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**Major Drainage and Stormwater
Management Report**

**Colonel Talbot Road
Development Area**

January 2024

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1.0 Introduction

Stantec was retained by W3 Farms and Sifton Properties to prepare this major drainage, flow routing assessment and stormwater management report in support of their proposed subdivisions located on Colonel Talbot Road in the City of London. This report identifies a preliminary drainage strategy for the proposed developments that is consistent with the goals and recommendations of the 2020 Dingman Creek Subwatershed: Stormwater Servicing Strategy, Schedule C Municipal Class Environmental Assessment (Dingman SWM EA), provides guidance for preparation of the corresponding Draft Plans, and provides recommendations for the functional stormwater management (SWM) design.

This report presents a preliminary channel corridor design for the proposed subdivisions and informs the dimensions of that channel. The proposed channel corridor is designed to:

- Safely convey the uncontrolled post-development stormwater from the proposed developments and external tributary area;
- Provide surface water to maintain proposed naturalized features; and
- Act as an amenity within the proposed subdivisions, providing both active and passive recreation opportunities to future residents.

1.1 Background Information

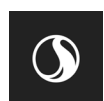
The following background information was reviewed to assist in the preparation of this assessment:

Talbot Village Subdivision Phase 2 Stormwater Management Functional Design Report, prepared by IBI Group, January 2010.

The existing Talbot Village Subdivision is located north of the subject properties. The report provides information regarding the upstream drainage area that contributes runoff to the subject sites.

Silverleaf Subdivision Drainage Servicing Report, prepared by Stantec, December 2016.

The Silverleaf Subdivision is located west of the subject sites. The drainage servicing strategy presented in this report accommodates minor flows from a portion of the proposed Sifton development.



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Colonel Talbot Road Subdivision Drainage Servicing Report, prepared by Stantec, December 2016.

Auburn Development's Colonel Talbot Road Subdivision is located south of the subject sites. The drainage servicing strategy presented in this report accommodates stormwater from a portion of the proposed W3 Farms Subdivision.

Dingman Creek Modeling Report, prepared by Aquafor Beech, November 2017.

This report provides a brief summary of the hydrologic modelling completed in support of the ongoing Dingman Creek SWM EA.

Dingman Creek Subwatershed; Stormwater Servicing Study, prepared by Aquafor Beech, September 2020.

This report provides a comprehensive high-level stormwater servicing strategy for the subject tributary among others.



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2.0 Pre-Development Conditions

The W3 Farms and Sifton properties are located in the Tributary B drainage area of the Dingman Creek watershed in the southwest portion of the City of London. Most of the runoff from these lands is conveyed to Dingman Creek by Tributary 12.

Tributary 12 carries agricultural runoff to Dingman Creek. Recent aerial photography shows that significant reaches of the tributary upstream of Colonel Talbot Road have been enclosed. The remaining open channel portions have been straightened. Stream flows are ephemeral with no significant baseflow due to the relatively small contributing drainage area.

A pre-development conditions hydrologic analysis was created to establish design target discharges from the proposed W3 Farms and Sifton Developments. A hydrologic model was developed using SWMHYMO to calculate the peak discharges in Dingman Creek Tributary 12. A brief summary of the model inputs, assumptions, and results is presented below.

2.1 Drainage Catchments

The pre-development condition drainage boundaries were delineated based on the available City of London topographic mapping, the drainage delineation previously developed for the neighboring Auburn Developments Colonel Talbot Road Subdivision, and the drainage catchments delineated for the Dingman Creek Stormwater Management Environmental Assessment. The catchments were delineated based on the drainage conditions prior to development of the most recent Phase of the North Talbot Subdivision. The pre-development drainage catchments are shown on Drawing 1 and are described briefly below:

Catchment S101 – Runoff from this agricultural catchment travels southward as shallow surface flow to a CSP culvert at Pack Road. This catchment is currently being developed, and while flows will be redirected to the North Talbot Subdivision ponds, it is represented here in its pre-development condition in order to accurately estimate the target discharges in Dingman Creek Tributary 12.

Catchment S102 – This external drainage area is comprised of actively cropped agricultural lands that contribute runoff to the downstream Sifton property. All runoff travels to the tributary as shallow surface flow.

Catchment S103 – This catchment includes the portion of the Sifton property that contributes runoff to Dingman Creek Tributary 12. This catchment is mostly comprised of actively cropped agricultural land, though there is a small woodland patch located in the southeast corner. All runoff travels to the tributary as shallow surface flow.



