.68 |  | 0.10 | 0.65 |  | 0.27 | 0.49 |  |


|  | 4 |  |  | 7 |  |  | , | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 46.3 | 18.3 |  | 26.4 | 18.9 |  | 6.0 | 10.9 |  | 8.7 | 8.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 46.3 | 18.3 |  | 26.4 | 18.9 |  | 6.0 | 10.9 |  | 8.7 | 8.2 |  |
| LOS | D | B |  | C | B |  | A | B |  | A | A |  |
| Approach Delay |  | 29.6 |  |  | 19.9 |  |  | 10.6 |  |  | 8.3 |  |
| Approach LOS |  | C |  |  | B |  |  | B |  |  | A |  |
| Queue Length 50th (m) | 7.1 | 5.7 |  | 4.8 | 11.4 |  | 1.8 | 47.0 |  | 3.6 | 29.1 |  |
| Queue Length 95th (m) | 17.9 | 16.3 |  | 12.3 | 32.6 |  | 7.3 | 114.1 |  | 14.0 | 70.5 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length ( m ) | 55.0 |  |  | 55.0 |  |  | 80.0 |  |  | 20.0 |  |  |
| Base Capacity (vph) | 224 | 586 |  | 445 | 667 |  | 480 | 1236 |  | 324 | 1204 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.27 | 0.15 |  | 0.10 | 0.43 |  | 0.10 | 0.65 |  | 0.27 | 0.49 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 68.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.68 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 12.7 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 88.1\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Mr |  |  | 个 | 个 | $\mathbf{7}$ |
| Traffic Vol, veh/h | 13 | 6 | 10 | 771 | 512 | 26 |
| Future Vol, veh/h | 13 | 6 | 10 | 771 | 512 | 26 |
| Conflicting Peds, \#/hr | 0 | 6 | 28 | 0 | 0 | 28 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 75 | - | - | 80 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 8 | 0 | 0 | 1 | 3 | 4 |
| Mvmt Flow | 14 | 6 | 11 | 812 | 539 | 27 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road SouthExisting Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | \% | $\hat{1}$ |  | \% | $\uparrow$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 61 | 626 | 39 | 132 | 620 | 91 | 27 | 40 | 87 | 97 | 45 | 65 |
| Future Volume (vph) | 61 | 626 | 39 | 132 | 620 | 91 | 27 | 40 | 87 | 97 | 45 | 65 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.99 |  |
| Frt |  | 0.991 |  |  | 0.981 |  |  | 0.897 |  |  | 0.911 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1848 | 0 | 1772 | 1868 | 0 | 1825 | 1677 | 0 | 1825 | 1724 | 0 |
| Flt Permitted | 0.306 |  |  | 0.332 |  |  | 0.671 |  |  | 0.611 |  |  |
| Satd. Flow (perm) | 588 | 1848 | 0 | 619 | 1868 | 0 | 1284 | 1677 | 0 | 1174 | 1724 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  | 15 |  |  | 95 |  |  | 69 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 66 | 680 | 42 | 143 | 674 | 99 | 29 | 43 | 95 | 105 | 49 | 71 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 66 | 722 | 0 | 143 | 773 | 0 | 29 | 138 | 0 | 105 | 120 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 70.0 | 70.0 |  | 70.0 | 70.0 |  | 30.0 | 30.0 |  | 30.0 | 30.0 |  |
| Total Split (\%) | 70.0\% | 70.0\% |  | 70.0\% | 70.0\% |  | 30.0\% | 30.0\% |  | 30.0\% | 30.0\% |  |
| Maximum Green (s) | 63.9 | 63.9 |  | 63.9 | 63.9 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 |  | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | C-Max | C-Max |  | C-Max | C-Max |  | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | , | , |  | 0 | 0 |  | , | 0 |  | 0 | 0 |  |
| Act Efft Green (s) | 74.3 | 74.3 |  | 74.3 | 74.3 |  | 13.6 | 13.6 |  | 13.6 | 13.6 |  |
| Actuated g/C Ratio | 0.74 | 0.74 |  | 0.74 | 0.74 |  | 0.14 | 0.14 |  | 0.14 | 0.14 |  |
| v/c Ratio | 0.15 | 0.53 |  | 0.31 | 0.56 |  | 0.17 | 0.45 |  | 0.66 | 0.41 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road SouthExisting Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  | , | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 5.7 | 7.7 |  | 7.3 | 8.1 |  | 38.1 | 18.4 |  | 59.7 | 21.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 5.7 | 7.7 |  | 7.3 | 8.1 |  | 38.1 | 18.4 |  | 59.7 | 21.8 |  |
| LOS | A | A |  | A | A |  | D | B |  | E | C |  |
| Approach Delay |  | 7.6 |  |  | 7.9 |  |  | 21.8 |  |  | 39.5 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | D |  |
| Queue Length 50th (m) | 3.1 | 48.8 |  | 7.8 | 53.5 |  | 5.0 | 7.5 |  | 19.6 | 8.9 |  |
| Queue Length 95th (m) | 9.2 | 92.5 |  | 20.7 | 101.7 |  | 12.3 | 23.0 |  | 34.5 | 23.2 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 437 | 1375 |  | 460 | 1392 |  | 308 | 474 |  | 281 | 466 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.53 |  | 0.31 | 0.56 |  | 0.09 | 0.29 |  | 0.37 | 0.26 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 32 (32\%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.66 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 12.3 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 77.4\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个 |  | * | ¢ |  | ${ }^{1}$ | f |  | \% | ¢ |  |
| Traffic Volume (vph) | 47 | 77 | 29 | 129 | 57 | 146 | 67 | 703 | 196 | 185 | 632 | 49 |
| Future Volume (vph) | 47 | 77 | 29 | 129 | 57 | 146 | 67 | 703 | 196 | 185 | 632 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 0.0 | 80.0 |  | 0.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 |  |  |  | 1.00 |  | 1.00 |  |  |
| Frt |  | 0.959 |  |  | 0.892 |  |  | 0.967 |  |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1697 | 0 | 1674 | 1499 | 0 | 1615 | 1719 | 0 | 1674 | 1792 | 0 |
| Flt Permitted | 0.290 |  |  | 0.617 |  |  | 0.311 |  |  | 0.197 |  |  |
| Satd. Flow (perm) | 511 | 1697 | 0 | 1081 | 1499 | 0 | 529 | 1719 | 0 | 347 | 1792 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 12 |  |  | 83 |  |  | 32 |  |  | 9 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 53 | 87 | 33 | 145 | 64 | 164 | 75 | 790 | 220 | 208 | 710 | 55 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 53 | 120 | 0 | 145 | 228 | 0 | 75 | 1010 | 0 | 208 | 765 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 25.2 | 25.2 |  | 45.9 | 45.9 |  | 45.9 | 45.9 |  |
| Total Split (s) | 25.2 | 25.2 |  | 25.2 | 25.2 |  | 104.8 | 104.8 |  | 104.8 | 104.8 |  |
| Total Split (\%) | 19.4\% | 19.4\% |  | 19.4\% | 19.4\% |  | 80.6\% | 80.6\% |  | 80.6\% | 80.6\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 19.0 | 19.0 |  | 98.9 | 98.9 |  | 98.9 | 98.9 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 4.3 | 4.3 |  | 3.8 | 3.8 |  | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 1.9 | 1.9 |  | 2.1 | 2.1 |  | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 6.2 | 6.2 |  | 5.9 | 5.9 |  | 5.9 | 5.9 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 28.0 | 28.0 |  | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effit Green (s) | 18.7 | 18.7 |  | 18.7 | 18.7 |  | 98.9 | 98.9 |  | 98.9 | 98.9 |  |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.14 | 0.14 |  | 0.76 | 0.76 |  | 0.76 | 0.76 |  |
| v/c Ratio | 0.73 | 0.47 |  | 0.94 | 0.80 |  | 0.19 | 0.77 |  | 0.79 | 0.56 |  |


|  | $\rangle$ |  |  |  |  |  | , | $\dagger$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 101.9 | 52.5 |  | 112.3 | 54.5 |  | 5.6 | 13.5 |  | 33.8 | 8.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 101.9 | 52.5 |  | 112.3 | 54.5 |  | 5.6 | 13.5 |  | 33.8 | 8.2 |  |
| LOS | F | D |  | F | D |  | A | B |  | C | A |  |
| Approach Delay |  | 67.6 |  |  | 77.0 |  |  | 12.9 |  |  | 13.7 |  |
| Approach LOS |  | E |  |  | E |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 13.1 | 25.6 |  | 37.1 | 36.7 |  | 4.6 | 124.9 |  | 27.6 | 69.8 |  |
| Queue Length 95th (m) | \#35.0 | 44.5 |  | \#76.1 | \#74.0 |  | 9.5 | 175.5 |  | \#87.3 | 93.5 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  |  | 80.0 |  |  | 120.0 |  |  |
| Base Capacity (vph) | 74 | 259 |  | 157 | 290 |  | 403 | 1318 |  | 264 | 1368 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.72 | 0.46 |  | 0.92 | 0.79 |  | 0.19 | 0.77 |  | 0.79 | 0.56 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 129.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.94 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 26.0 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 97.2\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road




## 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffwtere (2033) Background Traffic W3 Sunset Creek




4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

Future (2033) Background Traffic
AM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「' | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 566 | 53 | 26 | 780 | 32 |
| Future Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 566 | 53 | 26 | 780 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.856 |  |  | 0.862 |  |  |  | 0.850 |  | 0.994 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1541 | 0 | 1825 | 1656 | 0 | 1690 | 1746 | 1633 | 1825 | 1793 | 0 |
| Fit Permitted | 0.699 |  |  | 0.688 |  |  | 0.176 |  |  | 0.344 |  |  |
| Satd. Flow (perm) | 1304 | 1541 | 0 | 1322 | 1656 | 0 | 313 | 1746 | 1633 | 661 | 1793 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 103 |  |  | 83 |  |  |  | 60 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 3\% | 0\% | 7\% | 0\% | 0\% | 0\% | 8\% | 10\% | 0\% | 0\% | 6\% | 19\% |
| Adj. Flow (vph) | 46 | 4 | 103 | 239 | 7 | 83 | 67 | 636 | 60 | 29 | 876 | 36 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 46 | 107 | 0 | 239 | 90 | 0 | 67 | 636 | 60 | 29 | 912 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 56.0 | 56.0 | 56.0 | 56.0 | 56.0 |  |
| Total Split (\%) | 30.0\% | 30.0\% |  | 30.0\% | 30.0\% |  | 70.0\% | 70.0\% | 70.0\% | 70.0\% | 70.0\% |  |
| Maximum Green (s) | 18.3 | 18.3 |  | 18.3 | 18.3 |  | 49.6 | 49.6 | 49.6 | 49.6 | 49.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 17.0 | 17.0 |  | 17.0 | 17.0 |  | 50.8 | 50.8 | 50.8 | 50.8 | 50.8 |  |
| Actuated g/C Ratio | 0.21 | 0.21 |  | 0.21 | 0.21 |  | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 |  |
| v/c Ratio | 0.17 | 0.26 |  | 0.85 | 0.22 |  | 0.34 | 0.57 | 0.06 | 0.07 | 0.80 |  |
| Control Delay | 26.6 | 8.0 |  | 57.8 | 8.7 |  | 13.2 | 11.3 | 1.9 | 6.6 | 18.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

|  | 4 |  |  | $\checkmark$ |  |  | 4 | $\uparrow$ | 7 | - | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | 26.6 | 8.0 |  | 57.8 | 8.7 |  | 13.2 | 11.3 | 1.9 | 6.6 | 18.3 |  |
| LOS | C | A |  | E | A |  | B | B | A | A | B |  |
| Approach Delay |  | 13.6 |  |  | 44.4 |  |  | 10.7 |  |  | 17.9 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 5.6 | 0.5 |  | 34.3 | 0.8 |  | 4.4 | 51.6 | 0.0 | 1.6 | 95.1 |  |
| Queue Length 95th (m) | 13.9 | 11.8 |  | \#68.7 | 11.3 |  | 13.1 | 78.5 | 3.7 | 4.6 | 148.8 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 298 | 432 |  | 302 | 443 |  | 199 | 1109 | 1059 | 419 | 1141 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.25 |  | 0.79 | 0.20 |  | 0.34 | 0.57 | 0.06 | 0.07 | 0.80 |  |

## Intersection Summary

Area Type: Other

Cycle Length: 80
Actuated Cycle Length: 79.9

## Natural Cycle: 70

Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.85
Intersection Signal Delay: 19.1
Intersection LOS: B
Intersection Capacity Utilization 78.4\%
ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Whalfintiffe $\mathbb{R} 202 B$ BBattkground Traffic W3 Sunset Creek

|  | $\psi$ | $\rightarrow$ |  | 7 |  |  | 4 | 9 | $p$ |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F |  | ${ }^{*}$ | F |  | ${ }^{7}$ | F |  | ${ }^{1}$ | $\dagger$ |  |
| Traffic Volume (vph) | 64 | 616 | 43 | 187 | 702 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Future Volume (vph) | 64 | 616 | 43 | 187 | 702 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  | 1.00 |  | 0.98 | 0.98 |  | 1.00 | 0.96 |  |
| Frt |  | 0.990 |  |  | 0.982 |  |  | 0.888 |  |  | 0.880 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1810 | 0 | 1738 | 1775 | 0 | 1789 | 1572 | 0 | 1674 | 1438 | 0 |
| Fit Permitted | 0.133 |  |  | 0.239 |  |  | 0.639 |  |  | 0.315 |  |  |
| Satd. Flow (perm) | 241 | 1810 | 0 | 437 | 1775 | 0 | 1180 | 1572 | 0 | 555 | 1438 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  | 10 |  |  | 155 |  |  | 116 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 70 | 670 | 47 | 203 | 763 | 102 | 66 | 99 | 293 | 152 | 38 | 150 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 70 | 717 | 0 | 203 | 865 | 0 | 66 | 392 | 0 | 152 | 188 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 40.0 | 40.0 |  | 40.0 | 40.0 |  |
| Total Split (\%) | 52.4\% | 52.4\% |  | 52.4\% | 52.4\% |  | 47.6\% | 47.6\% |  | 47.6\% | 47.6\% |  |
| Maximum Green (s) | 38.0 | 38.0 |  | 38.0 | 38.0 |  | 34.0 | 34.0 |  | 34.0 | 34.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 |  | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max |  | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 38.5 | 38.5 |  | 38.5 | 38.5 |  | 19.9 | 19.9 |  | 19.9 | 19.9 |  |
| Actuated g/C Ratio | 0.54 | 0.54 |  | 0.54 | 0.54 |  | 0.28 | 0.28 |  | 0.28 | 0.28 |  |
| v/c Ratio | 0.53 | 0.73 |  | 0.85 | 0.89 |  | 0.20 | 0.71 |  | 0.98 | 0.39 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe ReazBSBattkground Traffic W3 Sunset Creek

|  |  |  |  |  |  |  |  | $\dagger$ | / |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 34.7 | 20.3 |  | 53.0 | 30.7 |  | 19.3 | 20.2 |  | 93.4 | 10.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 34.7 | 20.3 |  | 53.0 | 30.7 |  | 19.3 | 20.2 |  | 93.4 | 10.2 |  |
| LOS | C | C |  | D | C |  | B | C |  | F | B |  |
| Approach Delay |  | 21.6 |  |  | 35.0 |  |  | 20.1 |  |  | 47.4 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | D |  |
| Queue Length 50th (m) | 5.4 | 64.2 |  | 20.7 | 90.7 |  | 6.5 | 26.8 |  | 19.5 | 7.1 |  |
| Queue Length 95th (m) | \#30.3 | \#167.6 |  | \#74.9 | \#224.6 |  | 14.6 | 52.7 |  | \#49.0 | 20.1 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 131 | 988 |  | 238 | 972 |  | 575 | 846 |  | 270 | 760 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.53 | 0.73 |  | 0.85 | 0.89 |  | 0.11 | 0.46 |  | 0.56 | 0.25 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 84.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 70.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.98 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 30.0 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 97.9\% ICU Level of Service FAnalysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road South


|  | $\rangle$ |  |  |  |  |  |  | 4 | $p$ | * | $\frac{1}{\downarrow}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  | \% | $\uparrow$ |  | 7 | $\uparrow$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 54 | 85 | 49 | 241 | 104 | 308 | 65 | 893 | 200 | 174 | 690 | 53 |
| Future Volume (vph) | 54 | 85 | 49 | 241 | 104 | 308 | 65 | 893 | 200 | 174 | 690 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 0.0 | 80.0 |  | 0.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 | 0.98 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.945 |  |  | 0.888 |  |  | 0.973 |  |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1693 | 0 | 1825 | 1633 | 0 | 1789 | 1827 | 0 | 1789 | 1825 | 0 |
| Flt Permitted | 0.168 |  |  | 0.633 |  |  | 0.288 |  |  | 0.058 |  |  |
| Satd. Flow (perm) | 310 | 1693 | 0 | 1205 | 1633 | 0 | 542 | 1827 | 0 | 109 | 1825 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 24 |  |  | 123 |  |  | 18 |  |  | 8 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 57 | 90 | 52 | 256 | 111 | 328 | 69 | 950 | 213 | 185 | 734 | 56 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 57 | 142 | 0 | 256 | 439 | 0 | 69 | 1163 | 0 | 185 | 790 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 5.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 25.2 | 25.2 |  | 45.9 | 45.9 |  | 8.0 | 45.9 |  |
| Total Split (s) | 30.0 | 30.0 |  | 30.0 | 30.0 |  | 72.0 | 72.0 |  | 8.0 | 80.0 |  |
| Total Split (\%) | 27.3\% | 27.3\% |  | 27.3\% | 27.3\% |  | 65.5\% | 65.5\% |  | 7.3\% | 72.7\% |  |
| Maximum Green (s) | 23.8 | 23.8 |  | 23.8 | 23.8 |  | 66.1 | 66.1 |  | 5.0 | 74.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 4.3 | 4.3 |  | 3.8 | 3.8 |  | 3.0 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 1.9 | 1.9 |  | 2.1 | 2.1 |  | 0.0 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 6.2 | 6.2 |  | 5.9 | 5.9 |  | 3.0 | 5.9 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 28.0 | 28.0 |  |  | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  |  | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Act Effct Green (s) | 23.8 | 23.8 |  | 23.8 | 23.8 |  | 66.1 | 66.1 |  | 77.0 | 74.1 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.60 | 0.60 |  | 0.70 | 0.67 |  |
| v/c Ratio | 0.85 | 0.37 |  | 0.98 | 0.98 |  | 0.21 | 1.05 |  | 1.22 | 0.64 |  |


|  | 4 |  |  |  |  |  | , | $\uparrow$ | $>$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 118.7 | 33.5 |  | 96.2 | 69.1 |  | 12.1 | 64.9 |  | 166.1 | 13.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 118.7 | 33.5 |  | 96.2 | 69.1 |  | 12.1 | 64.9 |  | 166.1 | 13.2 |  |
| LOS | F | C |  | F | E |  | B | E |  | F | B |  |
| Approach Delay |  | 57.9 |  |  | 79.1 |  |  | 61.9 |  |  | 42.2 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | D |  |
| Queue Length 50th (m) | 11.8 | 21.5 |  | 55.0 | 71.1 |  | 6.3 | $\sim 272.2$ |  | $\sim 32.4$ | 87.0 |  |
| Queue Length 95th (m) | \#36.5 | 39.8 |  | \#105.5 | \#134.1 |  | 14.0 | \#351.1 |  | \#76.6 | 123.9 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  |  | 80.0 |  |  | 120.0 |  |  |
| Base Capacity (vph) | 67 | 385 |  | 260 | 449 |  | 325 | 1105 |  | 152 | 1231 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.85 | 0.37 |  | 0.98 | 0.98 |  | 0.21 | 1.05 |  | 1.22 | 0.64 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.22 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 59.3 |  |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 118.0\% |  |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2201 | 2201 | 935 | 2214 | 2229 | 1196 | 963 | 0 | 0 | 1196 | 0 | 0 |
| Stage 1 | 935 | 935 | - | 1266 | 1266 | - | - | - | - | - | - | - |
| Stage 2 | 1266 | 1266 | - | 948 | 963 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.24 | 7.1 | 6.5 | 6.2 | 4.13 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.336 | 3.5 | 4 | 3.3 | 2.227 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | ~32 | 45 | 319 | 32 | 43 | 229 | 711 | - | - | 591 | - | - |
| Stage 1 | 321 | 347 | - | 209 | 242 | - | - | - | - | - | - | - |
| Stage 2 | 209 | 242 | - | 316 | 337 | - | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | ~31 | 43 | 319 | 28 | 41 | 229 | 711 | - | - | 591 | - | - |
| Mov Cap-2 Maneuver | $\sim 31$ | 43 | - | 28 | 41 | - | - | - | - | - | - | - |
| Stage 1 | 305 | 347 | - | 199 | 230 | - | - | - | - | - | - | - |
| Stage 2 | 199 | 230 | - | 291 | 337 | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 214.9 |  |  | 0 |  |  | 0.3 |  |  | 0 |  |  |
| HCM LOS | F |  |  | A |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | EBLn2W | VBLn1 | SBL | SBT | SBR |  |  |
| Capacity (veh/h) |  | 711 | - | - | 31 | 319 | - | 591 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.049 | - | - | 1.053 | 0.079 | - | - | - | - |  |  |
| HCM Control Delay (s) |  | 10.3 | - |  | 367.8 | 17.3 | 0 | 0 | - | - |  |  |
| HCM Lane LOS |  | B | - | - | F | C | A | A | - | - |  |  |
| HCM 95th \%tile Q(veh) |  | 0.2 | - | - | 3.6 | 0.3 | - | 0 | - | - |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |

## 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffwtere (2033) Background Traffic W3 Sunset Creek




| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1WBLn2 |  |  | SBL | SBT | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 776 | - | 19 | 27 | 237 | 582 | - | - | - |
| HCM Lane V/C Ratio | 0.014 | - | - 1.053 | 0.741 | 0.382 | 0.192 | - |  | - |
| HCM Control Delay (s) | 9.7 | - | \$ 506.1 | 298.7 | 29.3 | 12.6 | - |  |  |
| HCM Lane LOS | A | - | F | F | D | B | - | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 2.8 | 2.3 | 1.7 | 0.7 | - | - | - |
| Notes |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity | \$: De | ay exc | ceeds 300s | +: Com | putation | Not D | fined | *: All | All major volume in platoon |