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Catchment S104 – This catchment is comprised of actively cropped agricultural lands and includes the portion of the W3 Farms property that contributes runoff to Dingman Creek Tributary 12. All runoff travels to the tributary as shallow surface flow.

2.2 Soils

The available Middlesex County soils mapping suggest that the soils within the Dingman Creek Tributary 12 drainage area are generally comprised of Teeswater silt loam, Brant silt loam, and Muriel silt loam. Nearby hydrogeological studies suggest that the area is comprised of silty clay/clayey silts.

2.3 Design Storms

The City of London Design Standards and Requirements Manual (DSRM) outlines the AES parameters for a range of Intensity Duration Frequency (IDF) curves for 3-hour Chicago Design Storms. The size of the drainage catchment and proposed development suggests that this distribution is appropriate for use in this assessment. Consequently, these storm distributions were used in the hydrologic calculations completed for this assessment.

2.4 Hydrologic Parameters

Overland flow lengths were estimated for each catchment based on the 2017 LiDAR Digital Terrain Model. Each overland flow route was measured from the local high point to the Dingman Creek tributary alignment. The 85/10 Method was used to calculate representative slopes and account for the variable catchment topography.

SCS Curve Number values were calculated for the existing and proposed catchments as per the MTO Drainage Manual and USDA TR-55. A summary of the values assigned to each catchment is presented in Appendix A.

2.5 Hydrologic Model Results

The calculated pre-development peak discharges at key locations in the Tributary 12 channel reach are summarized in the following table. These key locations are shown on Drawing 1.



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Table 1: Calculated Pre-Development Peak Discharges

Location	Peak Discharge (m³/s) 2-year	Peak Discharge (m³/s) 5-year	Peak Discharge (m³/s) 10-year	Peak Discharge (m³/s) 25-year	Peak Discharge (m³/s) 50-year	Peak Discharge (m³/s) 100-year	Peak Discharge (m³/s) 250-year
Upstream Sifton Property Limit	1.19	2.13	2.88	3.85	4.60	5.39	6.65
Upstream Sifton North Property Limit	0.39	0.70	0.95	1.27	1.52	1.78	2.19
Upstream Sifton East Property Limit	0.78	1.41	1.90	2.54	3.04	3.56	4.39
Upstream York Property Limit	1.80	3.24	4.38	5.86	7.01	8.21	10.12
Colonel Talbot Road	1.80	3.24	4.38	5.86	7.01	8.21	10.12



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3.0 Post-Development Conditions

Map 1 of the London Plan identifies the subject area as “Neighbourhood” place type. Consequently, both the W3 Farms and Sifton properties will be developed as residential subdivisions, and will include single family residential lots, multi-family blocks, park blocks, and SWM blocks. The preliminary stormwater management strategy to control runoff from the future development and supporting hydrologic and hydraulic analyses are described below.

3.1 Stormwater Management Strategy

The Southwest Area Plan Stormwater Management Servicing Report (AECOM, 2010) presents a preliminary SWM strategy for the subject properties that includes two proposed regional SWM facilities (North Lambeth P7 and P8) that provide all necessary stormwater treatment. This concept was intended to accommodate anticipated development phasing, but presents several drawbacks and challenges, including:

- Multiple SWM facilities to operate and maintain;
- Difficulties in developing an efficient strategy to convey the treated flows from P7 to the downstream outlet without interfering with the downstream storm sewers that convey stormwater to P8;
- Difficulties servicing lands in the western portion of the catchment due to relatively low local ground elevations; and
- Conflicts with the Dingman Creek SWM EA preliminary preferred alternative.

The Dingman Creek Subwatershed Stormwater Servicing Strategy (Aquafor Beech, 2020) proposes a “Complete Corridor” for the proposed developments within the Phase 1 study limits that includes both at-source treatment combined with end-of-pipe SWM controls. Consistent with this solution, the preliminary stormwater servicing strategy within the W3 Farms and Sifton developments will include at-source controls to provide water quality treatment, end-of-pipe quantity controls and conveyance provided by a channel corridor.

3.1.1 Proposed Channel Corridor

The proposed channel corridor provides the following opportunities to improve the existing Tributary 12 channel system:

- The undisturbed natural corridor limits are increased from the existing typical widths that range from 0 to 10 m to approximately 30 m;



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- Approximately 470 m of tile drain will be removed, resulting in a net increase in aquatic habitat;
- The proposed channel corridor includes a conveyance capacity to accommodate the runoff from the uncontrolled, post-development 250-year storm event as required by the UTRCA; and
- The proposed channel corridor limits are clearly defined to mitigate the possibility of future encroachments.