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | f |  | ${ }^{7}$ | ¢ |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | 个 |  |
| Traffic Volume (vph) | 39 | - | 78 | 136 | 10 | 49 | 106 | 1077 | 223 | 72 | 645 | 63 |
| Future Volume (vph) | 39 | 9 | 78 | 136 | 10 | 49 | 106 | 1077 | 223 | 72 | 645 | 63 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.98 |  | 1.00 |  |  |  |  |  |  |  |  |
| Frt |  | 0.866 |  |  | 0.876 |  |  |  | 0.850 |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1601 | 0 | 1825 | 1683 | 0 | 1825 | 1902 | 1633 | 1825 | 1826 | 0 |
| Flt Permitted | 0.715 |  |  | 0.696 |  |  | 0.312 |  |  | 0.122 |  |  |
| Satd. Flow (perm) | 1334 | 1601 | 0 | 1334 | 1683 | 0 | 599 | 1902 | 1633 | 234 | 1826 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 84 |  |  | 53 |  |  |  | 220 |  | 12 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 3\% | 0\% | 2\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 4\% | 2\% |
| Adj. Flow (vph) | 42 | 10 | 84 | 146 | 11 | 53 | 114 | 1158 | 240 | 77 | 694 | 68 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 42 | 94 | 0 | 146 | 64 | 0 | 114 | 1158 | 240 | 77 | 762 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 86.3 | 86.3 | 86.3 | 86.3 | 86.3 |  |
| Total Split (\%) | 21.5\% | 21.5\% |  | 21.5\% | 21.5\% |  | 78.5\% | 78.5\% | 78.5\% | 78.5\% | 78.5\% |  |
| Maximum Green (s) | 18.0 | 18.0 |  | 18.0 | 18.0 |  | 79.9 | 79.9 | 79.9 | 79.9 | 79.9 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effict Green (s) | 15.8 | 15.8 |  | 15.8 | 15.8 |  | 82.8 | 82.8 | 82.8 | 82.8 | 82.8 |  |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.14 | 0.14 |  | 0.75 | 0.75 | 0.75 | 0.75 | 0.75 |  |
| v/c Ratio | 0.22 | 0.31 |  | 0.77 | 0.22 |  | 0.25 | 0.81 | 0.19 | 0.44 | 0.56 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

|  | $\stackrel{ }{ }$ |  |  | 7 |  |  | + | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 43.3 | 13.8 |  | 70.8 | 16.2 |  | 6.5 | 15.8 | 1.1 | 15.5 | 8.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 43.3 | 13.8 |  | 70.8 | 16.2 |  | 6.5 | 15.8 | 1.1 | 15.5 | 8.2 |  |
| LOS | D | B |  | E | B |  | A | B | A | B | A |  |
| Approach Delay |  | 22.9 |  |  | 54.2 |  |  | 12.8 |  |  | 8.8 |  |
| Approach LOS |  | C |  |  | D |  |  | B |  |  | A |  |
| Queue Length 50th (m) | 7.9 | 1.8 |  | 29.8 | 2.0 |  | 7.0 | 147.8 | 1.0 | 5.7 | 63.8 |  |
| Queue Length 95th (m) | 18.2 | 15.9 |  | \#55.9 | 13.7 |  | 14.5 | 225.0 | 7.0 | 19.1 | 93.0 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 217 | 330 |  | 217 | 318 |  | 448 | 1422 | 1277 | 174 | 1368 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.19 | 0.28 |  | 0.67 | 0.20 |  | 0.25 | 0.81 | 0.19 | 0.44 | 0.56 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 110
Actuated Cycle Length: 110.7
Natural Cycle: 90
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.81
Intersection Signal Delay: $15.3 \quad$ Intersection LOS: B
Intersection Capacity Utilization 92.1\%
ICU Level of Service $F$
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Whalfintiffe $\mathbb{R} 202 B$ BBattkground Traffic W3 Sunset Creek

PM Peak Hour

|  | 4 |  |  |  |  |  |  | 4 |  |  |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | \% | $\hat{1}$ |  | ${ }^{7}$ | $\uparrow$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 169 | 824 | 50 | 132 | 887 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Future Volume (vph) | 169 | 824 | 50 | 132 | 887 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.98 |  |
| Frt |  | 0.991 |  |  | 0.981 |  |  | 0.902 |  |  | 0.892 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1848 | 0 | 1772 | 1868 | 0 | 1825 | 1689 | 0 | 1825 | 1683 | 0 |
| Flt Permitted | 0.131 |  |  | 0.209 |  |  | 0.466 |  |  | 0.603 |  |  |
| Satd. Flow (perm) | 252 | 1848 | 0 | 390 | 1868 | 0 | 892 | 1689 | 0 | 1158 | 1683 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  | 15 |  |  | 90 |  |  | 121 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 184 | 896 | 54 | 143 | 964 | 143 | 45 | 50 | 95 | 125 | 54 | 138 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 184 | 950 | 0 | 143 | 1107 | 0 | 45 | 145 | 0 | 125 | 192 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 |  | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 70.0 | 70.0 |  | 70.0 | 70.0 |  | 30.0 | 30.0 |  | 30.0 | 30.0 |  |
| Total Split (\%) | 70.0\% | 70.0\% |  | 70.0\% | 70.0\% |  | 30.0\% | 30.0\% |  | 30.0\% | 30.0\% |  |
| Maximum Green (s) | 63.9 | 63.9 |  | 63.9 | 63.9 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 |  | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | C-Max | C-Max |  | C-Max | C-Max |  | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | - | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Efftt Green (s) | 72.6 | 72.6 |  | 72.6 | 72.6 |  | 15.3 | 15.3 |  | 15.3 | 15.3 |  |
| Actuated g/C Ratio | 0.73 | 0.73 |  | 0.73 | 0.73 |  | 0.15 | 0.15 |  | 0.15 | 0.15 |  |
| v/c Ratio | 1.01 | 0.71 |  | 0.51 | 0.81 |  | 0.33 | 0.43 |  | 0.71 | 0.53 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfinatiffe ReazBSBattkground Traffic
W3 Sunset Creek


Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


| R |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 47 | 77 | 29 | 129 | 57 | 146 | 67 | 703 | 196 | 185 | 632 | 49 |
| Future Volume (vph) | 47 | 77 | 29 | 129 | 57 | 146 | 67 | 703 | 196 | 185 | 632 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 |  |  |  |  | 0.99 | 1.00 |  |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  |  | 0.850 |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1697 | 0 | 1674 | 1671 | 1432 | 1615 | 1762 | 1585 | 1674 | 1792 | 0 |
| Flt Permitted | 0.715 |  |  | 0.507 |  |  | 0.290 |  |  | 0.277 |  |  |
| Satd. Flow (perm) | 1260 | 1697 | 0 | 889 | 1671 | 1432 | 493 | 1762 | 1562 | 488 | 1792 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 14 |  |  |  | 164 |  |  | 175 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 53 | 87 | 33 | 145 | 64 | 164 | 75 | 790 | 220 | 208 | 710 | 55 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 53 | 120 | 0 | 145 | 64 | 164 | 75 | 790 | 220 | 208 | 765 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 |  |
| Total Split (s) | 37.0 | 37.0 |  | 8.0 | 45.0 | 45.0 | 85.0 | 85.0 | 85.0 | 85.0 | 85.0 |  |
| Total Split (\%) | 28.5\% | 28.5\% |  | 6.2\% | 34.6\% | 34.6\% | 65.4\% | 65.4\% | 65.4\% | 65.4\% | 65.4\% |  |
| Maximum Green (s) | 30.8 | 30.8 |  | 5.0 | 38.8 | 38.8 | 79.1 | 79.1 | 79.1 | 79.1 | 79.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 12.3 | 12.3 |  | 23.5 | 20.3 | 20.3 | 79.2 | 79.2 | 79.2 | 79.2 | 79.2 |  |
| Actuated g/C Ratio | 0.11 | 0.11 |  | 0.21 | 0.18 | 0.18 | 0.71 | 0.71 | 0.71 | 0.71 | 0.71 |  |
| v/c Ratio | 0.38 | 0.60 |  | 0.65 | 0.21 | 0.42 | 0.21 | 0.63 | 0.19 | 0.60 | 0.60 |  |



3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2033) Background Traffic W3 Sunset Creek

|  | $\rangle$ |  |  | 7 |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ | 「 | \% | $\hat{F}$ |  | ${ }_{1}$ | $\hat{+}$ |  |
| Traffic Volume (vph) | 26 | 0 | 13 | 49 | 0 | 157 | , | 651 | 26 | 47 | 772 | 8 |
| Future Volume (vph) | 26 | 0 | 13 | 49 | 0 | 157 | 2 | 651 | 26 | 47 | 772 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 1.00 |  |  |  |  |  |  |  |
| Frt |  | 0.955 |  |  |  | 0.850 |  | 0.994 |  |  | 0.998 |  |
| Flt Protected |  | 0.968 |  |  | 0.950 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1717 | 0 | 0 | 1825 | 1633 | 1825 | 1805 | 0 | 1825 | 1860 | 0 |
| FIt Permitted |  | 0.765 |  |  | 0.728 |  | 0.225 |  |  | 0.291 |  |  |
| Satd. Flow (perm) | 0 | 1357 | 0 | 0 | 1397 | 1633 | 432 | 1805 | 0 | 559 | 1860 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 41 |  |  |  | 148 |  | 4 |  |  | 1 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 8\% | 0\% | 0\% | 0\% | 0\% | 6\% | 0\% | 0\% | 3\% | 12\% |
| Adj. Flow (vph) | 30 | 0 | 15 | 56 | 0 | 178 | 2 | 740 | 30 | 53 | 877 | 9 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 45 | 0 | 0 | 56 | 178 | 2 | 770 | 0 | 53 | 886 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | - |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 34.3 | 34.3 |  | 34.3 | 34.3 | 34.3 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 45.0 | 45.0 |  | 45.0 | 45.0 |  |
| Total Split (\%) | 43.8\% | 43.8\% |  | 43.8\% | 43.8\% | 43.8\% | 56.3\% | 56.3\% |  | 56.3\% | 56.3\% |  |
| Maximum Green (s) | 28.7 | 28.7 |  | 28.7 | 28.7 | 28.7 | 39.0 | 39.0 |  | 39.0 | 39.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 21.0 | 21.0 |  | 21.0 | 21.0 | 21.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Efftt Green (s) |  | 8.1 |  |  | 8.1 | 8.1 | 41.8 | 41.8 |  | 41.8 | 41.8 |  |
| Actuated g/C Ratio |  | 0.13 |  |  | 0.13 | 0.13 | 0.67 | 0.67 |  | 0.67 | 0.67 |  |
| v/c Ratio |  | 0.21 |  |  | 0.31 | 0.52 | 0.01 | 0.63 |  | 0.14 | 0.71 |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2033) Background Traffic W3 Sunset Creek

AM Peak Hour (With Modifications)

| 4 |  |  |  |  | 4 | + | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 11.8 |  |  | 27.6 | 12.8 | 4.5 | 9.4 |  | 5.5 | 11.2 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 11.8 |  |  | 27.6 | 12.8 | 4.5 | 9.4 |  | 5.5 | 11.2 |  |
| LOS | B |  |  | C | B | A | A |  | A | B |  |
| Approach Delay | 11.8 |  |  | 16.3 |  |  | 9.4 |  |  | 10.8 |  |
| Approach LOS | B |  |  | B |  |  | A |  |  | B |  |
| Queue Length 50th (m) | 0.4 |  |  | 5.6 | 2.9 | 0.1 | 39.6 |  | 1.7 | 50.0 |  |
| Queue Length 95th (m) | 7.4 |  |  | 13.9 | 16.4 | 0.7 | 79.7 |  | 6.1 | 101.4 |  |
| Internal Link Dist ( $m$ ) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length ( m ) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 651 |  |  | 647 | 836 | 290 | 1213 |  | 375 | 1249 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.07 |  |  | 0.09 | 0.21 | 0.01 | 0.63 |  | 0.14 | 0.71 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 62.3 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.71 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 10.9 |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 65.9\% |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive
W3 Sunset Creek

Future (2033) Background Traffic
AM Peak Hour (With Modifications)

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 566 | 53 | 26 | 780 | 32 |
| Future Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 566 | 53 | 26 | 780 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.856 |  |  | 0.862 |  |  |  | 0.850 |  | 0.994 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1541 | 0 | 1825 | 1656 | 0 | 1690 | 1746 | 1633 | 1825 | 1793 | 0 |
| Fit Permitted | 0.699 |  |  | 0.688 |  |  | 0.170 |  |  | 0.341 |  |  |
| Satd. Flow (perm) | 1304 | 1541 | 0 | 1322 | 1656 | 0 | 302 | 1746 | 1633 | 655 | 1793 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 103 |  |  | 83 |  |  |  | 60 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 3\% | 0\% | 7\% | 0\% | 0\% | 0\% | 8\% | 10\% | 0\% | 0\% | 6\% | 19\% |
| Adj. Flow (vph) | 46 | 4 | 103 | 239 | 7 | 83 | 67 | 636 | 60 | 29 | 876 | 36 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 46 | 107 | 0 | 239 | 90 | 0 | 67 | 636 | 60 | 29 | 912 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 55.0 | 55.0 | 55.0 | 55.0 | 55.0 |  |
| Total Split (\%) | 31.3\% | 31.3\% |  | 31.3\% | 31.3\% |  | 68.8\% | 68.8\% | 68.8\% | 68.8\% | 68.8\% |  |
| Maximum Green (s) | 19.3 | 19.3 |  | 19.3 | 19.3 |  | 48.6 | 48.6 | 48.6 | 48.6 | 48.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 17.4 | 17.4 |  | 17.4 | 17.4 |  | 49.8 | 49.8 | 49.8 | 49.8 | 49.8 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 |  |
| v/c Ratio | 0.16 | 0.26 |  | 0.83 | 0.21 |  | 0.35 | 0.58 | 0.06 | 0.07 | 0.81 |  |
| Control Delay | 25.7 | 7.7 |  | 53.5 | 8.4 |  | 14.5 | 11.8 | 2.1 | 7.0 | 19.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe RroatBSBattkground Traffic W3 Sunset Creek

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  | \% | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 64 | 616 | 43 | 187 | 702 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Future Volume (vph) | 64 | 616 | 43 | 187 | 702 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  |  | 0.98 | 0.98 | 0.98 |  | 1.00 | 0.96 |  |
| Frt |  | 0.990 |  |  |  | 0.850 |  | 0.888 |  |  | 0.880 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1810 | 0 | 1738 | 1812 | 1541 | 1789 | 1572 | 0 | 1674 | 1436 | 0 |
| Flt Permitted | 0.204 |  |  | 0.236 |  |  | 0.639 |  |  | 0.193 |  |  |
| Satd. Flow (perm) | 370 | 1810 | 0 | 432 | 1812 | 1506 | 1178 | 1572 | 0 | 340 | 1436 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 102 |  | 152 |  |  | 150 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 70 | 670 | 47 | 203 | 763 | 102 | 66 | 99 | 293 | 152 | 38 | 150 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 70 | 717 | 0 | 203 | 763 | 102 | 66 | 392 | 0 | 152 | 188 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 5.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 8.0 | 26.0 |  |
| Total Split (s) | 55.0 | 55.0 |  | 55.0 | 55.0 | 55.0 | 26.0 | 26.0 |  | 9.0 | 35.0 |  |
| Total Split (\%) | 61.1\% | 61.1\% |  | 61.1\% | 61.1\% | 61.1\% | 28.9\% | 28.9\% |  | 10.0\% | 38.9\% |  |
| Maximum Green (s) | 48.9 | 48.9 |  | 48.9 | 48.9 | 48.9 | 20.0 | 20.0 |  | 6.0 | 29.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.0 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 0.0 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max | Max | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  |  | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Efft Green (s) | 49.0 | 49.0 |  | 49.0 | 49.0 | 49.0 | 17.7 | 17.7 |  | 29.7 | 26.7 |  |
| Actuated g/C Ratio | 0.56 | 0.56 |  | 0.56 | 0.56 | 0.56 | 0.20 | 0.20 |  | 0.34 | 0.30 |  |
| v/c Ratio | 0.34 | 0.71 |  | 0.85 | 0.75 | 0.12 | 0.28 | 0.90 |  | 0.74 | 0.35 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe ReazBSBattkground Traffic W3 Sunset Creek

AM Peak Hour (With Modifications)

|  | 4 |  |  |  |  |  | * | 4 | \% |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 17.4 | 19.5 |  | 50.5 | 21.5 | 2.5 | 32.7 | 45.5 |  | 45.1 | 8.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 17.4 | 19.5 |  | 50.5 | 21.5 | 2.5 | 32.7 | 45.5 |  | 45.1 | 8.3 |  |
| LOS | B | B |  | D | C | A | C | D |  | D | A |  |
| Approach Delay |  | 19.3 |  |  | 25.2 |  |  | 43.6 |  |  | 24.8 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | C |  |
| Queue Length 50th (m) | 6.4 | 87.2 |  | 28.4 | 97.7 | 0.0 | 9.5 | 40.7 |  | 18.3 | 4.6 |  |
| Queue Length 95th (m) | 16.9 | 130.5 |  | \#72.2 | 146.3 | 6.6 | 20.8 | \#8.7 |  | \#41.1 | 19.4 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  | 60.0 | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 206 | 1012 |  | 240 | 1011 | 885 | 268 | 475 |  | 206 | 575 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.34 | 0.71 |  | 0.85 | 0.75 | 0.12 | 0.25 | 0.83 |  | 0.74 | 0.33 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 87.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 26.6 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 93.1\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


|  | $\rangle$ | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | $\hat{\beta}$ |  | ${ }_{1}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{*}$ | $\hat{F}$ |  |
| Traffic Volume (vph) | 54 | 85 | 49 | 241 | 104 | 308 | 65 | 893 | 200 | 174 | 690 | 53 |
| Future Volume (vph) | 54 | 85 | 49 | 241 | 104 | 308 | 65 | 893 | 200 | 174 | 690 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 0.99 |  | 0.99 |  | 0.97 | 1.00 |  | 0.98 |  | 1.00 |  |
| Frt |  | 0.945 |  |  |  | 0.850 |  |  | 0.850 |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1692 | 0 | 1825 | 1921 | 1585 | 1789 | 1883 | 1601 | 1789 | 1825 | 0 |
| Flt Permitted | 0.685 |  |  | 0.449 |  |  | 0.296 |  |  | 0.078 |  |  |
| Satd. Flow (perm) | 1254 | 1692 | 0 | 854 | 1921 | 1538 | 557 | 1883 | 1576 | 147 | 1825 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 21 |  |  |  | 196 |  |  | 111 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 57 | 90 | 52 | 256 | 111 | 328 | 69 | 950 | 213 | 185 | 734 | 56 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 57 | 142 | 0 | 256 | 111 | 328 | 69 | 950 | 213 | 185 | 790 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 8.0 | 45.9 |  |
| Total Split (s) | 36.0 | 36.0 |  | 12.0 | 48.0 | 48.0 | 71.0 | 71.0 | 71.0 | 11.0 | 82.0 |  |
| Total Split (\%) | 27.7\% | 27.7\% |  | 9.2\% | 36.9\% | 36.9\% | 54.6\% | 54.6\% | 54.6\% | 8.5\% | 63.1\% |  |
| Maximum Green (s) | 29.8 | 29.8 |  | 9.0 | 41.8 | 41.8 | 65.1 | 65.1 | 65.1 | 8.0 | 76.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.0 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 0.0 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 |  | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 |  |
| Act Effct Green (s) | 13.5 | 13.5 |  | 28.7 | 25.5 | 25.5 | 65.2 | 65.2 | 65.2 | 79.1 | 76.2 |  |
| Actuated g/C Ratio | 0.12 | 0.12 |  | 0.25 | 0.22 | 0.22 | 0.57 | 0.57 | 0.57 | 0.70 | 0.67 |  |
| v/c Ratio | 0.39 | 0.65 |  | 0.88 | 0.26 | 0.66 | 0.22 | 0.88 | 0.22 | 0.85 | 0.65 |  |


|  | 4 |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 53.5 | 54.5 |  | 68.1 | 37.6 | 22.4 | 15.2 | 33.1 | 6.7 | 52.1 | 14.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 53.5 | 54.5 |  | 68.1 | 37.6 | 22.4 | 15.2 | 33.1 | 6.7 | 52.1 | 14.7 |  |
| LOS | D | D |  | E | D | C | B | C | A | D | B |  |
| Approach Delay |  | 54.2 |  |  | 41.7 |  |  | 27.5 |  |  | 21.8 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (m) | 11.9 | 26.0 |  | 49.7 | 20.5 | 26.0 | 7.1 | 172.6 | 9.8 | 18.8 | 92.4 |  |
| Queue Length 95th (m) | 24.7 | 46.5 |  | \#86.4 | 35.5 | 56.4 | 17.4 | \#289.8 | 23.8 | \#63.4 | 152.9 |  |
| Internal Link Dist ( m ) |  | 535.5 |  |  | 981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length ( m ) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 328 | 459 |  | 292 | 706 | 689 | 318 | 1078 | 949 | 217 | 1223 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.17 | 0.31 |  | 0.88 | 0.16 | 0.48 | 0.22 | 0.88 | 0.22 | 0.85 | 0.65 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 113.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.88 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 30.6 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 95.4\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road


3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2033) Background Traffic W3 Sunset Creek

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2033) Background Traffic W3 Sunset Creek

| $\dagger$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 13.1 |  |  | 48.7 | 17.2 | 2.4 | 9.3 |  | 10.0 | 4.6 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 13.1 |  |  | 48.7 | 17.2 | 2.4 | 9.3 |  | 10.0 | 4.6 |  |
| LOS | B |  |  | D | B | A | A |  | A | A |  |
| Approach Delay | 13.1 |  |  | 22.9 |  |  | 9.3 |  |  | 5.2 |  |
| Approach LOS | B |  |  | C |  |  | A |  |  | A |  |
| Queue Length 50th (m) | 0.0 |  |  | 3.9 | 0.0 | 0.3 | 93.8 |  | 5.0 | 40.4 |  |
| Queue Length 95th (m) | 5.2 |  |  | 10.9 | 14.4 | 1.5 | 185.6 |  | 19.4 | 72.9 |  |
| Internal Link Dist ( $m$ ) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length ( m ) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 268 |  |  | 251 | 370 | 517 | 1594 |  | 250 | 1565 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.07 |  |  | 0.08 | 0.25 | 0.02 | 0.76 |  | 0.45 | 0.52 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 103.2 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.76 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.3 |  |  | Intersection LOS: A |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 91.8\% |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive
W3 Sunset Creek