3.1.2 Quality Control

Water quality treatment to remove 80% of total suspended sediment (TSS) is provided to the runoff from the proposed development prior to being discharged to the channel corridor. The following water quality treatment strategies could potentially provide the necessary TSS removal without the need to dedicate additional land for quality treatment in the proposed Draft Plans:

- **Third Pipe System** – Areas of clean runoff such as rear-yards and parkland shall be collected in a separate sewer system, possibly perforated, that would allow runoff not requiring quality treatment to be managed separately from runoff that does require quality treatment. Storm private drain connections (PDC) would also connect to this system. These third pipe systems could outlet to the proposed end-of-pipe facilities or directly to the channel corridor/wetland compensation areas.
- **LID Measures in Boulevards** – The proposed boulevards are graded to provide shallow surface depressions that capture the first flush of runoff and allow it to infiltrate, providing filtration. The proposed depressions are grassed, with shallow slopes to permit mowing. A shallow perforated pipe collects the clean stormwater and conveys it to the local storm sewer. During severe storm events, overflows from the boulevard ponding areas are captured by standard catchbasins located in the roadway. This option would likely prevent planting boulevard street trees were this strategy is implemented, because roots could potentially clog the proposed subdrains. Since both Sifton and W3 Farms are concerned with the reaction of homebuilders and buyers to streetscapes that have a non-standard appearance, this strategy would likely best be implemented in areas with no fronting homes, such as side lots and parks.
- **Storm Sewer Exfiltration System** – Often referred to as the Etobicoke Exfiltration System, a perforated pipe is installed below the proposed local storm sewers and discharges the runoff from small frequent storm events to the granular trench backfill. The stormwater then infiltrates into the surrounding native soils. Pretreatment is provided by catchbasin inserts to improve sediment retention in the catchbasin sumps. These systems are appropriate for locations where the soil permeability is sufficiently high and groundwater elevations are sufficiently low.



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Further geotechnical and hydrogeological investigation is necessary to verify that this solution is feasible.

- **Oil/Grit Separators** – Oil/grit separators (OGSs) are provided upstream of each outlet to provide TSS removal. Pretreatment is provided by catchbasin inserts to improve sediment retention in the catchbasin sumps. This option is costly, as at least eight large OGSs will be required to provide the necessary water quality treatment. Furthermore, obtaining an Environmental Compliance Approval for this strategy may prove challenging, as the MECP typically only accepts OGSs as one component of a water quality treatment train. Consequently, OGSs would likely need to be implemented in conjunction with other water quality treatment methods.

The proposed water quality treatment strategy will be selected and developed as detailed design progresses and may involve a combination of the measures described above, or other potential measures not yet identified.

3.1.3 Quantity Control

Quantity control storage is to be provided within the integrated channel as proposed offline SWM facilities, either wet or dry, to attenuate the post-development peak flows from the proposed W3 Farms and Sifton Subdivisions to the pre-development targets. These facilities would drain directly to the channel corridor at various locations along its length. The volumetric requirements of these facilities are discussed later in this report. Locating and sizing of these facilities would be the next step in the design process.

3.1.4 Culverts

In accordance with City of London design standards for neighborhood streets, the culvert at the single proposed road crossing has been designed to convey the peak calculated discharge from all storm events up to and including the 25-year design event without overtopping. The proposed roadway embankment acts as a weir to control the peak discharges during more severe storm events. The downstream roadway embankment will be adequately armored to mitigate the risk of erosion during design events that result in overtopping. A summary of the anticipated overtopping flows at the proposed road crossing is presented in the following table.

Table 2: Depth of Roadway Overtopping at Proposed Road Crossings

Design Event	Campbell Street Crossing*
Pre-Dev 250-year	0.00 m
UTRCA 50-year	0.03 m
UTRCA 250-year	0.19 m

*Depths taken from HECRAS cross-section 2636.5



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The calculation results suggest that the maximum flow depth over the proposed road is less than the maximum allowable City of London standard of 300 mm. Furthermore, the corresponding flow velocities and depths do not present a significant safety hazard during severe storm events.

3.2 Hydrologic Modelling

A post-development conditions hydrologic model was created to assist in the preliminary design of the proposed channel corridor and to evaluate the hydraulic performance.

3.2.1 Catchments

The post-development catchments were delineated based on the available Draft Plan information and the anticipated general site grading. The post-development drainage plan is shown on Drawing 2, and the corresponding catchments are described briefly below:

Catchments 100, 200, 300, 400, 401, 500 and 501– Water quality treatment is provided to the runoff from the proposed Sifton and W3 Farms residential subdivisions by at-source controls. Minor flows are conveyed to the proposed channel corridor by the proposed local storm sewers and third pipe systems. Major flows are conveyed to the proposed SWM facilities as shallow surface flow by the proposed rights-of-way then to the channel corridor.

Catchment 301 – Based on the City of London Official Plan, this external drainage area is anticipated to remain undeveloped. The proposed Sifton subdivision minor and major system provide sufficient capacity to accommodate the peak flows from this catchment and convey them to the proposed channel corridor.

Catchment 302 – At-source SWM controls provide water quality treatment to the runoff from future residential development in this external drainage area. The proposed Sifton subdivision minor and major system provide sufficient capacity to accommodate the peak flows from this catchment and convey them to the proposed channel corridor.

Catchment 402 – In accordance with the drainage servicing strategy previously developed for the Silverleaf Subdivision, minor flows from Phase 1 of the Sifton Subdivision and the neighboring properties on Colonel Talbot Road are conveyed westward to the Silverleaf Subdivision storm sewer. The design peak minor flow rate of 1.2 m³/s was estimated based on the hydrologic calculations presented in the Silverleaf Subdivision Drainage Servicing Report (Stantec, 2016). Major flows are conveyed southward to the proposed channel corridor.

While this strategy is consistent with previous documentation, we recommend that the minor flows from Catchment S1 be conveyed southward to the proposed channel



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corridor. This would eliminate the need for a new storm sewer crossing at Colonel Talbot Road and would provide capacity in the existing North Lambeth Subdivision storm sewer to accommodate proposed development on the west side of Colonel Talbot Road.

Catchment 502 – This catchment consists of a portion of the Phase 1 W3 lands that cannot drain overland to SWMF P9, so major flows from this catchment are being directed to the integrated channel.

Catchments 600, 601 and 602 – These catchments are comprised the integrated channel and retained woodlot. All runoff travels directly to the channel corridor as shallow surface flow.

Catchment EXT1 and EXT2 – All runoff from future development in this external drainage area is treated by upstream SWM controls that provide water quality treatment and attenuate the post-development peak discharges to pre-development magnitudes. The minor and major systems will convey these external flows directly to the proposed channel corridor.

Catchment EXT3 – This catchment consists of properties fronting Colonel Talbot Road that will be contributing to a storm sewer on Colonel Talbot Road that would outlet to the channel corridor. All flows from this area will be controlled on site to come by pipe up to and including the 250-year event.

3.2.2 Hydrologic Parameters

The post-development hydrologic model inputs were developed as follows:

- Percent impervious values were determined assuming a base level imperviousness for single-family residential with additional private controls being assumed to be established on denser blocks;
- Subcatchment flow lengths were measured along the proposed rights-of-way; and
- An average surface slope of 1% was assumed for new development in all post-development catchments.

A summary of the post development hydrologic parameters assigned to each catchment is presented in Appendix A.

3.2.3 Hydrologic Model Results

A comparison of calculated pre-development and the uncontrolled post-development peak discharges at the Colonel Talbot Road culvert is provided in the following table. This table reports model results are compared to the design flows that the UTRCA calculated for the tributary assuming full development and no SWM controls.



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Table 3 Calculated Peak Discharges at Colonel Talbot Road

Design Event	3hr Chicago Model Pre-Development Peak Flow (m³/s)	3hr Chicago Model Controlled Post-Development Peak Flow (m³/s)	UTRCA HECRAS Uncontrolled Post-Development Peak Flow (m³/s)
2-year	1.80	1.44	4.9
5-year	3.24	2.46	8.2
10-year	4.38	3.44	11.1
25-year	5.86	4.64	n/a
50-year	7.01	5.55	17.9
100-year	8.21	6.49	21.6
250-year	10.12	7.98	26.0

Model input and output files are available in Appendix A.