Future (2033) Background Traffic
PM Peak Hour (With Modifications)

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | F |  |
| Traffic Volume (vph) | 39 | 9 | 78 | 136 | 10 | 49 | 106 | 1077 | 223 | 72 | 645 | 63 |
| Future Volume (vph) | 39 | 9 | 78 | 136 | 10 | 49 | 106 | 1077 | 223 | 72 | 645 | 63 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.98 |  | 1.00 |  |  |  |  |  |  |  |  |
| Frt |  | 0.866 |  |  | 0.876 |  |  |  | 0.850 |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1601 | 0 | 1825 | 1683 | 0 | 1825 | 1902 | 1633 | 1825 | 1826 | 0 |
| Flt Permitted | 0.715 |  |  | 0.696 |  |  | 0.302 |  |  | 0.099 |  |  |
| Satd. Flow (perm) | 1334 | 1601 | 0 | 1334 | 1683 | 0 | 580 | 1902 | 1633 | 190 | 1826 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 84 |  |  | 53 |  |  |  | 160 |  | 9 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 3\% | 0\% | 2\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 4\% | 2\% |
| Adj. Flow (vph) | 42 | 10 | 84 | 146 | 11 | 53 | 114 | 1158 | 240 | 77 | 694 | 68 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 42 | 94 | 0 | 146 | 64 | 0 | 114 | 1158 | 240 | 77 | 762 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 |  | 75.0 | 75.0 | 75.0 | 75.0 | 75.0 |  |
| Total Split (\%) | 31.8\% | 31.8\% |  | 31.8\% | 31.8\% |  | 68.2\% | 68.2\% | 68.2\% | 68.2\% | 68.2\% |  |
| Maximum Green (s) | 29.3 | 29.3 |  | 29.3 | 29.3 |  | 68.6 | 68.6 | 68.6 | 68.6 | 68.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 71.5 | 71.5 | 71.5 | 71.5 | 71.5 |  |
| Actuated g/C Ratio | 0.16 | 0.16 |  | 0.16 | 0.16 |  | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |  |
| v/c Ratio | 0.20 | 0.29 |  | 0.68 | 0.20 |  | 0.27 | 0.85 | 0.20 | 0.57 | 0.58 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

| W3 Sunset Creek |  |  |  |  |  |  |  |  | M Peak | Hour ( | h Mod | tions) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  |  | $\checkmark$ | - |  |  | $\uparrow$ | $p$ | * | $\ddagger$ | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 36.3 | 11.7 |  | 54.8 | 13.7 |  | 8.0 | 19.4 | 2.4 | 29.3 | 9.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 36.3 | 11.7 |  | 54.8 | 13.7 |  | 8.0 | 19.4 | 2.4 | 29.3 | 9.8 |  |
| LOS | D | B |  | D | B |  | A | B | A | C | A |  |
| Approach Delay |  | 19.3 |  |  | 42.3 |  |  | 15.8 |  |  | 11.6 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 6.9 | 1.6 |  | 25.9 | 1.8 |  | 6.6 | 136.5 | 3.9 | 6.0 | 59.2 |  |
| Queue Length 95th (m) | 16.1 | 14.2 |  | 45.5 | 12.2 |  | 18.2 | \#300.1 | 13.4 | \#35.2 | 115.0 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 392 | 530 |  | 392 | 532 |  | 416 | 1364 | 1217 | 136 | 1312 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.11 | 0.18 |  | 0.37 | 0.12 |  | 0.27 | 0.85 | 0.20 | 0.57 | 0.58 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 110
Actuated Cycle Length: 99.7
Natural Cycle: 90
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.85
Intersection Signal Delay: $16.7 \quad$ Intersection LOS: B
Intersection Capacity Utilization 92.1\%
ICU Level of Service $F$
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe RroatBSBattkground Traffic W3 Sunset Creek

PM Peak Hour (With Modifications)

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{\beta}$ |  | ${ }^{4}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{}$ |  | * | $\hat{\downarrow}$ |  |
| Traffic Volume (vph) | 169 | 824 | 50 | 132 | 887 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Future Volume (vph) | 169 | 824 | 50 | 132 | 887 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length ( m ) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.98 |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  | 0.902 |  |  | 0.892 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1848 | 0 | 1772 | 1902 | 1633 | 1825 | 1689 | 0 | 1825 | 1683 | 0 |
| Flt Permitted | 0.099 |  |  | 0.253 |  |  | 0.466 |  |  | 0.603 |  |  |
| Satd. Flow (perm) | 190 | 1848 | 0 | 472 | 1902 | 1633 | 892 | 1689 | 0 | 1158 | 1683 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 113 |  | 88 |  |  | 118 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 184 | 896 | 54 | 143 | 964 | 143 | 45 | 50 | 95 | 125 | 54 | 138 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 184 | 950 | 0 | 143 | 964 | 143 | 45 | 145 | 0 | 125 | 192 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 5 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 8.0 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 8.0 | 72.0 |  | 64.0 | 64.0 | 64.0 | 28.0 | 28.0 |  | 28.0 | 28.0 |  |
| Total Split (\%) | 8.0\% | 72.0\% |  | 64.0\% | 64.0\% | 64.0\% | 28.0\% | 28.0\% |  | 28.0\% | 28.0\% |  |
| Maximum Green (s) | 5.0 | 65.9 |  | 57.9 | 57.9 | 57.9 | 22.0 | 22.0 |  | 22.0 | 22.0 |  |
| Yellow Time (s) | 3.0 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 0.0 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 3.0 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C-Max |  | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) |  | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 75.7 | 72.6 |  | 60.0 | 60.0 | 60.0 | 15.3 | 15.3 |  | 15.3 | 15.3 |  |
| Actuated g/C Ratio | 0.76 | 0.73 |  | 0.60 | 0.60 | 0.60 | 0.15 | 0.15 |  | 0.15 | 0.15 |  |
| v/c Ratio | 0.61 | 0.71 |  | 0.51 | 0.85 | 0.14 | 0.33 | 0.44 |  | 0.71 | 0.54 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe RroatBSBattkground Traffic W3 Sunset Creek

PM Peak Hour (With Modifications)

|  |  |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 20.1 | 12.6 |  | 20.2 | 25.8 | 3.2 | 42.3 | 19.6 |  | 60.3 | 20.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 20.1 | 12.6 |  | 20.2 | 25.8 | 3.2 | 42.3 | 19.6 |  | 60.3 | 20.7 |  |
| LOS | C | B |  | C | C | A | D | B |  | E | C |  |
| Approach Delay |  | 13.8 |  |  | 22.6 |  |  | 25.0 |  |  | 36.3 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | D |  |
| Queue Length 50th (m) | 7.9 | 88.2 |  | 15.6 | 149.1 | 2.3 | 7.9 | 9.8 |  | 23.3 | 12.9 |  |
| Queue Length 95th (m) | \#32.8 | 171.3 |  | 35.7 | \#240.3 | 10.1 | 17.1 | 25.2 |  | 39.5 | 31.0 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  | 60.0 | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 300 | 1342 |  | 283 | 1140 | 1024 | 196 | 440 |  | 254 | 462 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.61 | 0.71 |  | 0.51 | 0.85 | 0.14 | 0.23 | 0.33 |  | 0.49 | 0.42 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 32 (32\%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.85 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 20.8 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 91.3\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\uparrow$ | 「 | * | $\uparrow$ | 「 | ${ }^{1}$ | F |  |
| Traffic Volume (vph) | 50 | 82 | 30 | 137 | 61 | 155 | 70 | 727 | 207 | 196 | 666 | 53 |
| Future Volume (vph) | 50 | 82 | 30 | 137 | 61 | 155 | 70 | 727 | 207 | 196 | 666 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 |  |  |  |  | 0.99 | 1.00 |  |  |
| Frt |  | 0.960 |  |  |  | 0.850 |  |  | 0.850 |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1701 | 0 | 1674 | 1671 | 1432 | 1615 | 1762 | 1585 | 1674 | 1792 | 0 |
| Flt Permitted | 0.712 |  |  | 0.494 |  |  | 0.260 |  |  | 0.255 |  |  |
| Satd. Flow (perm) | 1255 | 1701 | 0 | 866 | 1671 | 1432 | 442 | 1762 | 1562 | 449 | 1792 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 14 |  |  |  | 174 |  |  | 173 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 56 | 92 | 34 | 154 | 69 | 174 | 79 | 817 | 233 | 220 | 748 | 60 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 56 | 126 | 0 | 154 | 69 | 174 | 79 | 817 | 233 | 220 | 808 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 |  |
| Total Split (s) | 38.0 | 38.0 |  | 9.0 | 47.0 | 47.0 | 83.0 | 83.0 | 83.0 | 83.0 | 83.0 |  |
| Total Split (\%) | 29.2\% | 29.2\% |  | 6.9\% | 36.2\% | 36.2\% | 63.8\% | 63.8\% | 63.8\% | 63.8\% | 63.8\% |  |
| Maximum Green (s) | 31.8 | 31.8 |  | 6.0 | 40.8 | 40.8 | 77.1 | 77.1 | 77.1 | 77.1 | 77.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 12.6 | 12.6 |  | 24.8 | 21.6 | 21.6 | 77.2 | 77.2 | 77.2 | 77.2 | 77.2 |  |
| Actuated g/C Ratio | 0.11 | 0.11 |  | 0.22 | 0.19 | 0.19 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |  |
| v/c Ratio | 0.39 | 0.61 |  | 0.65 | 0.21 | 0.42 | 0.26 | 0.67 | 0.20 | 0.71 | 0.65 |  |


|  | 4 |  |  |  |  |  | + | $\dagger$ | \% |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 53.4 | 54.4 |  | 51.0 | 38.8 | 8.7 | 9.6 | 13.6 | 2.4 | 26.6 | 12.9 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 53.4 | 54.4 |  | 51.0 | 38.8 | 8.7 | 9.6 | 13.6 | 2.4 | 26.6 | 12.9 |  |
| LOS | D | D |  | D | D | A | A | B | A | C | B |  |
| Approach Delay |  | 54.1 |  |  | 30.3 |  |  | 11.0 |  |  | 15.9 |  |
| Approach LOS |  | D |  |  | C |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 11.4 | 23.3 |  | 28.7 | 12.6 | 0.0 | 5.6 | 89.3 | 3.7 | 25.2 | 85.5 |  |
| Queue Length 95th (m) | 23.5 | 41.8 |  | 47.1 | 24.6 | 16.7 | 14.7 | 48.1 | 12.4 | \#79.8 | 141.2 |  |
| Internal Link Dist ( m ) |  | 535.5 |  |  | 981.5 |  |  | 45.6 |  |  | 472.5 |  |
| Turn Bay Length ( m ) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 360 | 498 |  | 237 | 615 | 637 | 307 | 1226 | 1139 | 312 | 1248 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.16 | 0.25 |  | 0.65 | 0.11 | 0.27 | 0.26 | 0.67 | 0.20 | 0.71 | 0.65 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 110.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.71 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 18.5 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 78.4\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road




| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 280 | 0 | 0.1 | 0 |
| HCM LOS | F | A |  |  |


| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1 EBLn2WBLn1 | SBL | SBT | SBR |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 673 | - | - | 42 | 282 | - | 700 | - |
| HCM Lane V/C Ratio | 0.021 | - | - | 1.44 | 0.136 | - | - | - |
| HCM Control Delay (s) | 10.5 | - | $-\$ 445.2$ | 19.8 | 0 | 0 | - | - |
| HCM Lane LOS | B | - | - | F | C | A | A | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | 6.1 | 0.5 | - | 0 | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

## 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2038) Background Traffic W3 Sunset Creek <br> AM Peak Hour

|  | 4 |  |  | 7 |  |  | $4$ | 9 | $p$ | $t$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 26 | 0 | 13 | 49 | 0 | 157 | 2 | 684 | 26 | 47 | 815 | 8 |
| Future Volume (vph) | 26 | 0 | 13 | 49 | 0 | 157 | 2 | 684 | 26 | 47 | 815 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 1.00 |  |  |  |  |  |  |  |
| Frt |  | 0.955 |  |  |  | 0.850 |  | 0.994 |  |  | 0.999 |  |
| Flt Protected |  | 0.968 |  |  | 0.950 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1717 | 0 | 0 | 1825 | 1633 | 1825 | 1805 | 0 | 1825 | 1862 | 0 |
| Flt Permitted |  | 0.765 |  |  | 0.728 |  | 0.196 |  |  | 0.269 |  |  |
| Satd. Flow (perm) | 0 | 1357 | 0 | 0 | 1397 | 1633 | 377 | 1805 | 0 | 517 | 1862 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 41 |  |  |  | 133 |  | 3 |  |  | 1 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 8\% | 0\% | 0\% | 0\% | 0\% | 6\% | 0\% | 0\% | 3\% | 12\% |
| Adj. Flow (vph) | 30 | 0 | 15 | 56 | 0 | 178 | 2 | 777 | 30 | 53 | 926 | 9 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 45 | 0 | 0 | 56 | 178 | 2 | 807 | 0 | 53 | 935 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 34.3 | 34.3 |  | 34.3 | 34.3 | 34.3 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 45.0 | 45.0 |  | 45.0 | 45.0 |  |
| Total Split (\%) | 43.8\% | 43.8\% |  | 43.8\% | 43.8\% | 43.8\% | 56.3\% | 56.3\% |  | 56.3\% | 56.3\% |  |
| Maximum Green (s) | 28.7 | 28.7 |  | 28.7 | 28.7 | 28.7 | 39.0 | 39.0 |  | 39.0 | 39.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 21.0 | 21.0 |  | 21.0 | 21.0 | 21.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 8.2 |  |  | 8.2 | 8.2 | 41.8 | 41.8 |  | 41.8 | 41.8 |  |
| Actuated g/C Ratio |  | 0.13 |  |  | 0.13 | 0.13 | 0.67 | 0.67 |  | 0.67 | 0.67 |  |
| v/c Ratio |  | 0.21 |  |  | 0.30 | 0.54 | 0.01 | 0.67 |  | 0.15 | 0.75 |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2038) Background Traffic W3 Sunset Creek

|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

Future (2038) Background Traffic
AM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 43 | 4 | 97 | 213 | 6 | 74 | 64 | 597 | 53 | 26 | 823 | 34 |
| Future Volume (vph) | 43 | 4 | 97 | 213 | 6 | 74 | 64 | 597 | 53 | 26 | 823 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.855 |  |  | 0.862 |  |  |  | 0.850 |  | 0.994 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1539 | 0 | 1825 | 1656 | 0 | 1690 | 1746 | 1633 | 1825 | 1793 | 0 |
| Fit Permitted | 0.699 |  |  | 0.684 |  |  | 0.139 |  |  | 0.318 |  |  |
| Satd. Flow (perm) | 1304 | 1539 | 0 | 1314 | 1656 | 0 | 247 | 1746 | 1633 | 611 | 1793 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 109 |  |  | 83 |  |  |  | 60 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 3\% | 0\% | 7\% | 0\% | 0\% | 0\% | 8\% | 10\% | 0\% | 0\% | 6\% | 19\% |
| Adj. Flow (vph) | 48 | 4 | 109 | 239 | 7 | 83 | 72 | 671 | 60 | 29 | 925 | 38 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 48 | 113 | 0 | 239 | 90 | 0 | 72 | 671 | 60 | 29 | 963 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 55.0 | 55.0 | 55.0 | 55.0 | 55.0 |  |
| Total Split (\%) | 31.3\% | 31.3\% |  | 31.3\% | 31.3\% |  | 68.8\% | 68.8\% | 68.8\% | 68.8\% | 68.8\% |  |
| Maximum Green (s) | 19.3 | 19.3 |  | 19.3 | 19.3 |  | 48.6 | 48.6 | 48.6 | 48.6 | 48.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 17.4 | 17.4 |  | 17.4 | 17.4 |  | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 |  |
| v/c Ratio | 0.17 | 0.27 |  | 0.83 | 0.21 |  | 0.46 | 0.61 | 0.06 | 0.08 | 0.85 |  |
| Control Delay | 25.8 | 7.6 |  | 53.8 | 8.4 |  | 21.2 | 12.5 | 2.1 | 7.1 | 22.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

| W3 Sunset Cre |  |  |  |  |  |  |  |  |  |  | AM | Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ |  | $\downarrow$ |  |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\dagger$ | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | 25.8 | 7.6 |  | 53.8 | 8.4 |  | 21.2 | 12.5 | 2.1 | 7.1 | 22.3 |  |
| LOS | C | A |  | D | A |  | C | B | A | A | C |  |
| Approach Delay |  | 13.0 |  |  | 41.4 |  |  | 12.5 |  |  | 21.9 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 5.8 | 0.5 |  | 33.7 | 0.8 |  | 5.5 | 58.4 | 0.0 | 1.6 | 111.0 |  |
| Queue Length 95th (m) | 13.9 | 11.8 |  | \#66.3 | 11.1 |  | 19.8 | 89.5 | 3.9 | 4.8 | \#197.9 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 317 | 457 |  | 320 | 466 |  | 155 | 1095 | 1046 | 383 | 1127 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.25 |  | 0.75 | 0.19 |  | 0.46 | 0.61 | 0.06 | 0.08 | 0.85 |  |

## Intersection Summary <br> Area Type: Other

Cycle Length: 80
Actuated Cycle Length: 79.2
Natural Cycle: 80
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.85
Intersection Signal Delay: 20.8
Intersection LOS: C
Intersection Capacity Utilization 81.7\% ICU Level of Service D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive

 W3 Sunset Creek

| L |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 64 | 648 | 43 | 187 | 746 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Future Volume (vph) | 64 | 648 | 43 | 187 | 746 | 94 | 61 | 91 | 270 | 140 | 35 | 138 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  |  | 0.98 | 0.98 | 0.98 |  | 1.00 | 0.96 |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  | 0.888 |  |  | 0.880 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1812 | 0 | 1738 | 1812 | 1541 | 1789 | 1572 | 0 | 1674 | 1436 | 0 |
| Flt Permitted | 0.181 |  |  | 0.221 |  |  | 0.639 |  |  | 0.193 |  |  |
| Satd. Flow (perm) | 328 | 1812 | 0 | 404 | 1812 | 1506 | 1178 | 1572 | 0 | 340 | 1436 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 100 |  | 152 |  |  | 150 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 70 | 704 | 47 | 203 | 811 | 102 | 66 | 99 | 293 | 152 | 38 | 150 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 70 | 751 | 0 | 203 | 811 | 102 | 66 | 392 | 0 | 152 | 188 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 5.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 8.0 | 26.0 |  |
| Total Split (s) | 56.0 | 56.0 |  | 56.0 | 56.0 | 56.0 | 26.0 | 26.0 |  | 8.0 | 34.0 |  |
| Total Split (\%) | 62.2\% | 62.2\% |  | 62.2\% | 62.2\% | 62.2\% | 28.9\% | 28.9\% |  | 8.9\% | 37.8\% |  |
| Maximum Green (s) | 49.9 | 49.9 |  | 49.9 | 49.9 | 49.9 | 20.0 | 20.0 |  | 5.0 | 28.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.0 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 0.0 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max | Max | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  |  | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Effct Green (s) | 50.0 | 50.0 |  | 50.0 | 50.0 | 50.0 | 17.7 | 17.7 |  | 28.7 | 25.7 |  |
| Actuated g/C Ratio | 0.57 | 0.57 |  | 0.57 | 0.57 | 0.57 | 0.20 | 0.20 |  | 0.33 | 0.29 |  |
| v/c Ratio | 0.38 | 0.73 |  | 0.89 | 0.79 | 0.11 | 0.28 | 0.90 |  | 0.81 | 0.36 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe ReatBSBattkground Traffic W3 Sunset Creek

|  | 4 | $\rightarrow$ |  |  |  |  | , | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 18.8 | 19.5 |  | 58.2 | 22.4 | 2.5 | 32.7 | 45.5 |  | 57.0 | 8.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 18.8 | 19.5 |  | 58.2 | 22.4 | 2.5 | 32.7 | 45.5 |  | 57.0 | 8.7 |  |
| LOS | B | B |  | E | C | A | C | D |  | E | A |  |
| Approach Delay |  | 19.5 |  |  | 27.1 |  |  | 43.6 |  |  | 30.3 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | C |  |
| Queue Length 50th (m) | 6.4 | 91.5 |  | 29.4 | 105.7 | 0.2 | 9.5 | 40.7 |  | 18.7 | 4.6 |  |
| Queue Length 95th (m) | 17.9 | 137.1 |  | \#74.1 | 159.5 | 6.6 | 20.8 | \#88.7 |  | \#45.5 | 19.7 |  |
| Internal Link Dist ( $m$ ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  | 60.0 | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 186 | 1034 |  | 229 | 1031 | 900 | 268 | 475 |  | 187 | 561 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.38 | 0.73 |  | 0.89 | 0.79 | 0.11 | 0.25 | 0.83 |  | 0.81 | 0.34 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 87.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 28.0 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 94.8\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{1}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{*}$ | F |  |
| Traffic Volume (vph) | 57 | 90 | 52 | 254 | 110 | 326 | 68 | 938 | 212 | 184 | 717 | 57 |
| Future Volume (vph) | 57 | 90 | 52 | 254 | 110 | 326 | 68 | 938 | 212 | 184 | 717 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 0.99 |  | 0.99 |  | 0.97 | 1.00 |  | 0.98 |  | 1.00 |  |
| Frt |  | 0.945 |  |  |  | 0.850 |  |  | 0.850 |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1692 | 0 | 1825 | 1921 | 1585 | 1789 | 1883 | 1601 | 1789 | 1825 | 0 |
| Flt Permitted | 0.682 |  |  | 0.403 |  |  | 0.278 |  |  | 0.054 |  |  |
| Satd. Flow (perm) | 1249 | 1692 | 0 | 767 | 1921 | 1538 | 523 | 1883 | 1576 | 102 | 1825 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 19 |  |  |  | 218 |  |  | 123 |  | 6 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 61 | 96 | 55 | 270 | 117 | 347 | 72 | 998 | 226 | 196 | 763 | 61 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 61 | 151 | 0 | 270 | 117 | 347 | 72 | 998 | 226 | 196 | 824 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 8.0 | 45.9 |  |
| Total Split (s) | 26.0 | 26.0 |  | 14.0 | 40.0 | 40.0 | 77.0 | 77.0 | 77.0 | 13.0 | 90.0 |  |
| Total Split (\%) | 20.0\% | 20.0\% |  | 10.8\% | 30.8\% | 30.8\% | 59.2\% | 59.2\% | 59.2\% | 10.0\% | 69.2\% |  |
| Maximum Green (s) | 19.8 | 19.8 |  | 11.0 | 33.8 | 33.8 | 71.1 | 71.1 | 71.1 | 10.0 | 84.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.0 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 0.0 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 |  | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | , | 0 |  | 0 |  |
| Act Effict Green (s) | 14.7 | 14.7 |  | 31.9 | 28.7 | 28.7 | 71.1 | 71.1 | 71.1 | 87.1 | 84.2 |  |
| Actuated g/C Ratio | 0.12 | 0.12 |  | 0.26 | 0.23 | 0.23 | 0.57 | 0.57 | 0.57 | 0.70 | 0.67 |  |
| v/c Ratio | 0.41 | 0.70 |  | 0.93 | 0.27 | 0.67 | 0.24 | 0.93 | 0.24 | 0.95 | 0.67 |  |