3.3 Hydraulic Modelling

A hydraulic surface water model was created to calculate the Tributary 12 post-development condition various water surface elevations within the proposed channel corridor and to verify that the uncontrolled 250-year storm event flows are contained within. The model was created using the US Army Corps of Engineers HEC-RAS program, and the corresponding model development and results are described below.

3.3.1 Model Development

A topographic survey of the Tributary 12 channel and floodplain was completed from the Dingman Creek confluence to Colonel Talbot Road to develop cross sections for the downstream channel reach. Proposed typical sections were used to represent the channel corridor from Colonel Talbot Road to the Natural heritage woodlot on the Sifton Subdivision property. The model cross section locations were selected to provide an accurate hydraulic representation of the channel and floodplain geometry. Cross sections are positioned at all existing and proposed culverts to accurately estimate the corresponding hydraulic losses. The cross-sections themselves have upper limits guaranteed to contain the flows and do not necessarily represent proposed grades as flood elevation was the primary concern of the model.

Manning's equation hydraulic roughness values were assigned to the existing channel reach downstream of Colonel Talbot Road based on the observed site conditions. The cross sections that represent the proposed channel corridor were assigned low flow



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channel roughness values of 0.04 and floodplain roughness values of 0.08, which should provide a reasonable representation of the friction losses in the proposed channel reach based on the likely naturalized channel conditions under proposed conditions.

Normal depth was assumed at the downstream boundary of the hydraulic model. Given the relatively steep longitudinal channel and floodplain slopes from the downstream model boundary to Colonel Talbot Road, any error associated with this boundary condition assumption will not affect the calculation results within the proposed channel corridor limits.

Nine flow regime profiles were run as part of this hydraulic model so the water surface elevation in each scenario is known. The 2-year to 250-year predevelopment flows were modelled to show the expected flood levels with appropriate SWM controls in place. The UTRCA's 50 and 250-year flows were evaluated to determine adequate capacity within the channel corridor.

The existing culvert at Colonel Talbot Road is a substantial hydraulic restriction on the channel system and has a considerable backwater effect. Any future improvements to this culvert should be incorporated during future design to mitigate this backwater effect. Current work is being undertaken by the City of London to improve downstream conditions in Tributary 12, including redesigning the culvert under Colonel Talbot Road. While the new culvert dimensions are known, the downstream cross-sections have changed with this design and will also need to be incorporated into the model.

3.3.2 Proposed Conditions Hydraulic Model Results

The proposed channel corridor is shown on Drawings 3 and 4, and the corresponding model output is presented in Appendix B. As shown on Drawings 3 and 4, the 250-year floodplain is contained within the proposed channel corridor limits. Furthermore, approximately 0.3 m of freeboard is provided from the peak 250-year calculated water surface elevation to the top of the proposed channel section.

3.3.3 Channel Width Discussion

The channel width within the integrated channel proposed by this report is 30 m. This channel width is sufficient to accommodate the conveyance requirements of the uncontrolled 250-year storm with a 0.3 m freeboard.

The Fluvial Geomorphology and Meander Belt Assessment, Dingman Creek Tributary B1 (Stantec, Nov 2019), contained in Appendix C, concluded that the meander belt associated with upper portions of this tributary was 19.9 m (reach 1 in the report) and the lower portions of this tributary were 28.0 m (reaches 2, 3 and 4 in the report). The report acknowledged that these meander belt widths assumed the maximum meander



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of the watercourse without restraint and that the detailed design of the works will likely include measures that will limit the meander to a lesser width.

3.4 SWM Facility Volumetric Requirements

A SWMHYMO model was developed to determine the volume requirements for SWM facilities to be located along the integrated channel. The model was run for the 3-hour Chicago Storm events to determine target release rates and facility volumes based on a staged control release targeting the 2-year and 100-year storms. The total target release rates were divided between SWMF catchments based on the contributing area as a percentage of the total post-development area.

3.4.1 Proposed Facilities

Seven (7) total facilities are proposed, and their catchment areas are described below.

External Pond – This pond is to service the lands external to the Sifton and York properties upstream of the integrated channel. They consist of drainage areas EXT1 and EXT2. It will likely be further divided to serve the needs of the future developer.

Pond 1 – This pond services drainage area 100 and would best perform as a dry facility given the small catchment area. This facility would be located on Sifton lands.

Pond 2 – This pond services drainage area 200, servicing W3 lands. This facility would best perform as a dry facility. This facility would be located on W3 lands.

Pond 3 – This pond services drainage areas 300, 301 and 302, servicing primarily Sifton and external lands, although likely located in W3. This facility would best perform as a dry facility.