|  | $\rangle$ |  |  |  |  |  |  | $\uparrow$ | $p$ | $\checkmark$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 59.5 | 63.5 |  | 81.7 | 40.8 | 22.3 | 17.2 | 41.4 | 7.0 | 83.5 | 16.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 59.5 | 63.5 |  | 81.7 | 40.8 | 22.3 | 17.2 | 41.4 | 7.0 | 83.5 | 16.1 |  |
| LOS | E | E |  | F | D | C | B | D | A | F | B |  |
| Approach Delay |  | 62.3 |  |  | 47.1 |  |  | 34.0 |  |  | 29.1 |  |
| Approach LOS |  | E |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (m) | 14.1 | 31.6 |  | 58.2 | 23.7 | 28.2 | 8.5 | 216.3 | 11.2 | 32.2 | 110.7 |  |
| Queue Length 95th (m) | 28.1 | 53.7 |  | \#105.9 | 40.2 | 60.8 | 19.5 | \#334.8 | 25.7 | \#83.1 | 171.3 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 198 | 284 |  | 289 | 519 | 575 | 297 | 1071 | 949 | 206 | 1230 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.31 | 0.53 |  | 0.93 | 0.23 | 0.60 | 0.24 | 0.93 | 0.24 | 0.95 | 0.67 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 37.3 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.4\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2304 | 2304 | 976 | 2317 | 2332 | 1258 | 1004 | 0 | 0 | 1258 | 0 | 0 |
| Stage 1 | 976 | 976 | - | 1328 | 1328 | - | - | - |  | - | - | - |
| Stage 2 | 1328 | 1328 | - | 989 | 1004 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.24 | 7.1 | 6.5 | 6.2 | 4.13 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.336 | 3.5 | 4 | 3.3 | 2.227 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | ~ 27 | 39 | 302 | 27 | 37 | 211 | 686 | - | - | 560 | - | - |
| Stage 1 | 305 | 332 | - | 193 | 226 | - | - | - | - | - | - | - |
| Stage 2 | 193 | 226 | - | 300 | 322 | - | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | $\sim 26$ | 37 | 302 | 24 | 35 | 211 | 686 | - | - | 560 | - | - |
| Mov Cap-2 Maneuver | $\sim 26$ | 37 | - | 24 | 35 | - | - | - | - | - | - | - |
| Stage 1 | 289 | 332 | - | 183 | 214 | - | - | - | - | - | - | - |
| Stage 2 | 183 | 214 | - | 275 | 322 | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 282 |  |  | 0 |  |  | 0.3 |  |  | 0 |  |  |
| HCM LOS | F |  |  | A |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | EBLn2W | VBLn1 | SBL | SBT | SBR |  |  |
| Capacity (veh/h) |  | 686 | - | - | 26 | 302 | - | 560 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.051 | - | - | 1.255 | 0.084 | - | - | - | - |  |  |
| HCM Control Delay (s) |  | 10.5 | - |  | 486.3 | 18 | 0 | 0 | - | - |  |  |
| HCM Lane LOS |  | B | - | - | F | C | A | A | - | - |  |  |
| HCM 95th \%tile Q(veh |  | 0.2 | - | - | 3.9 | 0.3 | - | 0 | - | - |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2038) Background Traffic
W3 Sunset Creek

|  | 4 | $\rightarrow$ | \% | 7 |  |  | 4 | $\dagger$ |  | 4 | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\uparrow$ | T | ${ }^{7}$ | 个 |  | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 13 | 0 | 6 | 17 | 2 | 86 | 10 | 1129 | 83 | 106 | 792 | 26 |
| Future Volume (vph) | 13 | 0 | 6 | 17 | 2 | 86 | 10 | 1129 | 83 | 106 | 792 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  |  |  |  |  | 1.00 |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  | 0.990 |  |  | 0.995 |  |
| Flt Protected |  | 0.966 |  |  | 0.957 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1666 | 0 | 0 | 1839 | 1633 | 1825 | 1884 | 0 | 1825 | 1849 | 0 |
| Flt Permitted |  | 0.779 |  |  | 0.733 |  | 0.300 |  |  | 0.128 |  |  |
| Satd. Flow (perm) | 0 | 1344 | 0 | 0 | 1386 | 1633 | 576 | 1884 | 0 | 246 | 1849 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 30 |  |  |  | 91 |  | 9 |  |  | 4 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 6 | 6 |  |  | 28 |  |  |  |  | 28 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 8\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 3\% | 4\% |
| Adj. Flow (vph) | 14 | 0 | 6 | 18 | 2 | 91 | 11 | 1188 | 87 | 112 | 834 | 27 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 20 | 0 | 0 | 20 | 91 | 11 | 1275 | 0 | 112 | 861 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.3 | 24.3 |  | 24.3 | 24.3 | 24.3 | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 85.0 | 85.0 |  | 85.0 | 85.0 |  |
| Total Split (\%) | 22.7\% | 22.7\% |  | 22.7\% | 22.7\% | 22.7\% | 77.3\% | 77.3\% |  | 77.3\% | 77.3\% |  |
| Maximum Green (s) | 18.7 | 18.7 |  | 18.7 | 18.7 | 18.7 | 79.0 | 79.0 |  | 79.0 | 79.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 7.2 |  |  | 7.2 | 7.2 | 87.3 | 87.3 |  | 87.3 | 87.3 |  |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.07 | 0.07 | 0.85 | 0.85 |  | 0.85 | 0.85 |  |
| v/c Ratio |  | 0.17 |  |  | 0.21 | 0.46 | 0.02 | 0.80 |  | 0.54 | 0.55 |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Aveffutere (2038) Background Traffic W3 Sunset Creek

| 4 |  |  |  |  |  | , | 4 | $p$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 13.1 |  |  | 48.7 | 17.2 | 2.4 | 11.0 |  | 15.8 | 4.9 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 13.1 |  |  | 48.7 | 17.2 | 2.4 | 11.0 |  | 15.8 | 4.9 |  |
| LOS | B |  |  | D | B | A | B |  | B | A |  |
| Approach Delay | 13.1 |  |  | 22.9 |  |  | 10.9 |  |  | 6.1 |  |
| Approach LOS | B |  |  | C |  |  | B |  |  | A |  |
| Queue Length 50th (m) | 0.0 |  |  | 3.9 | 0.0 | 0.3 | 108.5 |  | 5.7 | 44.3 |  |
| Queue Length 95th (m) | 5.2 |  |  | 10.9 | 14.4 | 1.5 | 222.7 |  | \#33.0 | 79.8 |  |
| Internal Link Dist (m) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length (m) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 268 |  |  | 251 | 370 | 487 | 1595 |  | 208 | 1565 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.07 |  |  | 0.08 | 0.25 | 0.02 | 0.80 |  | 0.54 | 0.55 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 103.2 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.80 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 9.5 |  |  |  | Intersection LOS: A |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 94.8\% ICU Level of Service FAnalysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

Future (2038) Background Traffic
PM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | F |  |
| Traffic Volume (vph) | 41 | 9 | 83 | 136 | 10 | 49 | 112 | 1134 | 223 | 72 | 681 | 67 |
| Future Volume (vph) | 41 | 9 | 83 | 136 | 10 | 49 | 112 | 1134 | 223 | 72 | 681 | 67 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.98 |  | 1.00 |  |  |  |  |  |  |  |  |
| Frt |  | 0.865 |  |  | 0.876 |  |  |  | 0.850 |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1599 | 0 | 1825 | 1683 | 0 | 1825 | 1902 | 1633 | 1825 | 1826 | 0 |
| Flt Permitted | 0.715 |  |  | 0.693 |  |  | 0.284 |  |  | 0.075 |  |  |
| Satd. Flow (perm) | 1334 | 1599 | 0 | 1328 | 1683 | 0 | 546 | 1902 | 1633 | 144 | 1826 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 89 |  |  | 53 |  |  |  | 178 |  | 10 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 3\% | 0\% | 2\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 4\% | 2\% |
| Adj. Flow (vph) | 44 | 10 | 89 | 146 | 11 | 53 | 120 | 1219 | 240 | 77 | 732 | 72 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 44 | 99 | 0 | 146 | 64 | 0 | 120 | 1219 | 240 | 77 | 804 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 29.0 | 29.0 |  | 29.0 | 29.0 |  | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 |  |
| Total Split (\%) | 26.4\% | 26.4\% |  | 26.4\% | 26.4\% |  | 73.6\% | 73.6\% | 73.6\% | 73.6\% | 73.6\% |  |
| Maximum Green (s) | 23.3 | 23.3 |  | 23.3 | 23.3 |  | 74.6 | 74.6 | 74.6 | 74.6 | 74.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 16.6 | 16.6 |  | 16.6 | 16.6 |  | 77.6 | 77.6 | 77.6 | 77.6 | 77.6 |  |
| Actuated g/C Ratio | 0.16 | 0.16 |  | 0.16 | 0.16 |  | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |  |
| v/c Ratio | 0.21 | 0.31 |  | 0.71 | 0.21 |  | 0.30 | 0.88 | 0.19 | 0.73 | 0.60 |  |

4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive W3 Sunset Creek

|  | 4 |  |  | $\checkmark$ |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 39.5 | 12.2 |  | 60.0 | 14.6 |  | 8.3 | 21.5 | 2.0 | 54.8 | 10.0 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 39.5 | 12.2 |  | 60.0 | 14.6 |  | 8.3 | 21.5 | 2.0 | 54.8 | 10.0 |  |
| LOS | D | B |  | E | B |  | A | C | A | D | A |  |
| Approach Delay |  | 20.6 |  |  | 46.2 |  |  | 17.5 |  |  | 13.9 |  |
| Approach LOS |  | C |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 7.7 | 1.7 |  | 28.0 | 1.9 |  | 7.4 | 162.3 | 3.1 | 7.9 | 67.5 |  |
| Queue Length 95th (m) | 17.4 | 15.3 |  | 48.4 | 12.8 |  | 19.8 | \#335.0 | 11.7 | \#21.5 | 125.3 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length (m) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 293 | 420 |  | 291 | 411 |  | 398 | 1387 | 1239 | 105 | 1335 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.24 |  | 0.50 | 0.16 |  | 0.30 | 0.88 | 0.19 | 0.73 | 0.60 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 110
Actuated Cycle Length: 106.3
Natural Cycle: 100
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.88
Intersection Signal Delay: $18.7 \quad$ Intersection LOS: B
Intersection Capacity Utilization 95.1\%
ICU Level of Service $F$
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive

 W3 Sunset Creek

|  | 4 |  |  |  |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | \% | $\hat{F}$ |  |
| Traffic Volume (vph) | 169 | 874 | 50 | 132 | 935 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Future Volume (vph) | 169 | 874 | 50 | 132 | 935 | 132 | 41 | 46 | 87 | 115 | 50 | 127 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.98 |  |
| Frt |  | 0.992 |  |  |  | 0.850 |  | 0.902 |  |  | 0.892 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1850 | 0 | 1772 | 1902 | 1633 | 1825 | 1689 | 0 | 1825 | 1683 | 0 |
| Flt Permitted | 0.064 |  |  | 0.224 |  |  | 0.464 |  |  | 0.602 |  |  |
| Satd. Flow (perm) | 123 | 1850 | 0 | 418 | 1902 | 1633 | 888 | 1689 | 0 | 1157 | 1683 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 110 |  | 87 |  |  | 116 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 184 | 950 | 54 | 143 | 1016 | 143 | 45 | 50 | 95 | 125 | 54 | 138 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 184 | 1004 | 0 | 143 | 1016 | 143 | 45 | 145 | 0 | 125 | 192 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases |  |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 5 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 8.0 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 8.0 | 73.0 |  | 65.0 | 65.0 | 65.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (\%) | 8.0\% | 73.0\% |  | 65.0\% | 65.0\% | 65.0\% | 27.0\% | 27.0\% |  | 27.0\% | 27.0\% |  |
| Maximum Green (s) | 5.0 | 66.9 |  | 58.9 | 58.9 | 58.9 | 21.0 | 21.0 |  | 21.0 | 21.0 |  |
| Yellow Time (s) | 3.0 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 0.0 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 3.0 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C-Max |  | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) |  | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effict Green (s) | 75.8 | 72.7 |  | 59.4 | 59.4 | 59.4 | 15.2 | 15.2 |  | 15.2 | 15.2 |  |
| Actuated g/C Ratio | 0.76 | 0.73 |  | 0.59 | 0.59 | 0.59 | 0.15 | 0.15 |  | 0.15 | 0.15 |  |
| v/c Ratio | 0.69 | 0.75 |  | 0.58 | 0.90 | 0.14 | 0.34 | 0.44 |  | 0.71 | 0.54 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharfictiffe ReatBSBattkground Traffic W3 Sunset Creek

|  |  |  |  |  |  |  |  | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 34.6 | 13.7 |  | 24.3 | 30.6 | 3.2 | 42.9 | 20.1 |  | 61.3 | 21.4 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 34.6 | 13.7 |  | 24.3 | 30.6 | 3.2 | 42.9 | 20.1 |  | 61.3 | 21.4 |  |
| LOS | C | B |  | C | C | A | D | C |  | E | C |  |
| Approach Delay |  | 16.9 |  |  | 26.9 |  |  | 25.5 |  |  | 37.1 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | D |  |
| Queue Length 50th (m) | 17.3 | 99.6 |  | 16.1 | 161.8 | 2.5 | 7.9 | 10.0 |  | 23.2 | 13.2 |  |
| Queue Length 95th (m) | \#65.4 | 187.6 |  | 39.8 | \#258.7 | 10.1 | 17.4 | 25.8 |  | 40.0 | 31.9 |  |
| Internal Link Dist ( m ) |  | 322.2 |  |  | 343.0 |  |  | 264.8 |  |  | 219.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  | 60.0 | 5.0 |  |  | 45.0 |  |  |
| Base Capacity (vph) | 268 | 1346 |  | 248 | 1129 | 1014 | 186 | 423 |  | 242 | 445 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.69 | 0.75 |  | 0.58 | 0.90 | 0.14 | 0.24 | 0.34 |  | 0.52 | 0.43 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $32(32 \%)$, Referenced to phase 2:EBTL and 6:WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 23.9 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 93.8\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


|  | $\psi$ | $\rightarrow$ |  | 4 |  |  | 4 | $\dagger$ | 7 | ( | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | 4 | 「' | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 47 | 77 | 29 | 163 | 57 | 146 | 67 | 811 | 304 | 185 | 666 | 49 |
| Future Volume (vph) | 47 | 77 | 29 | 163 | 57 | 146 | 67 | 811 | 304 | 185 | 666 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 |  |  |  |  | 0.99 |  |  |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  |  | 0.850 |  | 0.990 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1697 | 0 | 1674 | 1671 | 1432 | 1615 | 1762 | 1585 | 1674 | 1794 | 0 |
| Flt Permitted | 0.715 |  |  | 0.507 |  |  | 0.255 |  |  | 0.197 |  |  |
| Satd. Flow (perm) | 1260 | 1697 | 0 | 889 | 1671 | 1432 | 434 | 1762 | 1562 | 347 | 1794 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 14 |  |  |  | 138 |  |  | 223 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 53 | 87 | 33 | 183 | 64 | 164 | 75 | 911 | 342 | 208 | 748 | 55 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 53 | 120 | 0 | 183 | 64 | 164 | 75 | 911 | 342 | 208 | 803 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 |  |
| Total Split (s) | 37.0 | 37.0 |  | 11.0 | 48.0 | 48.0 | 82.0 | 82.0 | 82.0 | 82.0 | 82.0 |  |
| Total Split (\%) | 28.5\% | 28.5\% |  | 8.5\% | 36.9\% | 36.9\% | 63.1\% | 63.1\% | 63.1\% | 63.1\% | 63.1\% |  |
| Maximum Green (s) | 30.8 | 30.8 |  | 8.0 | 41.8 | 41.8 | 76.1 | 76.1 | 76.1 | 76.1 | 76.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 12.3 | 12.3 |  | 26.5 | 23.3 | 23.3 | 76.2 | 76.2 | 76.2 | 76.2 | 76.2 |  |
| Actuated g/C Ratio | 0.11 | 0.11 |  | 0.24 | 0.21 | 0.21 | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 |  |
| v/c Ratio | 0.38 | 0.60 |  | 0.69 | 0.18 | 0.40 | 0.25 | 0.76 | 0.30 | 0.88 | 0.65 |  |


|  | 4 |  |  | 7 |  |  | , | $\dagger$ | / |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 53.9 | 54.4 |  | 50.9 | 37.2 | 12.2 | 10.3 | 17.6 | 3.3 | 53.8 | 13.9 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 53.9 | 54.4 |  | 50.9 | 37.2 | 12.2 | 10.3 | 17.6 | 3.3 | 53.8 | 13.9 |  |
| LOS | D | D |  | D | D | B | B | B | A | D | B |  |
| Approach Delay |  | 54.2 |  |  | 33.3 |  |  | 13.5 |  |  | 22.1 |  |
| Approach LOS |  | D |  |  | C |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 10.9 | 22.3 |  | 34.3 | 11.6 | 4.6 | 5.6 | 117.2 | 8.0 | 32.3 | 89.7 |  |
| Queue Length 95th (m) | 22.8 | 40.3 |  | 54.4 | 22.8 | 21.5 | 14.7 | 193.4 | 20.1 | \#90.5 | 145.5 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length ( m ) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 348 | 478 |  | 267 | 626 | 623 | 296 | 1202 | 1136 | 236 | 1226 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.25 |  | 0.69 | 0.10 | 0.26 | 0.25 | 0.76 | 0.30 | 0.88 | 0.65 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 111.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.88 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 21.7 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 83.6\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road




3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2033) Total Traffic W3 Sunset Creek

AM Peak Hour

|  | 4 |  |  | 7 |  |  | $4$ | 9 | $p$ | $\pm$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 26 | 0 | 13 | 80 | 0 | 312 | 2 | 656 | 31 | 96 | 788 | 8 |
| Future Volume (vph) | 26 | 0 | 13 | 80 | 0 | 312 | 2 | 656 | 31 | 96 | 788 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 1.00 |  |  |  |  |  |  |  |
| Frt |  | 0.955 |  |  |  | 0.850 |  | 0.993 |  |  | 0.999 |  |
| Flt Protected |  | 0.968 |  |  | 0.950 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1717 | 0 | 0 | 1825 | 1633 | 1825 | 1804 | 0 | 1825 | 1862 | 0 |
| Flt Permitted |  | 0.775 |  |  | 0.728 |  | 0.153 |  |  | 0.234 |  |  |
| Satd. Flow (perm) | 0 | 1375 | 0 | 0 | 1397 | 1633 | 294 | 1804 | 0 | 450 | 1862 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 41 |  |  |  | 146 |  | 4 |  |  | 1 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 8\% | 0\% | 0\% | 0\% | 0\% | 6\% | 0\% | 0\% | 3\% | 12\% |
| Adj. Flow (vph) | 30 | 0 | 15 | 91 | 0 | 355 | 2 | 745 | 35 | 109 | 895 | 9 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 45 | 0 | 0 | 91 | 355 | 2 | 780 | 0 | 109 | 904 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 34.3 | 34.3 |  | 34.3 | 34.3 | 34.3 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 45.0 | 45.0 |  | 45.0 | 45.0 |  |
| Total Split (\%) | 43.8\% | 43.8\% |  | 43.8\% | 43.8\% | 43.8\% | 56.3\% | 56.3\% |  | 56.3\% | 56.3\% |  |
| Maximum Green (s) | 28.7 | 28.7 |  | 28.7 | 28.7 | 28.7 | 39.0 | 39.0 |  | 39.0 | 39.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 21.0 | 21.0 |  | 21.0 | 21.0 | 21.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 14.5 |  |  | 14.5 | 14.5 | 39.3 | 39.3 |  | 39.3 | 39.3 |  |
| Actuated g/C Ratio |  | 0.22 |  |  | 0.22 | 0.22 | 0.59 | 0.59 |  | 0.59 | 0.59 |  |
| v/c Ratio |  | 0.14 |  |  | 0.30 | 0.75 | 0.01 | 0.73 |  | 0.41 | 0.82 |  |


| 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 8.4 |  |  | 23.2 | 24.2 | 8.5 | 16.8 |  | 15.5 | 20.8 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 8.4 |  |  | 23.2 | 24.2 | 8.5 | 16.8 |  | 15.5 | 20.8 |  |
| LOS | A |  |  | C | C | A | B |  | B | C |  |
| Approach Delay | 8.4 |  |  | 24.0 |  |  | 16.8 |  |  | 20.3 |  |
| Approach LOS | A |  |  | C |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 0.4 |  |  | 9.3 | 23.2 | 0.1 | 59.1 |  | 6.2 | 76.0 |  |
| Queue Length 95th (m) | 6.5 |  |  | 19.2 | 46.3 | 1.1 | \#150.8 |  | 23.5 | \#187.3 |  |
| Internal Link Dist ( m ) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length ( m ) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 623 |  |  | 610 | 795 | 174 | 1072 |  | 267 | 1105 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.07 |  |  | 0.15 | 0.45 | 0.01 | 0.73 |  | 0.41 | 0.82 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 66.2 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.82 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 19.6 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 76.0\% ICU Level of Service DAnalysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | 4 | $\pm$ |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\hat{\dagger}$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | ¢ |  |
| Traffic Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 576 | 53 | 26 | 811 | 32 |
| Future Volume (vph) | 41 | 4 | 92 | 213 | 6 | 74 | 60 | 576 | 53 | 26 | 811 | 32 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.856 |  |  | 0.862 |  |  |  | 0.850 |  | 0.994 |  |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1541 | 0 | 1825 | 1656 | 0 | 1690 | 1746 | 1633 | 1825 | 1793 | 0 |
| Flt Permitted | 0.699 |  |  | 0.688 |  |  | 0.149 |  |  | 0.334 |  |  |
| Satd. Flow (perm) | 1304 | 1541 | 0 | 1322 | 1656 | 0 | 265 | 1746 | 1633 | 642 | 1793 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 103 |  |  | 83 |  |  |  | 60 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 3\% | 0\% | 7\% | 0\% | 0\% | 0\% | 8\% | 10\% | 0\% | 0\% | 6\% | 19\% |
| Adj. Flow (vph) | 46 | 4 | 103 | 239 | 7 | 83 | 67 | 647 | 60 | 29 | 911 | 36 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 46 | 107 | 0 | 239 | 90 | 0 | 67 | 647 | 60 | 29 | 947 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 55.0 | 55.0 | 55.0 | 55.0 | 55.0 |  |
| Total Split (\%) | 31.3\% | 31.3\% |  | 31.3\% | 31.3\% |  | 68.8\% | 68.8\% | 68.8\% | 68.8\% | 68.8\% |  |
| Maximum Green (s) | 19.3 | 19.3 |  | 19.3 | 19.3 |  | 48.6 | 48.6 | 48.6 | 48.6 | 48.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 17.4 | 17.4 |  | 17.4 | 17.4 |  | 49.8 | 49.8 | 49.8 | 49.8 | 49.8 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 |  |
| v/c Ratio | 0.16 | 0.26 |  | 0.83 | 0.21 |  | 0.40 | 0.59 | 0.06 | 0.07 | 0.84 |  |
| Control Delay | 25.7 | 7.7 |  | 53.5 | 8.4 |  | 17.4 | 12.0 | 2.1 | 7.0 | 21.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |


|  | 4 |  |  | 1 |  |  | - | 4 | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | 25.7 | 7.7 |  | 53.5 | 8.4 |  | 17.4 | 12.0 | 2.1 | 7.0 | 21.2 |  |
| LOS | C | A |  | D | A |  | B | B | A | A | C |  |
| Approach Delay |  | 13.1 |  |  | 41.2 |  |  | 11.7 |  |  | 20.8 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 5.5 | 0.5 |  | 33.7 | 0.8 |  | 4.8 | 55.1 | 0.0 | 1.6 | 107.1 |  |
| Queue Length 95th (m) | 13.6 | 11.6 |  | \#66.0 | 11.1 |  | 16.0 | 84.1 | 3.9 | 4.8 | \#192.6 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 317 | 452 |  | 321 | 466 |  | 166 | 1096 | 1047 | 403 | 1128 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.24 |  | 0.74 | 0.19 |  | 0.40 | 0.59 | 0.06 | 0.07 | 0.84 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 79.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.84 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 20.1 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 78.4\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomadeS(\&AB3) Total Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  | 4 | 4 |  |  |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{\beta}$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 69 | 616 | 43 | 187 | 702 | 99 | 61 | 91 | 270 | 155 | 35 | 153 |
| Future Volume (vph) | 69 | 616 | 43 | 187 | 702 | 99 | 61 | 91 | 270 | 155 | 35 | 153 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  |  | 0.98 | 0.98 | 0.98 |  | 1.00 | 0.96 |  |
| Frt |  | 0.990 |  |  |  | 0.850 |  | 0.888 |  |  | 0.878 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1810 | 0 | 1738 | 1812 | 1541 | 1789 | 1572 | 0 | 1674 | 1430 | 0 |
| Flt Permitted | 0.204 |  |  | 0.236 |  |  | 0.630 |  |  | 0.193 |  |  |
| Satd. Flow (perm) | 370 | 1810 | 0 | 432 | 1812 | 1506 | 1162 | 1572 | 0 | 340 | 1430 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 108 |  | 152 |  |  | 166 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 75 | 670 | 47 | 203 | 763 | 108 | 66 | 99 | 293 | 168 | 38 | 166 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 75 | 717 | 0 | 203 | 763 | 108 | 66 | 392 | 0 | 168 | 204 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 5.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 8.0 | 26.0 |  |
| Total Split (s) | 55.0 | 55.0 |  | 55.0 | 55.0 | 55.0 | 26.0 | 26.0 |  | 9.0 | 35.0 |  |
| Total Split (\%) | 61.1\% | 61.1\% |  | 61.1\% | 61.1\% | 61.1\% | 28.9\% | 28.9\% |  | 10.0\% | 38.9\% |  |
| Maximum Green (s) | 48.9 | 48.9 |  | 48.9 | 48.9 | 48.9 | 20.0 | 20.0 |  | 6.0 | 29.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.0 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 0.0 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max | Max | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  |  | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Efftt Green (s) | 49.0 | 49.0 |  | 49.0 | 49.0 | 49.0 | 17.7 | 17.7 |  | 29.7 | 26.7 |  |
| Actuated g/C Ratio | 0.56 | 0.56 |  | 0.56 | 0.56 | 0.56 | 0.20 | 0.20 |  | 0.34 | 0.30 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.36 | 0.71 |  | 0.85 | 0.75 | 0.12 | 0.28 | 0.90 |  | 0.82 | 0.37 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomnteS(\&AB3) Total Traffic W3 Sunset Creek


Splits and Phases: 9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | f |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 54 | 85 | 49 | 336 | 104 | 308 | 65 | 952 | 259 | 174 | 784 | 53 |
| Future Volume (vph) | 54 | 85 | 49 | 336 | 104 | 308 | 65 | 952 | 259 | 174 | 784 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 0.99 |  | 0.99 |  | 0.97 | 1.00 |  | 0.98 |  | 1.00 |  |
| Frt |  | 0.945 |  |  |  | 0.850 |  |  | 0.850 |  | 0.991 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1692 | 0 | 1825 | 1921 | 1585 | 1789 | 1883 | 1601 | 1789 | 1829 | 0 |
| Flt Permitted | 0.685 |  |  | 0.424 |  |  | 0.203 |  |  | 0.057 |  |  |
| Satd. Flow (perm) | 1254 | 1692 | 0 | 807 | 1921 | 1538 | 382 | 1883 | 1576 | 107 | 1829 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 19 |  |  |  | 198 |  |  | 139 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 57 | 90 | 52 | 357 | 111 | 328 | 69 | 1013 | 276 | 185 | 834 | 56 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 57 | 142 | 0 | 357 | 111 | 328 | 69 | 1013 | 276 | 185 | 890 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 8.0 | 45.9 |  |
| Total Split (s) | 26.0 | 26.0 |  | 19.0 | 45.0 | 45.0 | 73.0 | 73.0 | 73.0 | 12.0 | 85.0 |  |
| Total Split (\%) | 20.0\% | 20.0\% |  | 14.6\% | 34.6\% | 34.6\% | 56.2\% | 56.2\% | 56.2\% | 9.2\% | 65.4\% |  |
| Maximum Green (s) | 19.8 | 19.8 |  | 16.0 | 38.8 | 38.8 | 67.1 | 67.1 | 67.1 | 9.0 | 79.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.0 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 0.0 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 |  | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 |  |
| Act Efft Green (s) | 14.2 | 14.2 |  | 36.4 | 33.2 | 33.2 | 67.2 | 67.2 | 67.2 | 82.1 | 79.2 |  |
| Actuated g/C Ratio | 0.11 | 0.11 |  | 0.29 | 0.27 | 0.27 | 0.54 | 0.54 | 0.54 | 0.66 | 0.64 |  |
| v/c Ratio | 0.40 | 0.68 |  | 0.98 | 0.22 | 0.59 | 0.33 | 1.00 | 0.30 | 0.97 | 0.76 |  |


|  | $\rangle$ |  |  |  |  |  |  | $\uparrow$ | 7 | $\downarrow$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 59.2 | 62.0 |  | 81.7 | 36.3 | 19.5 | 23.1 | 57.1 | 8.8 | 87.5 | 22.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 59.2 | 62.0 |  | 81.7 | 36.3 | 19.5 | 23.1 | 57.1 | 8.8 | 87.5 | 22.3 |  |
| LOS | E | E |  | F | D | B | C | E | A | F | C |  |
| Approach Delay |  | 61.2 |  |  | 49.8 |  |  | 45.6 |  |  | 33.5 |  |
| Approach LOS |  | E |  |  | D |  |  | D |  |  | C |  |
| Queue Length 50th (m) | 13.1 | 29.3 |  | 76.9 | 21.2 | 26.5 | 9.2 | 238.6 | 16.3 | 29.3 | 143.7 |  |
| Queue Length 95th (m) | 26.5 | 50.9 |  | \#137.8 | 36.2 | 56.6 | 22.9 | \#358.7 | 35.5 | \#80.6 | 223.8 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 199 | 285 |  | 366 | 599 | 615 | 206 | 1015 | 914 | 191 | 1164 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.29 | 0.50 |  | 0.98 | 0.19 | 0.53 | 0.33 | 1.00 | 0.30 | 0.97 | 0.76 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 124.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.00 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 43.7 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 103.8\% <br> ICU Level of Service G Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2571 | 2560 | 1077 | 2566 | 2581 | 1292 | 1105 | 0 | 0 | 1299 | 0 | 0 |
| Stage 1 | 1191 | 1191 | - | 1362 | 1362 | - | - | - | - | - | - | - |
| Stage 2 | 1380 | 1369 | - | 1204 | 1219 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.24 | 7.1 | 6.5 | 6.2 | 4.13 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.336 | 3.5 | 4 | 3.3 | 2.227 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | ~18 | 27 | 264 | 18 | 26 | 201 | 628 | - | - | 540 | - | - |
| Stage 1 | 231 | 263 | - | 185 | 218 | - | - | - | - | - | - | - |
| Stage 2 | 180 | 216 | - | 227 | 255 | - | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | $\sim 13$ | 23 | 264 | 14 | 22 | 201 | 628 | - | - | 540 | - | - |
| Mov Cap-2 Maneuver | $\sim 13$ | 23 | - | 14 | 22 | - | - | - | - | - | - | - |
| Stage 1 | 218 | 235 | - | 175 | 206 | - | - | - | - | - | - | - |
| Stage 2 | 140 | 204 | - | 184 | 228 | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | \$ 728 |  |  | 26.8 |  |  | 0.3 |  |  | 0.6 |  |  |
| HCM LOS | F |  |  | D |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | EBLn2W | VBLn1 | SBL | SBT | SBR |  |  |
| Capacity (veh/h) |  | 628 | - |  | 13 | 264 | 201 | 540 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.055 | - | - | 2.51 | 0.096 | 0.178 | 0.105 | - | - |  |  |
| HCM Control Delay (s) |  | 11.1 | - |  | 1276.1 | 20.1 | 26.8 | 12.4 | - | - |  |  |
| HCM Lane LOS |  | B | - | - | F | C | D | B | - | - |  |  |
| HCM 95th \%tile Q(veh |  | 0.2 | - |  | 4.9 | 0.3 | 0.6 | 0.4 | - | - |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2033) Total Traffic W3 Sunset Creek

PM Peak Hour

|  | 4 |  |  |  |  | 4 | 4 | $\dagger$ |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | \% | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1084 | 96 | 241 | 762 | 26 |
| Future Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1084 | 96 | 241 | 762 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  | 0.97 |  |  |  | 1.00 |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  | 0.988 |  |  | 0.995 |  |
| Flt Protected |  | 0.966 |  |  | 0.955 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1664 | 0 | 0 | 1835 | 1633 | 1825 | 1881 | 0 | 1825 | 1848 | 0 |
| Flt Permitted |  | 0.768 |  |  | 0.723 |  | 0.354 |  |  | 0.047 |  |  |
| Satd. Flow (perm) | 0 | 1323 | 0 | 0 | 1361 | 1633 | 661 | 1881 | 0 | 90 | 1848 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 50 |  |  |  | 179 |  | 7 |  |  | 4 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 6 | 6 |  |  | 28 |  |  |  |  | 28 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 8\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 3\% | 4\% |
| Adj. Flow (vph) | 14 | 0 | 6 | 36 | 2 | 179 | 11 | 1141 | 101 | 254 | 802 | 27 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 20 | 0 | 0 | 38 | 179 | 11 | 1242 | 0 | 254 | 829 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.3 | 24.3 |  | 24.3 | 24.3 | 24.3 | 24.0 | 24.0 |  | 8.0 | 24.0 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 89.0 | 89.0 |  | 16.0 | 105.0 |  |
| Total Split (\%) | 19.2\% | 19.2\% |  | 19.2\% | 19.2\% | 19.2\% | 68.5\% | 68.5\% |  | 12.3\% | 80.8\% |  |
| Maximum Green (s) | 18.7 | 18.7 |  | 18.7 | 18.7 | 18.7 | 83.0 | 83.0 |  | 13.0 | 99.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 3.0 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 0.0 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  |  | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Effict Green (s) |  | 8.9 |  |  | 8.9 | 8.9 | 83.0 | 83.0 |  | 102.0 | 99.0 |  |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.07 | 0.07 | 0.69 | 0.69 |  | 0.85 | 0.82 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.14 |  |  | 0.38 | 0.63 | 0.02 | 0.95 |  | 0.96 | 0.54 |  |


| 4 |  |  |  |  |  |  | $\dagger$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 2.5 |  |  | 63.7 | 17.7 | 6.8 | 34.5 |  | 82.7 | 5.2 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 2.5 |  |  | 63.7 | 17.7 | 6.8 | 34.5 |  | 82.7 | 5.2 |  |
| LOS | A |  |  | E | B | A | C |  | F | A |  |
| Approach Delay | 2.5 |  |  | 25.7 |  |  | 34.3 |  |  | 23.4 |  |
| Approach LOS | A |  |  | C |  |  | C |  |  | C |  |
| Queue Length 50th (m) | 0.0 |  |  | 8.7 | 0.0 | 0.7 | 238.2 |  | 43.3 | 47.5 |  |
| Queue Length 95th (m) | 0.9 |  |  | 19.9 | 20.7 | 2.8 | \#391.8 |  | \#100.0 | 84.2 |  |
| Internal Link Dist (m) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length (m) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 247 |  |  | 211 | 405 | 456 | 1301 |  | 264 | 1523 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.08 |  |  | 0.18 | 0.44 | 0.02 | 0.95 |  | 0.96 | 0.54 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120.2 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 140 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.96 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 28.7 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.0\% ICU Level of Service FAnalysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F |  | ${ }^{7}$ | f |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | ¢ |  |
| Traffic Volume (vph) | 39 | - | 78 | 136 | 10 | 49 | 106 | 1104 | 223 | 72 | 661 | 63 |
| Future Volume (vph) | 39 | 9 | 78 | 136 | 10 | 49 | 106 | 1104 | 223 | 72 | 661 | 63 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.98 |  | 1.00 |  |  |  |  |  |  |  |  |
| Frt |  | 0.866 |  |  | 0.876 |  |  |  | 0.850 |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1601 | 0 | 1825 | 1683 | 0 | 1825 | 1902 | 1633 | 1825 | 1826 | 0 |
| Flt Permitted | 0.715 |  |  | 0.696 |  |  | 0.293 |  |  | 0.083 |  |  |
| Satd. Flow (perm) | 1334 | 1601 | 0 | 1334 | 1683 | 0 | 563 | 1902 | 1633 | 159 | 1826 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 84 |  |  | 53 |  |  |  | 156 |  | 8 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 3\% | 0\% | 2\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 4\% | 2\% |
| Adj. Flow (vph) | 42 | 10 | 84 | 146 | 11 | 53 | 114 | 1187 | 240 | 77 | 711 | 68 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 42 | 94 | 0 | 146 | 64 | 0 | 114 | 1187 | 240 | 77 | 779 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 |  | 75.0 | 75.0 | 75.0 | 75.0 | 75.0 |  |
| Total Split (\%) | 31.8\% | 31.8\% |  | 31.8\% | 31.8\% |  | 68.2\% | 68.2\% | 68.2\% | 68.2\% | 68.2\% |  |
| Maximum Green (s) | 29.3 | 29.3 |  | 29.3 | 29.3 |  | 68.6 | 68.6 | 68.6 | 68.6 | 68.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effict Green (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 71.5 | 71.5 | 71.5 | 71.5 | 71.5 |  |
| Actuated g/C Ratio | 0.16 | 0.16 |  | 0.16 | 0.16 |  | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 |  |
| v/c Ratio | 0.20 | 0.29 |  | 0.68 | 0.20 |  | 0.28 | 0.87 | 0.20 | 0.68 | 0.59 |  |


|  | 4 |  |  | 7 |  |  |  | $\dagger$ | / |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 36.3 | 11.7 |  | 54.8 | 13.7 |  | 8.2 | 20.9 | 2.5 | 44.9 | 10.0 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 36.3 | 11.7 |  | 54.8 | 13.7 |  | 8.2 | 20.9 | 2.5 | 44.9 | 10.0 |  |
| LOS | D | B |  | D | B |  | A | C | A | D | B |  |
| Approach Delay |  | 19.3 |  |  | 42.3 |  |  | 17.1 |  |  | 13.2 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | B |  |
| Queue Length 50th (m) | 6.9 | 1.6 |  | 25.9 | 1.8 |  | 6.6 | 145.5 | 4.1 | 6.9 | 61.8 |  |
| Queue Length 95th (m) | 16.1 | 14.2 |  | 45.5 | 12.2 |  | 18.5 | \#312.8 | 13.7 | \#39.5 | 119.9 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 392 | 530 |  | 392 | 532 |  | 403 | 1364 | 1216 | 113 | 1312 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.11 | 0.18 |  | 0.37 | 0.12 |  | 0.28 | 0.87 | 0.20 | 0.68 | 0.59 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 99.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.87 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 17.9 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 93.6\% |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomateS(』AB3) Total Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  | 4 | 4 |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\dagger}$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 182 | 824 | 50 | 132 | 887 | 146 | 41 | 46 | 87 | 123 | 50 | 136 |
| Future Volume (vph) | 182 | 824 | 50 | 132 | 887 | 146 | 41 | 46 | 87 | 123 | 50 | 136 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.98 |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  | 0.902 |  |  | 0.890 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1848 | 0 | 1772 | 1902 | 1633 | 1825 | 1689 | 0 | 1825 | 1679 | 0 |
| Flt Permitted | 0.067 |  |  | 0.261 |  |  | 0.449 |  |  | 0.608 |  |  |
| Satd. Flow (perm) | 129 | 1848 | 0 | 487 | 1902 | 1633 | 860 | 1689 | 0 | 1168 | 1679 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  |  | 120 |  | 90 |  |  | 130 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 198 | 896 | 54 | 143 | 964 | 159 | 45 | 50 | 95 | 134 | 54 | 148 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 198 | 950 | 0 | 143 | 964 | 159 | 45 | 145 | 0 | 134 | 202 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  |  |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 5 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 8.0 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 8.0 | 70.0 |  | 62.0 | 62.0 | 62.0 | 30.0 | 30.0 |  | 30.0 | 30.0 |  |
| Total Split (\%) | 8.0\% | 70.0\% |  | 62.0\% | 62.0\% | 62.0\% | 30.0\% | 30.0\% |  | 30.0\% | 30.0\% |  |
| Maximum Green (s) | 5.0 | 63.9 |  | 55.9 | 55.9 | 55.9 | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Yellow Time (s) | 3.0 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 0.0 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 3.0 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C-Max |  | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) |  | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Efftt Green (s) | 75.0 | 71.9 |  | 56.3 | 56.3 | 56.3 | 16.0 | 16.0 |  | 16.0 | 16.0 |  |
| Actuated g/C Ratio | 0.75 | 0.72 |  | 0.56 | 0.56 | 0.56 | 0.16 | 0.16 |  | 0.16 | 0.16 |  |
| v/c Ratio | 0.64 | 0.71 |  | 0.52 | 0.90 | 0.16 | 0.33 | 0.42 |  | 0.72 | 0.53 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomnteS(\&AB3) Total Traffic W3 Sunset Creek


Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2033) Total Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  | 4 | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\hat{}$ |  | ${ }_{1}$ | $\hat{F}$ |  |
| Traffic Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1084 | 96 | 241 | 762 | 26 |
| Future Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1084 | 96 | 241 | 762 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  |  |  |  |  | 1.00 |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  | 0.988 |  |  | 0.995 |  |
| FIt Protected |  | 0.966 |  |  | 0.955 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1666 | 0 | 0 | 1835 | 1633 | 1825 | 1881 | 0 | 1825 | 1849 | 0 |
| Flt Permitted |  | 0.768 |  |  | 0.723 |  | 0.300 |  |  | 0.116 |  |  |
| Satd. Flow (perm) | 0 | 1325 | 0 | 0 | 1366 | 1633 | 576 | 1881 | 0 | 223 | 1849 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 30 |  |  |  | 134 |  | 10 |  |  | 4 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 6 | 6 |  |  | 28 |  |  |  |  | 28 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 8\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 3\% | 4\% |
| Adj. Flow (vph) | 14 | 0 | 6 | 36 | 2 | 179 | 11 | 1141 | 101 | 254 | 802 | 27 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 20 | 0 | 0 | 38 | 179 | 11 | 1242 | 0 | 254 | 829 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | , |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.3 | 24.3 |  | 24.3 | 24.3 | 24.3 | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 85.0 | 85.0 |  | 85.0 | 85.0 |  |
| Total Split (\%) | 22.7\% | 22.7\% |  | 22.7\% | 22.7\% | 22.7\% | 77.3\% | 77.3\% |  | 77.3\% | 77.3\% |  |
| Maximum Green (s) | 18.7 | 18.7 |  | 18.7 | 18.7 | 18.7 | 79.0 | 79.0 |  | 79.0 | 79.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 9.4 |  |  | 9.4 | 9.4 | 82.2 | 82.2 |  | 82.2 | 82.2 |  |
| Actuated g/C Ratio |  | 0.09 |  |  | 0.09 | 0.09 | 0.79 | 0.79 |  | 0.79 | 0.79 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.14 |  |  | 0.31 | 0.66 | 0.02 | 0.83 |  | 1.44 | 0.57 |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue W3 Sunset Creek

Future (2033) Total Traffic
PM Peak Hour (With SBL Phase)

|  | $\rightarrow \quad \rightarrow$ |  | $\%$ |  |  | 4 | 9 | \% |  | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBL EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 11.5 |  |  | 48.6 | 25.7 | 3.3 | 14.3 |  | 247.4 | 6.4 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 11.5 |  |  | 48.6 | 25.7 | 3.3 | 14.3 |  | 247.4 | 6.4 |  |
| LOS | B |  |  | D | C | A | B |  | F | A |  |
| Approach Delay | 11.5 |  |  | 29.7 |  |  | 14.2 |  |  | 63.0 |  |
| Approach LOS | B |  |  | C |  |  | B |  |  | E |  |
| Queue Length 50th (m) | 0.0 |  |  | 7.0 | 8.3 | 0.4 | 112.7 |  | ~32.3 | 46.5 |  |
| Queue Length 95th (m) | 5.0 |  |  | 16.7 | 28.7 | 1.9 | \#285.9 |  | \#88.7 | 97.7 |  |
| Internal Link Dist (m) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length (m) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 263 |  |  | 246 | 403 | 455 | 1489 |  | 176 | 1463 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.08 |  |  | 0.15 | 0.44 | 0.02 | 0.83 |  | 1.44 | 0.57 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 110 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 104 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.44 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 36.0 <br> Intersection LOS: D |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 100.7\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


|  | 4 |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | f |  | * | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 50 | 82 | 30 | 171 | 61 | 155 | 70 | 835 | 315 | 196 | 700 | 53 |
| Future Volume (vph) | 50 | 82 | 30 | 171 | 61 | 155 | 70 | 835 | 315 | 196 | 700 | 53 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  | 0.99 |  |  |  |  | 0.99 |  |  |  |
| Frt |  | 0.960 |  |  |  | 0.850 |  |  | 0.850 |  | 0.989 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1674 | 1701 | 0 | 1674 | 1671 | 1432 | 1615 | 1762 | 1585 | 1674 | 1792 | 0 |
| Flt Permitted | 0.712 |  |  | 0.486 |  |  | 0.243 |  |  | 0.197 |  |  |
| Satd. Flow (perm) | 1255 | 1701 | 0 | 852 | 1671 | 1432 | 413 | 1762 | 1562 | 347 | 1792 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 13 |  |  |  | 149 |  |  | 247 |  | 6 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) |  |  | 2 | 2 |  |  |  |  | 3 | 3 |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 9\% | 2\% | 23\% | 9\% | 15\% | 14\% | 13\% | 9\% | 3\% | 9\% | 6\% | 6\% |
| Adj. Flow (vph) | 56 | 92 | 34 | 192 | 69 | 174 | 79 | 938 | 354 | 220 | 787 | 60 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 56 | 126 | 0 | 192 | 69 | 174 | 79 | 938 | 354 | 220 | 847 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 |  |
| Total Split (s) | 34.0 | 34.0 |  | 9.0 | 43.0 | 43.0 | 87.0 | 87.0 | 87.0 | 87.0 | 87.0 |  |
| Total Split (\%) | 26.2\% | 26.2\% |  | 6.9\% | 33.1\% | 33.1\% | 66.9\% | 66.9\% | 66.9\% | 66.9\% | 66.9\% |  |
| Maximum Green (s) | 27.8 | 27.8 |  | 6.0 | 36.8 | 36.8 | 81.1 | 81.1 | 81.1 | 81.1 | 81.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 | 28.0 | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Act Efft Green (s) | 13.0 | 13.0 |  | 25.2 | 22.0 | 22.0 | 81.2 | 81.2 | 81.2 | 81.2 | 81.2 |  |
| Actuated g/C Ratio | 0.11 | 0.11 |  | 0.22 | 0.19 | 0.19 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 |  |
| v/c Ratio | 0.40 | 0.62 |  | 0.84 | 0.22 | 0.44 | 0.27 | 0.76 | 0.30 | 0.90 | 0.67 |  |


|  | 4 |  |  | 7 |  |  | , | $\dagger$ | / |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 55.5 | 57.1 |  | 71.5 | 40.7 | 12.9 | 10.0 | 16.7 | 2.8 | 56.3 | 13.5 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 55.5 | 57.1 |  | 71.5 | 40.7 | 12.9 | 10.0 | 16.7 | 2.8 | 56.3 | 13.5 |  |
| LOS | E | E |  | E | D | B | A | B | A | E | B |  |
| Approach Delay |  | 56.6 |  |  | 43.2 |  |  | 12.7 |  |  | 22.3 |  |
| Approach LOS |  | E |  |  | D |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 11.9 | 24.6 |  | 38.5 | 13.2 | 4.7 | 5.8 | 119.1 | 6.8 | 35.7 | 94.4 |  |
| Queue Length 95th (m) | 24.2 | 43.4 |  | \#66.4 | 25.5 | 22.7 | 15.5 | 199.4 | 18.1 | \#97.6 | 155.5 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length ( m ) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 302 | 420 |  | 229 | 533 | 558 | 290 | 1240 | 1172 | 244 | 1263 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.19 | 0.30 |  | 0.84 | 0.13 | 0.31 | 0.27 | 0.76 | 0.30 | 0.90 | 0.67 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other | her |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 115.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 23.0 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 85.9\% ICU Level of Service EAnalysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road



| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2330 | 2297 | 1039 | 2313 | 2305 | 1183 | 1050 | 0 | 0 | 1186 | 0 | 0 |
| Stage 1 | 1083 | 1083 |  | 1211 | 1211 | - | - | - | - | - | - | - |
| Stage 2 | 1247 | 1214 | - | 1102 | 1094 | - | - | - |  |  | - | - |
| Critical Hdwy | 7.14 | 6.5 | 6.38 | 7.1 | 6.5 | 6.2 | 4.18 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.14 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.14 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.536 | 4 | 3.462 | 3.5 | 4 | 3.3 | 2.272 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | $\sim 26$ | 39 | 261 | 27 | 39 | 233 | 640 | - |  | 596 | - | - |
| Stage 1 | 261 | 296 | - | 225 | 257 | - | - | - | - | - | - | - |
| Stage 2 | 211 | 257 | - | 259 | 292 | - | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | $\sim 17$ | 37 | 261 | 22 | 37 | 233 | 640 | - | - | 596 | - | - |
| Mov Cap-2 Maneuver | $\sim 17$ | 37 | - | 22 | 37 | - | - | - | - | - | - | - |
| Stage 1 | 255 | 285 | - | 220 | 251 | - | - | - | - | - | - | - |
| Stage 2 | 143 | 251 | - | 213 | 281 | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, S\$ | \$ 993.5 |  |  | 27.2 |  |  | 0.1 |  |  | 0.2 |  |  |
| HCM LOS | F |  |  | D |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | EBLn2V | NBLn1 | SBL | SBT | SBR |  |  |
| Capacity (veh/h) |  | 640 | - | - | 17 | 261 | 233 | 596 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.022 | - |  | 3.557 | 0.147 | 0.309 | 0.037 | - | - |  |  |
| HCM Control Delay (s) |  | 10.8 | - |  | 1610.5 | 21.2 | 27.2 | 11.3 | - | - |  |  |
| HCM Lane LOS |  | B | - | - | F | C | D | B | - | - |  |  |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 8.2 | 0.5 | 1.3 | 0.1 | - | - |  |  |
| $\frac{\text { Notes }}{\sim}$ Volume exceeds capacity |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2038) Total Traffic W3 Sunset Creek

AM Peak Hour

|  | 4 |  |  | 7 |  |  | $4$ | 9 | $p$ | $t$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 26 | 0 | 13 | 80 | 0 | 312 | 2 | 688 | 31 | 96 | 831 | 8 |
| Future Volume (vph) | 26 | 0 | 13 | 80 | 0 | 312 | 2 | 688 | 31 | 96 | 831 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 1.00 |  |  |  |  |  |  |  |
| Frt |  | 0.955 |  |  |  | 0.850 |  | 0.994 |  |  | 0.999 |  |
| Flt Protected |  | 0.968 |  |  | 0.950 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1717 | 0 | 0 | 1825 | 1633 | 1825 | 1806 | 0 | 1825 | 1862 | 0 |
| Flt Permitted |  | 0.779 |  |  | 0.728 |  | 0.115 |  |  | 0.204 |  |  |
| Satd. Flow (perm) | 0 | 1382 | 0 | 0 | 1397 | 1633 | 221 | 1806 | 0 | 392 | 1862 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 41 |  |  |  | 131 |  | 4 |  |  | 1 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Heavy Vehicles (\%) | 0\% | 0\% | 8\% | 0\% | 0\% | 0\% | 0\% | 6\% | 0\% | 0\% | 3\% | 12\% |
| Adj. Flow (vph) | 30 | 0 | 15 | 91 | 0 | 355 | 2 | 782 | 35 | 109 | 944 | 9 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 45 | 0 | 0 | 91 | 355 | 2 | 817 | 0 | 109 | 953 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 34.3 | 34.3 |  | 34.3 | 34.3 | 34.3 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 45.0 | 45.0 |  | 45.0 | 45.0 |  |
| Total Split (\%) | 43.8\% | 43.8\% |  | 43.8\% | 43.8\% | 43.8\% | 56.3\% | 56.3\% |  | 56.3\% | 56.3\% |  |
| Maximum Green (s) | 28.7 | 28.7 |  | 28.7 | 28.7 | 28.7 | 39.0 | 39.0 |  | 39.0 | 39.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 4.1 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 1.9 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 21.0 | 21.0 |  | 21.0 | 21.0 | 21.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) |  | 15.2 |  |  | 15.2 | 15.2 | 39.3 | 39.3 |  | 39.3 | 39.3 |  |
| Actuated g/C Ratio |  | 0.23 |  |  | 0.23 | 0.23 | 0.59 | 0.59 |  | 0.59 | 0.59 |  |
| v/c Ratio |  | 0.13 |  |  | 0.29 | 0.75 | 0.02 | 0.77 |  | 0.47 | 0.87 |  |



Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


|  | 4 |  |  |  |  |  |  | 4 |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | ¢ |  | \% | $\hat{F}$ |  | \% | 4 | F | \% | $\hat{\dagger}$ |  |
| Traffic Volume (vph) | 43 | 4 | 97 | 213 | - | 74 | 64 | 607 | 53 | 26 | 854 | 34 |
| Future Volume (vph) | 43 | 4 | 97 | 213 | 6 | 74 | 64 | 607 | 53 | 26 | 854 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.855 |  |  | 0.862 |  |  |  | 0.850 |  | 0.994 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1539 | 0 | 1825 | 1656 | 0 | 1690 | 1746 | 1633 | 1825 | 1793 | 0 |
| Flt Permitted | 0.699 |  |  | 0.684 |  |  | 0.118 |  |  | 0.311 |  |  |
| Satd. Flow (perm) | 1304 | 1539 | 0 | 1314 | 1656 | 0 | 210 | 1746 | 1633 | 597 | 1793 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 109 |  |  | 83 |  |  |  | 60 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 3\% | 0\% | 7\% | 0\% | 0\% | 0\% | 8\% | 10\% | 0\% | 0\% | 6\% | 19\% |
| Adj. Flow (vph) | 48 | 4 | 109 | 239 | 7 | 83 | 72 | 682 | 60 | 29 | 960 | 38 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 48 | 113 | 0 | 239 | 90 | 0 | 72 | 682 | 60 | 29 | 998 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 55.0 | 55.0 | 55.0 | 55.0 | 55.0 |  |
| Total Split (\%) | 31.3\% | 31.3\% |  | 31.3\% | 31.3\% |  | 68.8\% | 68.8\% | 68.8\% | 68.8\% | 68.8\% |  |
| Maximum Green (s) | 19.3 | 19.3 |  | 19.3 | 19.3 |  | 48.6 | 48.6 | 48.6 | 48.6 | 48.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 17.4 | 17.4 |  | 17.4 | 17.4 |  | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 |  |
| Actuated g/C Ratio | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 0.63 | 0.63 | 0.63 | 0.63 | 0.63 |  |
| v/c Ratio | 0.17 | 0.27 |  | 0.83 | 0.21 |  | 0.55 | 0.62 | 0.06 | 0.08 | 0.89 |  |
| Control Delay | 25.8 | 7.6 |  | 53.8 | 8.4 |  | 30.0 | 12.7 | 2.1 | 7.2 | 25.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |


|  | 4 |  |  | 7 |  |  |  | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Total Delay | 25.8 | 7.6 |  | 53.8 | 8.4 |  | 30.0 | 12.7 | 2.1 | 7.2 | 25.1 |  |
| LOS | C | A |  | D | A |  | C | B | A | A | C |  |
| Approach Delay |  | 13.0 |  |  | 41.4 |  |  | 13.5 |  |  | 24.6 |  |
| Approach LOS |  | B |  |  | D |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 5.8 | 0.5 |  | 33.7 | 0.8 |  | 5.9 | 60.1 | 0.0 | 1.6 | 120.1 |  |
| Queue Length 95th (m) | 13.9 | 11.8 |  | \#66.3 | 11.1 |  | \#27.0 | 91.5 | 3.9 | 4.8 | \#210.4 |  |
| Internal Link Dist (m) |  | 444.4 |  |  | 226.7 |  |  | 276.3 |  |  | 343.6 |  |
| Turn Bay Length (m) | 45.0 |  |  |  |  |  | 55.0 |  | 60.0 | 45.0 |  |  |
| Base Capacity (vph) | 317 | 457 |  | 320 | 466 |  | 131 | 1095 | 1046 | 374 | 1127 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.25 |  | 0.75 | 0.19 |  | 0.55 | 0.62 | 0.06 | 0.08 | 0.89 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 79.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.89 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 22.3 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 81.7\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomadeS(\&AB8) Total Traffic W3 Sunset Creek

|  | 4 |  |  | $\dagger$ | - | 4 | 4 | $\uparrow$ | 7 |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | \% | 4 | F | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\hat{\dagger}$ |  |
| Traffic Volume (vph) | 69 | 648 | 43 | 187 | 746 | 99 | 61 | 91 | 270 | 155 | 35 | 153 |
| Future Volume (vph) | 69 | 648 | 43 | 187 | 746 | 99 | 61 | 91 | 270 | 155 | 35 | 153 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 |  |  |  |  | 0.98 | 0.98 | 0.98 |  | 1.00 | 0.96 |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  | 0.888 |  |  | 0.878 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1722 | 1812 | 0 | 1738 | 1812 | 1541 | 1789 | 1572 | 0 | 1674 | 1430 | 0 |
| Flt Permitted | 0.181 |  |  | 0.221 |  |  | 0.630 |  |  | 0.193 |  |  |
| Satd. Flow (perm) | 328 | 1812 | 0 | 404 | 1812 | 1506 | 1162 | 1572 | 0 | 340 | 1430 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  |  | 106 |  | 152 |  |  | 158 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) | 2 |  |  |  |  | 2 | 12 |  | 1 | 1 |  | 12 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 6\% | 5\% | 6\% | 5\% | 6\% | 6\% | 2\% | 6\% | 7\% | 9\% | 7\% | 15\% |
| Adj. Flow (vph) | 75 | 704 | 47 | 203 | 811 | 108 | 66 | 99 | 293 | 168 | 38 | 166 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 75 | 751 | 0 | 203 | 811 | 108 | 66 | 392 | 0 | 168 | 204 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  | 7 | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 5.0 | 7.0 |  |
| Minimum Split (s) | 44.1 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 8.0 | 26.0 |  |
| Total Split (s) | 56.0 | 56.0 |  | 56.0 | 56.0 | 56.0 | 26.0 | 26.0 |  | 8.0 | 34.0 |  |
| Total Split (\%) | 62.2\% | 62.2\% |  | 62.2\% | 62.2\% | 62.2\% | 28.9\% | 28.9\% |  | 8.9\% | 37.8\% |  |
| Maximum Green (s) | 49.9 | 49.9 |  | 49.9 | 49.9 | 49.9 | 20.0 | 20.0 |  | 5.0 | 28.0 |  |
| Yellow Time (s) | 3.3 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.0 | 3.3 |  |
| All-Red Time (s) | 2.8 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 0.0 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.1 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | Max |  | Max | Max | Max | None | None |  | None | None |  |
| Walk Time (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  |  | 13.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Effct Green (s) | 50.0 | 50.0 |  | 50.0 | 50.0 | 50.0 | 17.7 | 17.7 |  | 28.7 | 25.7 |  |
| Actuated g/C Ratio | 0.57 | 0.57 |  | 0.57 | 0.57 | 0.57 | 0.20 | 0.20 |  | 0.33 | 0.29 |  |
| v/c Ratio | 0.40 | 0.73 |  | 0.89 | 0.79 | 0.12 | 0.28 | 0.90 |  | 0.90 | 0.39 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomateS(\&AB8) Total Traffic W3 Sunset Creek


Splits and Phases: 9: Campbell Street/Campbell Street North \& Main StreetWharncliffe Road South


|  | 4 |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | f |  | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ | 「 | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 57 | 90 | 52 | 348 | 110 | 326 | 68 | 997 | 271 | 184 | 812 | 57 |
| Future Volume (vph) | 57 | 90 | 52 | 348 | 110 | 326 | 68 | 997 | 271 | 184 | 812 | 57 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 55.0 |  | 0.0 | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 0.99 |  | 0.99 |  | 0.97 | 1.00 |  | 0.98 |  | 1.00 |  |
| Frt |  | 0.945 |  |  |  | 0.850 |  |  | 0.850 |  | 0.990 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1755 | 1692 | 0 | 1825 | 1921 | 1585 | 1789 | 1883 | 1601 | 1789 | 1827 | 0 |
| Flt Permitted | 0.682 |  |  | 0.405 |  |  | 0.183 |  |  | 0.056 |  |  |
| Satd. Flow (perm) | 1249 | 1692 | 0 | 771 | 1921 | 1538 | 344 | 1883 | 1576 | 105 | 1827 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 19 |  |  |  | 191 |  |  | 140 |  | 5 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 559.5 |  |  | 2005.5 |  |  | 477.6 |  |  | 496.5 |  |
| Travel Time (s) |  | 33.6 |  |  | 120.3 |  |  | 28.7 |  |  | 29.8 |  |
| Confl. Peds. (\#/hr) | 3 |  | 4 | 4 |  | 3 | 4 |  | 4 | 4 |  | 4 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 4\% | 6\% | 6\% | 0\% | 0\% | 3\% | 2\% | 2\% | 2\% | 2\% | 4\% | 3\% |
| Adj. Flow (vph) | 61 | 96 | 55 | 370 | 117 | 347 | 72 | 1061 | 288 | 196 | 864 | 61 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 61 | 151 | 0 | 370 | 117 | 347 | 72 | 1061 | 288 | 196 | 925 | 0 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA |  |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 2 | 2 | 2 | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 |  |
| Minimum Split (s) | 25.2 | 25.2 |  | 8.0 | 25.2 | 25.2 | 45.9 | 45.9 | 45.9 | 8.0 | 45.9 |  |
| Total Split (s) | 26.0 | 26.0 |  | 18.0 | 44.0 | 44.0 | 74.0 | 74.0 | 74.0 | 12.0 | 86.0 |  |
| Total Split (\%) | 20.0\% | 20.0\% |  | 13.8\% | 33.8\% | 33.8\% | 56.9\% | 56.9\% | 56.9\% | 9.2\% | 66.2\% |  |
| Maximum Green (s) | 19.8 | 19.8 |  | 15.0 | 37.8 | 37.8 | 68.1 | 68.1 | 68.1 | 9.0 | 80.1 |  |
| Yellow Time (s) | 4.3 | 4.3 |  | 3.0 | 4.3 | 4.3 | 3.8 | 3.8 | 3.8 | 3.0 | 3.8 |  |
| All-Red Time (s) | 1.9 | 1.9 |  | 0.0 | 1.9 | 1.9 | 2.1 | 2.1 | 2.1 | 0.0 | 2.1 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.2 | 6.2 |  | 3.0 | 6.2 | 6.2 | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 |  |
| Lead/Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max | Max | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 | 7.0 | 28.0 | 28.0 | 28.0 |  | 28.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  |  | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  | 12.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 |  |
| Act Effct Green (s) | 14.7 | 14.7 |  | 35.9 | 32.7 | 32.7 | 68.1 | 68.1 | 68.1 | 83.1 | 80.2 |  |
| Actuated g/C Ratio | 0.12 | 0.12 |  | 0.29 | 0.26 | 0.26 | 0.54 | 0.54 | 0.54 | 0.66 | 0.64 |  |
| v/c Ratio | 0.41 | 0.70 |  | 1.06 | 0.23 | 0.64 | 0.39 | 1.03 | 0.31 | 1.03 | 0.79 |  |


|  | 4 |  |  |  |  |  |  | $\uparrow$ | $>$ | , | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 59.5 | 63.5 |  | 106.1 | 37.2 | 23.3 | 25.3 | 66.3 | 9.0 | 104.1 | 23.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 59.5 | 63.5 |  | 106.1 | 37.2 | 23.3 | 25.3 | 66.3 | 9.0 | 104.1 | 23.2 |  |
| LOS | E | E |  | F | D | C | C | E | A | F | C |  |
| Approach Delay |  | 62.3 |  |  | 62.0 |  |  | 52.6 |  |  | 37.4 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | D |  |
| Queue Length 50th (m) | 14.1 | 31.6 |  | $\sim 87.7$ | 22.7 | 33.6 | 9.8 | ~281.5 | 17.7 | $\sim 35.3$ | 154.3 |  |
| Queue Length 95th (m) | 28.1 | 53.7 |  | \#160.0 | 38.4 | 65.4 | 25.0 | \#381.0 | 37.2 | \#87.3 | 237.9 |  |
| Internal Link Dist (m) |  | 535.5 |  |  | 1981.5 |  |  | 453.6 |  |  | 472.5 |  |
| Turn Bay Length (m) | 55.0 |  |  | 55.0 |  | 60.0 | 80.0 |  | 60.0 | 120.0 |  |  |
| Base Capacity (vph) | 198 | 284 |  | 348 | 581 | 598 | 187 | 1026 | 922 | 191 | 1173 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | , | , | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.31 | 0.53 |  | 1.06 | 0.20 | 0.58 | 0.39 | 1.03 | 0.31 | 1.03 | 0.79 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 50.6 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 107.7\% |  |  |  |  | ICU Level of Service G |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Colonel Talbot Road \& Pack Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 20 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | F |  |  | \$ |  | ${ }^{7}$ | 个 |  | ${ }^{7}$ | F |  |
| Traffic Vol, veh/h | 31 | 0 | 24 | 0 | 0 | 34 | 33 | 1279 | 14 | 54 | 1036 | 53 |
| Future Vol, veh/h | 31 | 0 | 24 | 0 | 0 | 34 | 33 | 1279 | 14 | 54 | 1036 | 53 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stor | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 30 | - | - | - | - | - | 110 | - | - | 45 | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 4 | 0 | 0 | 0 | 3 | 1 | 0 | 0 | 3 | 0 |
| Mvmt Flow | 33 | 0 | 25 | 0 | 0 | 36 | 35 | 1346 | 15 | 57 | 1091 | 56 |


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2675 | 2664 | 1119 | 2670 | 2685 | 1354 | 1147 | 0 | 0 | 1361 | 0 | 0 |
| Stage 1 | 1233 | 1233 | - | 1424 | 1424 | - |  | - | - | - | - | - |
| Stage 2 | 1442 | 1431 | - | 1246 | 1261 | - | - | - |  |  | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.24 | 7.1 | 6.5 | 6.2 | 4.13 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 4 | 3.336 | 3.5 | 4 | 3.3 | 2.227 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | ~15 | 23 | 249 | 15 | 22 | 185 | 605 | - | - | 512 | - | - |
| Stage 1 | 219 | 251 | - | 170 | 204 | - | - | - | - | - | - | - |
| Stage 2 | 166 | 202 | - | 215 | 244 | - | - | - | - | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | $\sim 11$ | 19 | 249 | 12 | 18 | 185 | 605 | - | - | 512 | - | - |
| Mov Cap-2 Maneuver | $\sim 11$ | 19 | - | 12 | 18 | - | - | - | - | - | - | - |
| Stage 1 | 206 | 223 | - | 160 | 192 | - | - | - | - | - | - | - |
| Stage 2 | 126 | 190 | - | 172 | 217 | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, S\$ | \$ 894.2 |  |  | 29.1 |  |  | 0.3 |  |  | 0.6 |  |  |
| HCM LOS | F |  |  | D |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | EBLn2V | WBLn1 | SBL | SBT | SBR |  |  |
| Capacity (veh/h) |  | 605 | - | - | 11 | 249 | 185 | 512 | - | - |  |  |
| HCM Lane V/C Ratio |  | 0.057 | - |  | 2.967 | 0.101 | 0.193 | 0.111 |  | - |  |  |
| HCM Control Delay (s) |  | 11.3 | - |  | 1570.1 | 21.1 | 29.1 | 12.9 |  | - |  |  |
| HCM Lane LOS |  | B | - | - | F | C | D | B | - | - |  |  |
| HCM 95th \%tile Q(veh) |  | 0.2 | - | - | 5.1 | 0.3 | 0.7 | 0.4 | - | - |  |  |
| $\frac{\text { Notes }}{\sim} \sim$ Volume exceeds capacity |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2038) Total Traffic W3 Sunset Creek

PM Peak Hour

|  | 4 |  |  | 7 | $4$ |  | $4$ | 9 | $p$ | $\pm$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1142 | 96 | 241 | 800 | 26 |
| Future Volume (vph) | 13 | 0 | 6 | 34 | 2 | 170 | 10 | 1142 | 96 | 241 | 800 | 26 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 |  | 0.0 | 0.0 |  | 60.0 | 75.0 |  | 0.0 | 75.0 |  | 80.0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 |  |  | 0.98 |  | 0.98 |  |  |  | 1.00 |  |
| Frt |  | 0.959 |  |  |  | 0.850 |  | 0.988 |  |  | 0.995 |  |
| Flt Protected |  | 0.966 |  |  | 0.955 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1664 | 0 | 0 | 1835 | 1633 | 1825 | 1881 | 0 | 1825 | 1848 | 0 |
| Flt Permitted |  | 0.768 |  |  | 0.723 |  | 0.341 |  |  | 0.047 |  |  |
| Satd. Flow (perm) | 0 | 1323 | 0 | 0 | 1361 | 1633 | 639 | 1881 | 0 | 90 | 1848 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 50 |  |  |  | 179 |  | 6 |  |  | 4 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 287.7 |  |  | 284.1 |  |  | 119.4 |  |  | 298.9 |  |
| Travel Time (s) |  | 20.7 |  |  | 20.5 |  |  | 7.2 |  |  | 17.9 |  |
| Confl. Peds. (\#/hr) |  |  | 6 | 6 |  |  | 28 |  |  |  |  | 28 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 8\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 3\% | 4\% |
| Adj. Flow (vph) | 14 | 0 | 6 | 36 | 2 | 179 | 11 | 1202 | 101 | 254 | 842 | 27 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 20 | 0 | 0 | 38 | 179 | 11 | 1303 | 0 | 254 | 869 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 | 8 | 2 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.3 | 24.3 |  | 24.3 | 24.3 | 24.3 | 24.0 | 24.0 |  | 8.0 | 24.0 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 | 25.0 | 89.0 | 89.0 |  | 16.0 | 105.0 |  |
| Total Split (\%) | 19.2\% | 19.2\% |  | 19.2\% | 19.2\% | 19.2\% | 68.5\% | 68.5\% |  | 12.3\% | 80.8\% |  |
| Maximum Green (s) | 18.7 | 18.7 |  | 18.7 | 18.7 | 18.7 | 83.0 | 83.0 |  | 13.0 | 99.0 |  |
| Yellow Time (s) | 3.6 | 3.6 |  | 3.6 | 3.6 | 3.6 | 4.1 | 4.1 |  | 3.0 | 4.1 |  |
| All-Red Time (s) | 2.7 | 2.7 |  | 2.7 | 2.7 | 2.7 | 1.9 | 1.9 |  | 0.0 | 1.9 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.3 |  |  | 6.3 | 6.3 | 6.0 | 6.0 |  | 3.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lag | Lag |  | Lead |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes | Yes |  | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Max | Max |  | None | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  |  | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |  | 0 |  |
| Act Effct Green (s) |  | 8.9 |  |  | 8.9 | 8.9 | 83.0 | 83.0 |  | 102.0 | 99.0 |  |
| Actuated g/C Ratio |  | 0.07 |  |  | 0.07 | 0.07 | 0.69 | 0.69 |  | 0.85 | 0.82 |  |
| v/c Ratio |  | 0.14 |  |  | 0.38 | 0.63 | 0.02 | 1.00 |  | 0.96 | 0.57 |  |

3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue Future (2038) Total Traffic W3 Sunset Creek

| 4 |  |  |  |  |  | 4 | 4 |  |  |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Control Delay | 2.5 |  |  | 63.7 | 17.7 | 6.8 | 45.1 |  | 82.7 | 5.5 |  |
| Queue Delay | 0.0 |  |  | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 2.5 |  |  | 63.7 | 17.7 | 6.8 | 45.1 |  | 82.7 | 5.5 |  |
| LOS | A |  |  | E | B | A | D |  | F | A |  |
| Approach Delay | 2.5 |  |  | 25.7 |  |  | 44.7 |  |  | 23.0 |  |
| Approach LOS | A |  |  | C |  |  | D |  |  | C |  |
| Queue Length 50th (m) | 0.0 |  |  | 8.7 | 0.0 | 0.7 | $\sim 276.4$ |  | 43.3 | 51.9 |  |
| Queue Length 95th ( m ) | 0.9 |  |  | 19.9 | 20.7 | 2.9 | \#423.9 |  | \#100.0 | 92.0 |  |
| Internal Link Dist (m) | 263.7 |  |  | 260.1 |  |  | 95.4 |  |  | 274.9 |  |
| Turn Bay Length ( m ) |  |  |  |  | 60.0 | 75.0 |  |  | 75.0 |  |  |
| Base Capacity (vph) | 247 |  |  | 211 | 405 | 441 | 1301 |  | 264 | 1523 |  |
| Starvation Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.08 |  |  | 0.18 | 0.44 | 0.02 | 1.00 |  | 0.96 | 0.57 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120.2 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.00 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 33.7 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 102.1\%Analysis Period (min) 15 |  |  |  | ICU Level of Service G |  |  |  |  |  |  |  |
|  |  |  |  | Analysis Period (min) 15 |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Colonel Talbot Road \& Diane Crescent/Royal Magnolia Avenue


|  | 4 |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | f |  | \% | F |  | ${ }^{7}$ | $\uparrow$ | 「 | * | F |  |
| Traffic Volume (vph) | 41 | 9 | 83 | 136 | 10 | 49 | 112 | 1161 | 223 | 72 | 698 | 67 |
| Future Volume (vph) | 41 | 9 | 83 | 136 | 10 | 49 | 112 | 1161 | 223 | 72 | 698 | 67 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 0.0 | 55.0 |  | 60.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |
| Taper Length ( m ) | 7.6 |  |  | 2.5 |  |  | 7.6 |  |  | 7.6 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.98 |  | 1.00 |  |  |  |  |  |  |  |  |
| Frt |  | 0.865 |  |  | 0.876 |  |  |  | 0.850 |  | 0.987 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1772 | 1599 | 0 | 1825 | 1683 | 0 | 1825 | 1902 | 1633 | 1825 | 1826 | 0 |
| Flt Permitted | 0.715 |  |  | 0.693 |  |  | 0.282 |  |  | 0.074 |  |  |
| Satd. Flow (perm) | 1334 | 1599 | 0 | 1328 | 1683 | 0 | 542 | 1902 | 1633 | 142 | 1826 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 89 |  |  | 53 |  |  |  | 203 |  | 11 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 468.4 |  |  | 250.7 |  |  | 300.3 |  |  | 367.6 |  |
| Travel Time (s) |  | 28.1 |  |  | 15.0 |  |  | 18.0 |  |  | 22.1 |  |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 3\% | 0\% | 2\% | 0\% | 0\% | 0\% | 0\% | 1\% | 0\% | 0\% | 4\% | 2\% |
| Adj. Flow (vph) | 44 | 10 | 89 | 146 | 11 | 53 | 120 | 1248 | 240 | 77 | 751 | 72 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 44 | 99 | 0 | 146 | 64 | 0 | 120 | 1248 | 240 | 77 | 823 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 | 2 | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Minimum Split (s) | 23.7 | 23.7 |  | 23.7 | 23.7 |  | 43.4 | 43.4 | 43.4 | 43.4 | 43.4 |  |
| Total Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 |  |
| Total Split (\%) | 21.8\% | 21.8\% |  | 21.8\% | 21.8\% |  | 78.2\% | 78.2\% | 78.2\% | 78.2\% | 78.2\% |  |
| Maximum Green (s) | 18.3 | 18.3 |  | 18.3 | 18.3 |  | 79.6 | 79.6 | 79.6 | 79.6 | 79.6 |  |
| Yellow Time (s) | 3.7 | 3.7 |  | 3.7 | 3.7 |  | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 5.7 | 5.7 |  | 5.7 | 5.7 |  | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | Max | Max | Max | Max | Max |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Act Effct Green (s) | 15.9 | 15.9 |  | 15.9 | 15.9 |  | 82.5 | 82.5 | 82.5 | 82.5 | 82.5 |  |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.14 | 0.14 |  | 0.75 | 0.75 | 0.75 | 0.75 | 0.75 |  |
| v/c Ratio | 0.23 | 0.32 |  | 0.77 | 0.22 |  | 0.30 | 0.88 | 0.19 | 0.73 | 0.60 |  |



Splits and Phases: 4: Colonel Talbot Road \& Kilbourne Road/Hayward Drive


9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomateS(』AB8) Total Traffic W3 Sunset Creek

|  | 4 |  |  |  |  |  |  | 4 |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\dagger}$ |  | \% | $\uparrow$ | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\hat{\dagger}$ |  |
| Traffic Volume (vph) | 182 | 874 | 50 | 132 | 935 | 146 | 41 | 46 | 87 | 123 | 50 | 136 |
| Future Volume (vph) | 182 | 874 | 50 | 132 | 935 | 146 | 41 | 46 | 87 | 123 | 50 | 136 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 45.0 |  | 0.0 | 0.0 |  | 60.0 | 5.0 |  | 0.0 | 45.0 |  | 0.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  | 2.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  | 1.00 |  |  |  | 0.98 |  |
| Frt |  | 0.992 |  |  |  | 0.850 |  | 0.902 |  |  | 0.890 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1825 | 1850 | 0 | 1772 | 1902 | 1633 | 1825 | 1689 | 0 | 1825 | 1679 | 0 |
| Flt Permitted | 0.066 |  |  | 0.219 |  |  | 0.440 |  |  | 0.604 |  |  |
| Satd. Flow (perm) | 127 | 1850 | 0 | 408 | 1902 | 1633 | 842 | 1689 | 0 | 1160 | 1679 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  |  | 125 |  | 86 |  |  | 123 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 346.2 |  |  | 367.0 |  |  | 288.8 |  |  | 243.6 |  |
| Travel Time (s) |  | 24.9 |  |  | 26.4 |  |  | 20.8 |  |  | 17.5 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  |  |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 0\% | 3\% | 3\% | 3\% | 1\% | 0\% | 0\% | 0\% | 4\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 198 | 950 | 54 | 143 | 1016 | 159 | 45 | 50 | 95 | 134 | 54 | 148 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 198 | 1004 | 0 | 143 | 1016 | 159 | 45 | 145 | 0 | 134 | 202 | 0 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  |  |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 5 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 8.0 | 44.1 |  | 44.1 | 44.1 | 44.1 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 8.0 | 74.0 |  | 66.0 | 66.0 | 66.0 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (\%) | 8.0\% | 74.0\% |  | 66.0\% | 66.0\% | 66.0\% | 26.0\% | 26.0\% |  | 26.0\% | 26.0\% |  |
| Maximum Green (s) | 5.0 | 67.9 |  | 59.9 | 59.9 | 59.9 | 20.0 | 20.0 |  | 20.0 | 20.0 |  |
| Yellow Time (s) | 3.0 | 3.3 |  | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |  | 3.3 | 3.3 |  |
| All-Red Time (s) | 0.0 | 2.8 |  | 2.8 | 2.8 | 2.8 | 2.7 | 2.7 |  | 2.7 | 2.7 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 3.0 | 6.1 |  | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C-Max |  | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) |  | 25.0 |  | 25.0 | 25.0 | 25.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 13.0 |  | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Efftt Green (s) | 75.5 | 72.4 |  | 59.9 | 59.9 | 59.9 | 15.5 | 15.5 |  | 15.5 | 15.5 |  |
| Actuated g/C Ratio | 0.76 | 0.72 |  | 0.60 | 0.60 | 0.60 | 0.16 | 0.16 |  | 0.16 | 0.16 |  |
| v/c Ratio | 0.77 | 0.75 |  | 0.59 | 0.89 | 0.15 | 0.35 | 0.43 |  | 0.74 | 0.55 |  |

9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe RomateS(\&AB8) Total Traffic W3 Sunset Creek


Splits and Phases: 9: Campbell Street/Campbell Street North \& Main Street/Wharncliffe Road South


## MOVEMENT SUMMARY

$\nexists$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: BG 2033 AM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2033) Background Traffic
AM Peak Hour
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: IBI GROUP | Licence: PLUS / 1PC | Processed: August 8, 2023 10:09:43 AM
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IW3SunsetCreek_2023-07-18.sip9

## MOVEMENT SUMMARY

$\nexists$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: BG 2033 PM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2033) Background Traffic
PM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  |  | DEMAND FLOWS | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 247 | 2.0 | 268 | 2.0 | 0.638 | 14.8 | LOS B | 6.2 | 47.7 | 0.76 | 0.97 | 1.33 | 48.3 |
| 8 T1 | 710 | 1.0 | 772 | 1.0 | 0.638 | 14.1 | LOS B | 6.4 | 48.8 | 0.75 | 0.96 | 1.31 | 49.7 |
| 18 R2 | 67 | 0.0 | 73 | 0.0 | 0.638 | 13.8 | LOS B | 6.4 | 48.8 | 0.75 | 0.95 | 1.30 | 49.2 |
| Approach | 1024 | 1.2 | 1113 | 1.2 | 0.638 | 14.3 | LOS B | 6.4 | 48.8 | 0.75 | 0.96 | 1.31 | 49.3 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 74 | 0.0 | 80 | 0.0 | 0.453 | 16.9 | LOS C | 2.1 | 15.8 | 0.79 | 0.89 | 1.15 | 47.5 |
| 6 T1 | 259 | 0.0 | 282 | 0.0 | 0.453 | 15.9 | LOS C | 2.1 | 16.1 | 0.78 | 0.88 | 1.14 | 48.6 |
| 16 R 2 | 65 | 0.0 | 71 | 0.0 | 0.453 | 15.1 | LOS C | 2.1 | 16.1 | 0.77 | 0.87 | 1.13 | 48.3 |
| Approach | 398 | 0.0 | 433 | 0.0 | 0.453 | 15.9 | LOS C | 2.1 | 16.1 | 0.78 | 0.88 | 1.14 | 48.3 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 70 | 0.0 | 76 | 0.0 | 0.468 | 11.5 | LOS B | 2.7 | 21.0 | 0.68 | 0.77 | 0.96 | 51.4 |
| 4 T1 | 420 | 6.0 | 457 | 6.0 | 0.468 | 11.4 | LOS B | 2.7 | 21.2 | 0.67 | 0.76 | 0.95 | 51.6 |
| 14 R2 | 163 | 1.0 | 177 | 1.0 | 0.468 | 10.6 | LOS B | 2.7 | 21.2 | 0.66 | 0.75 | 0.93 | 51.1 |
| Approach | 653 | 4.1 | 710 | 4.1 | 0.468 | 11.2 | LOS B | 2.7 | 21.2 | 0.67 | 0.76 | 0.94 | 51.5 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 141 | 0.0 | 153 | 0.0 | 0.373 | 9.5 | LOS A | 1.8 | 13.7 | 0.64 | 0.68 | 0.75 | 51.7 |
| 2 T1 | 258 | 0.0 | 280 | 0.0 | 0.373 | 9.1 | LOS A | 1.8 | 13.7 | 0.63 | 0.66 | 0.73 | 52.9 |
| 12 R 2 | 135 | 4.0 | 147 | 4.0 | 0.373 | 9.0 | LOS A | 1.7 | 13.4 | 0.62 | 0.65 | 0.71 | 52.3 |
| Approach | 534 | 1.0 | 580 | 1.0 | 0.373 | 9.2 | LOS A | 1.8 | 13.7 | 0.63 | 0.66 | 0.73 | 52.4 |
| All Vehicles | 2609 | 1.7 | 2836 | 1.7 | 0.638 | 12.7 | LOS B | 6.4 | 48.8 | 0.71 | 0.84 | 1.07 | 50.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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IW3SunsetCreek_2023-07-18.sip9

## MOVEMENT SUMMARY

$\nexists$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: BG 2038 AM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2038) Background Traffic
AM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID |  | $\begin{aligned} & \text { IN } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { IT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{array}$ | $\begin{gathered} \hline \text { ND } \\ \text { NS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | $\begin{array}{r} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{array}$ | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. <br> Cycles | Aver. Speed <br> km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 90 | 9.0 | 98 | 9.0 | 0.440 | 10.5 | LOS B | 2.3 | 18.9 | 0.62 | 0.68 | 0.79 | 51.6 |
| 8 | T1 | 498 | 9.0 | 541 | 9.0 | 0.440 | 10.0 | LOS B | 2.3 | 18.8 | 0.61 | 0.66 | 0.77 | 52.5 |
| 18 | R2 | 73 | 0.0 | 79 | 0.0 | 0.440 | 9.4 | LOS A | 2.3 | 18.8 | 0.60 | 0.65 | 0.75 | 52.0 |
| Appr | ach | 661 | 8.0 | 718 | 8.0 | 0.440 | 10.0 | LOS B | 2.3 | 18.9 | 0.61 | 0.67 | 0.77 | 52.3 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 42 | 0.0 | 46 | 0.0 | 0.195 | 8.3 | LOS A | 0.7 | 5.5 | 0.63 | 0.63 | 0.63 | 53.2 |
| 6 | T1 | 140 | 0.0 | 152 | 0.0 | 0.195 | 7.9 | LOS A | 0.7 | 5.5 | 0.62 | 0.62 | 0.62 | 54.1 |
|  | R2 | 50 | 0.0 | 54 | 0.0 | 0.195 | 7.5 | LOS A | 0.7 | 5.4 | 0.61 | 0.61 | 0.61 | 53.5 |
| Appr | ach | 232 | 0.0 | 252 | 0.0 | 0.195 | 7.9 | LOS A | 0.7 | 5.5 | 0.62 | 0.62 | 0.62 | 53.8 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 48 | 0.0 | 52 | 0.0 | 0.285 | 6.4 | LOS A | 1.3 | 9.8 | 0.46 | 0.37 | 0.46 | 55.5 |
| 4 | T1 | 409 | 3.0 | 445 | 3.0 | 0.285 | 6.3 | LOS A | 1.3 | 9.8 | 0.45 | 0.36 | 0.45 | 55.7 |
| 14 | R2 | 83 | 4.0 | 90 | 4.0 | 0.285 | 6.2 | LOS A | 1.2 | 9.6 | 0.44 | 0.34 | 0.44 | 54.4 |
| Approach |  | 540 | 2.9 | 587 | 2.9 | 0.285 | 6.3 | LOS A | 1.3 | 9.8 | 0.45 | 0.35 | 0.45 | 55.5 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 151 | 0.0 | 164 | 0.0 | 0.390 | 9.2 | LOS A | 2.0 | 15.0 | 0.63 | 0.66 | 0.72 | 52.0 |
| 2 | T1 | 271 | 0.0 | 295 | 0.0 | 0.390 | 8.9 | LOS A | 2.0 | 15.0 | 0.62 | 0.65 | 0.70 | 53.0 |
| 12 | R2 | 182 | 2.0 | 198 | 2.0 | 0.390 | 8.7 | LOS A | 1.9 | 14.6 | 0.60 | 0.63 | 0.68 | 52.5 |
| Appr | oach | 604 | 0.6 | 657 | 0.6 | 0.390 | 8.9 | LOS A | 2.0 | 15.0 | 0.61 | 0.64 | 0.70 | 52.6 |
| All V | hicles | 2037 | 3.5 | 2214 | 3.5 | 0.440 | 8.5 | LOS A | 2.3 | 18.9 | 0.57 | 0.57 | 0.65 | 53.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nexists$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: BG 2038 PM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2038) Background Traffic
PM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 262 | 2.0 | 285 | 2.0 | 0.683 | 16.9 | LOS C | 7.3 | 56.3 | 0.80 | 1.06 | 1.51 | 47.1 |
| 8 T1 | 741 | 1.0 | 805 | 1.0 | 0.683 | 16.1 | LOS C | 7.6 | 57.9 | 0.80 | 1.05 | 1.49 | 48.5 |
| 18 R2 | 68 | 0.0 | 74 | 0.0 | 0.683 | 15.7 | LOS C | 7.6 | 57.9 | 0.79 | 1.04 | 1.48 | 48.0 |
| Approach | 1071 | 1.2 | 1164 | 1.2 | 0.683 | 16.2 | LOS C | 7.6 | 57.9 | 0.80 | 1.05 | 1.50 | 48.1 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 75 | 0.0 | 82 | 0.0 | 0.503 | 19.4 | LOS C | 2.4 | 18.2 | 0.82 | 0.94 | 1.27 | 46.1 |
| 6 T1 | 273 | 0.0 | 297 | 0.0 | 0.503 | 18.2 | LOS C | 2.4 | 18.5 | 0.80 | 0.93 | 1.25 | 47.2 |
| 16 R 2 | 71 | 0.0 | 77 | 0.0 | 0.503 | 17.2 | LOS C | 2.4 | 18.5 | 0.80 | 0.92 | 1.24 | 47.0 |
| Approach | 419 | 0.0 | 455 | 0.0 | 0.503 | 18.2 | LOS C | 2.4 | 18.5 | 0.80 | 0.93 | 1.25 | 47.0 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 75 | 0.0 | 82 | 0.0 | 0.497 | 12.4 | LOS B | 3.0 | 23.4 | 0.70 | 0.82 | 1.05 | 50.7 |
| 4 T1 | 431 | 6.0 | 468 | 6.0 | 0.497 | 12.3 | LOS B | 3.0 | 23.7 | 0.69 | 0.81 | 1.03 | 51.0 |
| 14 R2 | 168 | 1.0 | 183 | 1.0 | 0.497 | 11.5 | LOS B | 3.0 | 23.7 | 0.68 | 0.80 | 1.02 | 50.5 |
| Approach | 674 | 4.1 | 733 | 4.1 | 0.497 | 12.1 | LOS B | 3.0 | 23.7 | 0.69 | 0.81 | 1.03 | 50.8 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 148 | 0.0 | 161 | 0.0 | 0.398 | 10.1 | LOS B | 2.0 | 15.5 | 0.66 | 0.71 | 0.82 | 51.3 |
| 2 T1 | 271 | 0.0 | 295 | 0.0 | 0.398 | 9.7 | LOS A | 2.0 | 15.5 | 0.65 | 0.70 | 0.80 | 52.4 |
| 12 R 2 | 142 | 4.0 | 154 | 4.0 | 0.398 | 9.6 | LOS A | 2.0 | 15.2 | 0.64 | 0.69 | 0.78 | 51.9 |
| Approach | 561 | 1.0 | 610 | 1.0 | 0.398 | 9.8 | LOS A | 2.0 | 15.5 | 0.65 | 0.70 | 0.80 | 52.0 |
| All Vehicles | 2725 | 1.7 | 2962 | 1.7 | 0.683 | 14.2 | LOS B | 7.6 | 57.9 | 0.74 | 0.90 | 1.20 | 49.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\forall$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: TT 2033 AM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2033) Total Traffic
AM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 85 | 9.0 | 92 | 9.0 | 0.489 | 12.3 | LOS B | 2.8 | 23.1 | 0.67 | 0.78 | 0.99 | 50.4 |
| 8 | T1 | 488 | 9.0 | 530 | 9.0 | 0.489 | 11.8 | LOS B | 2.9 | 23.4 | 0.66 | 0.77 | 0.98 | 51.3 |
| 18 | R2 | 103 | 0.0 | 112 | 0.0 | 0.489 | 10.9 | LOS B | 2.9 | 23.4 | 0.66 | 0.77 | 0.96 | 50.8 |
| App | oach | 676 | 7.6 | 735 | 7.6 | 0.489 | 11.7 | LOS B | 2.9 | 23.4 | 0.66 | 0.77 | 0.98 | 51.1 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 51 | 0.0 | 55 | 0.0 | 0.215 | 8.4 | LOS A | 0.8 | 6.1 | 0.63 | 0.63 | 0.63 | 53.0 |
| 6 | T1 | 165 | 0.0 | 179 | 0.0 | 0.215 | 8.0 | LOS A | 0.8 | 6.1 | 0.62 | 0.62 | 0.62 | 54.1 |
| 16 | R2 | 45 | 0.0 | 49 | 0.0 | 0.215 | 7.6 | LOS A | 0.8 | 6.1 | 0.61 | 0.61 | 0.61 | 53.4 |
| App | oach | 261 | 0.0 | 284 | 0.0 | 0.215 | 8.0 | LOS A | 0.8 | 6.1 | 0.62 | 0.62 | 0.62 | 53.7 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 46 | 0.0 | 50 | 0.0 | 0.282 | 6.5 | LOS A | 1.2 | 9.6 | 0.47 | 0.39 | 0.47 | 55.4 |
| 4 | T1 | 393 | 3.0 | 427 | 3.0 | 0.282 | 6.4 | LOS A | 1.2 | 9.6 | 0.46 | 0.38 | 0.46 | 55.6 |
| 14 | R2 | 80 | 4.0 | 87 | 4.0 | 0.282 | 6.3 | LOS A | 1.2 | 9.4 | 0.45 | 0.37 | 0.45 | 54.3 |
| App | oach | 519 | 2.9 | 564 | 2.9 | 0.282 | 6.4 | LOS A | 1.2 | 9.6 | 0.46 | 0.38 | 0.46 | 55.4 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 146 | 0.0 | 159 | 0.0 | 0.438 | 10.0 | LOS A | 2.5 | 19.2 | 0.65 | 0.71 | 0.82 | 51.8 |
| 2 | T1 | 368 | 0.0 | 400 | 0.0 | 0.438 | 9.7 | LOS A | 2.5 | 19.2 | 0.64 | 0.70 | 0.80 | 52.6 |
| 12 | R2 | 172 | 2.0 | 187 | 2.0 | 0.438 | 9.4 | LOS A | 2.5 | 19.0 | 0.63 | 0.68 | 0.79 | 52.0 |
| Approach |  | 686 | 0.5 | 746 | 0.5 | 0.438 | 9.7 | LOS A | 2.5 | 19.2 | 0.64 | 0.70 | 0.80 | 52.3 |
| All Vehicles |  | 2142 | 3.3 | 2328 | 3.3 | 0.489 | 9.3 | LOS A | 2.9 | 23.4 | 0.60 | 0.63 | 0.75 | 52.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\forall$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: TT 2033 PM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2033) Total Traffic
PM Peak Hour
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\forall$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: TT 2038 AM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2038) Total Traffic
AM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 90 | 9.0 | 98 | 9.0 | 0.509 | 13.0 | LOS B | 3.1 | 24.9 | 0.69 | 0.81 | 1.06 | 49.9 |
| 8 | T1 | 498 | 9.0 | 541 | 9.0 | 0.509 | 12.4 | LOS B | 3.2 | 25.3 | 0.68 | 0.80 | 1.04 | 50.8 |
| 18 | R2 | 104 | 0.0 | 113 | 0.0 | 0.509 | 11.5 | LOS B | 3.2 | 25.3 | 0.67 | 0.80 | 1.02 | 50.4 |
| App | ach | 692 | 7.6 | 752 | 7.6 | 0.509 | 12.4 | LOS B | 3.2 | 25.3 | 0.68 | 0.80 | 1.04 | 50.7 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 52 | 0.0 | 57 | 0.0 | 0.232 | 8.8 | LOS A | 0.9 | 6.6 | 0.64 | 0.64 | 0.64 | 52.8 |
| 6 | T1 | 174 | 0.0 | 189 | 0.0 | 0.232 | 8.4 | LOS A | 0.9 | 6.6 | 0.63 | 0.63 | 0.63 | 53.8 |
| 16 | R2 | 50 | 0.0 | 54 | 0.0 | 0.232 | 8.0 | LOS A | 0.9 | 6.6 | 0.62 | 0.62 | 0.62 | 53.1 |
| App | ach | 276 | 0.0 | 300 | 0.0 | 0.232 | 8.4 | LOS A | 0.9 | 6.6 | 0.63 | 0.63 | 0.63 | 53.5 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 48 | 0.0 | 52 | 0.0 | 0.298 | 6.8 | LOS A | 1.3 | 10.2 | 0.49 | 0.42 | 0.49 | 55.2 |
| 4 | T1 | 409 | 3.0 | 445 | 3.0 | 0.298 | 6.7 | LOS A | 1.3 | 10.2 | 0.48 | 0.40 | 0.48 | 55.4 |
| 14 | R2 | 83 | 4.0 | 90 | 4.0 | 0.298 | 6.5 | LOS A | 1.3 | 10.0 | 0.47 | 0.39 | 0.47 | 54.1 |
| App | ach | 540 | 2.9 | 587 | 2.9 | 0.298 | 6.7 | LOS A | 1.3 | 10.2 | 0.48 | 0.40 | 0.48 | 55.2 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 151 | 0.0 | 164 | 0.0 | 0.463 | 10.6 | LOS B | 2.8 | 21.5 | 0.67 | 0.75 | 0.90 | 51.3 |
| 2 | T1 | 379 | 0.0 | 412 | 0.0 | 0.463 | 10.3 | LOS B | 2.8 | 21.5 | 0.66 | 0.74 | 0.88 | 52.1 |
| 12 | R2 | 182 | 2.0 | 198 | 2.0 | 0.463 | 10.0 | LOS B | 2.8 | 21.4 | 0.65 | 0.72 | 0.87 | 51.6 |
| Approach |  | 712 | 0.5 | 774 | 0.5 | 0.463 | 10.3 | LOS B | 2.8 | 21.5 | 0.66 | 0.74 | 0.88 | 51.8 |
| All Vehicles |  | 2220 | 3.3 | 2413 | 3.3 | 0.509 | 9.8 | LOS A | 3.2 | 25.3 | 0.62 | 0.66 | 0.80 | 52.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\forall$ Site: 8 [Bostwick \& Pack/Bradley (Site Folder: TT 2038 PM)]
Bostwick Road \& Pack Road/Bradley Avenue
Future (2038) Total Traffic
PM Peak Hour
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 262 | 2.0 | 285 | 2.0 | 0.735 | 20.2 | LOS C | 8.4 | 64.9 | 0.85 | 1.17 | 1.77 | 45.2 |
| 8 | T1 | 741 | 1.0 | 805 | 1.0 | 0.735 | 19.3 | LOS C | 8.8 | 67.3 | 0.85 | 1.16 | 1.75 | 46.6 |
| 18 | R2 | 85 | 0.0 | 92 | 0.0 | 0.735 | 18.7 | LOS C | 8.8 | 67.3 | 0.84 | 1.16 | 1.74 | 46.2 |
| App | oach | 1088 | 1.2 | 1183 | 1.2 | 0.735 | 19.5 | LOS C | 8.8 | 67.3 | 0.85 | 1.16 | 1.75 | 46.2 |
| East: Bradley Avenue |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 102 | 0.0 | 111 | 0.0 | 0.649 | 26.2 | LOS D | 3.7 | 28.5 | 0.86 | 1.06 | 1.61 | 42.5 |
| 6 | T1 | 368 | 0.0 | 400 | 0.0 | 0.649 | 24.5 | LOS C | 3.9 | 29.4 | 0.85 | 1.05 | 1.60 | 43.7 |
| 16 | R2 | 71 | 0.0 | 77 | 0.0 | 0.649 | 23.4 | LOS C | 3.9 | 29.4 | 0.85 | 1.05 | 1.59 | 43.6 |
| App | oach | 541 | 0.0 | 588 | 0.0 | 0.649 | 24.7 | LOS C | 3.9 | 29.4 | 0.85 | 1.06 | 1.60 | 43.5 |
| North: Bostwick Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 75 | 0.0 | 82 | 0.0 | 0.559 | 15.5 | LOS C | 3.5 | 27.5 | 0.75 | 0.91 | 1.26 | 48.6 |
| 4 | T1 | 431 | 6.0 | 468 | 6.0 | 0.559 | 15.2 | LOS C | 3.6 | 28.1 | 0.74 | 0.90 | 1.24 | 49.0 |
| 14 | R2 | 168 | 1.0 | 183 | 1.0 | 0.559 | 14.2 | LOS B | 3.6 | 28.1 | 0.74 | 0.89 | 1.23 | 48.7 |
| App | oach | 674 | 4.1 | 733 | 4.1 | 0.559 | 15.0 | LOS C | 3.6 | 28.1 | 0.74 | 0.90 | 1.24 | 48.9 |
| West: Pack Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 148 | 0.0 | 161 | 0.0 | 0.451 | 11.4 | LOS B | 2.6 | 19.4 | 0.69 | 0.78 | 0.95 | 50.6 |
| 2 | T1 | 330 | 0.0 | 359 | 0.0 | 0.451 | 10.9 | LOS B | 2.6 | 19.4 | 0.68 | 0.76 | 0.94 | 51.7 |
| 12 | R2 | 142 | 4.0 | 154 | 4.0 | 0.451 | 10.8 | LOS B | 2.5 | 19.4 | 0.67 | 0.75 | 0.92 | 51.1 |
| Approach |  | 620 | 0.9 | 674 | 0.9 | 0.451 | 11.0 | LOS B | 2.6 | 19.4 | 0.68 | 0.76 | 0.94 | 51.3 |
| All Vehicles |  | 2923 | 1.6 | 3177 | 1.6 | 0.735 | 17.6 | LOS C | 8.8 | 67.3 | 0.79 | 1.00 | 1.43 | 47.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## Appendix F - Traffic Signal Warrants

## OTM BOOK $12^{*}$ - TRAFFIC SIGNAL WARRANT



Justification 7 - Projected Volumes

| WARRANT | DESCRIPTION | MINIMUM REQUIREMENT |  |  |  | COMPLIANCE |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FREE FLOW | RESTRICTED FLOW | ADJUSTED <br> FREE FLOW | $\begin{aligned} & \hline \text { ADJUSTED } \\ & \text { RESTRICTED } \\ & \text { FLOW } \end{aligned}$ | SECTIONAL |  | ENTIRE \% |
|  |  |  |  |  |  | AHV | \% |  |
| 1. MINIMUM VEHICULAR VOLUME | A. Vehicle volumes, all approaches (Average Hour) | 480 | 720 | 720 | 1080 | 1164 | 100\% |  |
|  | B. Vehicle volume along minor roads (Average Hour) | $120$ | 170 | 180 | 255 | 59 | 33\% | 33\% |
| 2. DELAY TO CROSS TRAFFIC | A. Vehicle volumes, along artery (Average Hour) | 480 | 720 | 720 | 1080 | 1105 | 100\% |  |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor roads (Average Hour) | 50 | 75 | 75 | 113 | 21 | 28\% | 28\% |

## Projected Traffic Volumes:

| AM Peak Hour Volumes |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  | $\kappa$ | 62 |  |
| 20 | 883 | 19 | $\leftarrow$ | 0 |  |
| $K$ | $\downarrow$ | $\searrow$ | $\swarrow$ | 0 |  |
|  | 52 | $\nearrow$ | $\nwarrow$ | $\uparrow$ | $\pi$ |
|  | 0 | $\rightarrow$ | 12 | 1015 | 5 |
| 33 | $\searrow$ |  |  |  |  |

Average Hourly Volume (AHV) Equation: $\qquad$


| Average Hourly Volumes (AHV) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 18$K$ | $\begin{gathered} 480 \\ \downarrow \\ \hline \hline \end{gathered}$ | $\begin{aligned} & 18 \\ & \searrow \end{aligned}$ | $\kappa$$\leftarrow$$K$ | 24 |  |
|  |  |  |  | 0 |  |
|  |  |  |  | 0 |  |
|  | 21 | 7 | К | 个 | 7 |
|  | 0 | $\rightarrow$ | 11 | 573 | 5 |
|  |  | $v$ |  |  |  |

## Notes:

1. Vehicle volume warrant (1A) and (2A) for intersections of roadways having two or more moving lanes in one direction should be $25 \%$ higher than the values given above.
2. Warrant values for free flow apply when the 85th percentile speed of artery traffic equals or exceeds $70 \mathrm{~km} / \mathrm{h}$ or when the intersection lies within the built-up area of an isolated community having a population of less than 10,000. Warrant values for restricted flow apply to large urban communities when the 85th percentile speed of artery traffic does not exceed $70 \mathrm{~km} / \mathrm{h}$.
1 Lane per Direction
3. The lowest sectional percentage governs the entire warrant.
4. For " T " intersections the warrant values for the minor road should be increased by $50 \%$ (Warrant 1B only). $\qquad$
5. All flow values for Justification 1 and 2 are to be increased by $20 \%$ in the case of new intersections, Justification 3 is to only be used for existing intersections and all flow values for Warrant 1 and Warrant 2 of Justification 7 are to be increased by $20 \%$ for existing intersections and by $50 \%$ in the
(b) The heaviest through volume from the minor road.
(c) $50 \%$ of the heavier left turn movement from major road when both of the following are met:
(i) the left-turn volume $>120 \mathrm{vph}$
(ii) the left-turn volume plus the opposing volume $>720 \mathrm{vph}$
(d) Pedestrians crossing the main road.

## CONCLUSION:

OTM BOOK $12^{*}$ - TRAFFIC SIGNAL WARRANT


Justification 7 - Projected Volumes

| WARRANT | DESCRIPTION | MINIMUM REQUIREMENT |  |  |  | COMPLIANCE |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FREE FLOW | RESTRICTED FLOW | ADJUSTED <br> FREE FLOW | $\begin{aligned} & \hline \text { ADJUSTED } \\ & \text { RESTRICTED } \\ & \text { FLOW } \end{aligned}$ | SECTIONAL |  | ENTIRE \% |
|  |  |  |  |  |  | AHV | \% |  |
| 1. MINIMUM VEHICULAR VOLUME | A. Vehicle volumes, all approaches (Average Hour) | 480 | 720 | 720 | 1080 | 1157 | 100\% |  |
|  | B. Vehicle volume along minor roads (Average Hour) | $120$ | 170 | 180 | 255 | 164 | 91\% | 91\% |
| 2. DELAY TO CROSS TRAFFIC | A. Vehicle volumes, along artery (Average Hour) | 480 | 720 | 720 | 1080 | 993 | 100\% |  |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor roads (Average Hour) | 50 | 75 | 75 | 113 | 41 | 55\% | 55\% |

## Projected Traffic Volumes:



Average Hourly Volume (AHV) Equation: $\qquad$


| Average Hourly Volumes (AHV) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\kappa$ | 120 |  |
|  | 408 | 84 | $\leftarrow$ | 1 |  |
| k | $\downarrow$ | $\pm$ | $k$ | 28 |  |
|  | 10 | $\pi$ | К | $\uparrow$ | 7 |
|  |  | $\rightarrow$ | 3 | 458 | 32 |
|  |  | $\pm$ |  |  |  |

## Notes:

1. Vehicle volume warrant (1A) and (2A) for intersections of roadways having two or more moving lanes in one direction should be $25 \%$ higher than the values given above.
2. Warrant values for free flow apply when the 85th percentile speed of artery traffic equals or exceeds $70 \mathrm{~km} / \mathrm{h}$ or when the intersection lies within the built-up area of an isolated community having a population of less than 10,000. Warrant values for restricted flow apply to large urban communities when the 85th percentile speed of artery traffic does not exceed $70 \mathrm{~km} / \mathrm{h}$.
3. The lowest sectional percentage governs the entire warrant.
4. For " T " intersections the warrant values for the minor road should be increased by $50 \%$ (Warrant 1B only). $\qquad$
5. All flow values for Justification 1 and 2 are to be increased by $20 \%$ in the case of new intersections, Justification 3 is to only be used for existing intersections and all flow values for Warrant 1 and Warrant 2 of Justification 7 are to be increased by $20 \%$ for existing intersections and by $50 \%$ in the
6. The crossing volumes are defined as the sum of:
(a) Left-turns from both minor road approaches.
(b) The heaviest through volume from the minor road.
(c) $50 \%$ of the heavier left turn movement from major road when both of the following are met:
(i) the left-turn volume $>120 \mathrm{vph}$
(ii) the left-turn volume plus the opposing volume $>720 \mathrm{vph}$
(d) Pedestrians crossing the main road.

## CONCLUSION:

## Appendix G - Auxiliary Left-Turn Lane Warrant Analysis

## Colonel Talbot Road \& Clayton Walk | Northbound Left-Turn | AM Peak Hour

Left-turn volume represents less than $5 \%$ of approaching volumes. As such, left-turn warrant analysis can not be completed.

## Colonel Talbot Road \& Clayton Walk \| Southbound Left-Turn \| AM Peak Hour

Left-turn volume represents less than $5 \%$ of approaching volumes. As such, left-turn warrant analysis can not be completed.

## Colonel Talbot Road \& Clayton Walk | Northbound Left-Turn | PM Peak Hour

Left-turn volume represents less than $5 \%$ of approaching volumes. As such, left-turn warrant analysis can not be completed.


```
TRAFFIC SIGNALS MAY BE WARRANTED IN RURAL
AREAS OR URBAN AREAS WITH RESTRICTED FLOW
    TRAFFIC SIGNALS MAY BE WARRANTED IN
    "FREE FLOW" UREAN AREAS
```

Colonel Talbot Road \& Clayton Walk | Southbound Left-Turn | PM Peak Hour


[^0]:    ${ }^{1}$ City of London staff agreed to the use of a $1.5 \%$ linear traffic growth rate via email on August 3, 2023.