Pond 4 – This pond services drainage areas 400, 401 and 402, servicing both Sifton and W3 lands, although located on W3 lands. This facility would best perform as a dry facility.

Pond 5 – This pond services drainage areas 500, 501 and 502, servicing W3 and external lands, located on W3 lands. This facility would best perform as a dry facility.

External 3 Controls – This facility is to service the lands external to the Sifton and York properties south of the integrated channel. It consists of drainage area EXT3. It will likely be further divided to serve the needs of the future developers. This area will drain by sewer with no overland flow outlet.

3.4.2 Modelling Results

Using the above catchments, the SWMF sizes were conservatively found to be as described in the following table. Model files can be found in Appendix A.



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Table 4: SWMF Release Rates and Sizes

	Contributing Area (ha)	2-Year Allowable Release Rate (m³/s)	100-Year Allowable Release Rate (m³/s)	Storage Volume with Freeboard (m³)
External Pond	32.7	0.53	2.42	14400
Pond 1	4.1	0.07	0.30	2400
Pond 2	7.5	0.12	0.56	3600
Pond 3	18.9	0.31	1.40	7000
Pond 4	18.9	0.31	1.40	8400
Pond 5	11.5	0.19	0.85	6000
EXT3	9.2	0.15	-	5000

The release rates shown above are the calculated total allowable release rate for that facility based on meeting existing rate targets. These rates were used in the model's stage-storage curves to then determine a volume to control the 100-year event. These volumes were then expanded on to account for containing the 250-year event and providing 0.3m of freeboard.

3.5 Wetland Compensation Areas

Both the proposed W3 Farms and Sifton subdivisions include wetland compensation areas to replace areas that are to be developed. Though their locations have not yet been finalized, the proposed features will be integrated into the proposed channel corridor to receive sufficient surface runoff to sustain their function.

3.6 Natural heritage Woodlot

The woodlot on the western edge of the Sifton property provides a challenge in conveying the 250-year uncontrolled flow. Further discussion with the City and UTRCA is required to determine the best way forward in incorporating the woodlot and the watercourse it contains into the integrated channel design.



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4.0 Fluvial Geomorphological Assessment

A fluvial geomorphological and meander belt assessment was completed for Tributary 12 to:

- Characterize the existing channel;
- Estimate the existing channel meander belt width; and
- Verify that the proposed channel corridor is sufficiently wide to accommodate a stable low flow swale design.

The corresponding assessment is presented in Appendix C and is briefly summarized, as follows:

1. A site visit was completed on November 1, 2019 to review and document the existing channel conditions. The results of the site visit suggest that significant portions of the tributary have been enclosed in drainage tile and the remaining open channel portions have been straightened.
2. Since Tributary 12 has been significantly altered by channel straightening and enclosures, empirical equations were used to estimate the maximum meander belt width. The results of the empirical analysis suggest that the maximum meander belt width of the existing channel is approximately 28 m. Note that this is a theoretical value for an unconfined natural channel allowed to fully mature under the existing flow conditions flow regime. As such, it is simply an indication of the long-term channel migration that could occur in the absence of intervention and land use changes and is not a rigid target that must be adhered to in future design. A stable confined channel with a narrower meander belt width can be designed to convey safely convey the post-development flows.
3. Based on the meander belt assessment results, the proposed channel corridor width of 30 m is sufficient to accommodate a stable low flow swale design. The proposed design will incorporate erosion mitigation measures that will limit lateral movement of the proposed low flow swale.

The channel corridor includes design measures to limit the post-development meander belt width to confine the proposed channel movement and mitigate the possibility of side slope erosion. As seen in the HECRAS cross-sections, the channel corridor cross section incorporates the following design elements to mitigate the risk of channel erosion and to support the natural function of the Tributary 12:

- A low flow swale conveys discharges from small, frequent, flood events; and,



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- The proposed low flow bench width has been maximized to accommodate a meandering low flow swale planform.



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5.0 Conclusions and Recommendations

A stormwater management strategy was developed to service the proposed W3 Farms and Sifton Subdivisions that is consistent with the preferred alternative identified in the Dingman SWM EA. The proposed SWM strategy meets the stormwater treatment requirements as follows:

- Water quality treatment is provided by at-source SWM controls that will be selected as detailed design proceeds; and
- Peak flow attenuation is provided by offline SWM facilities within the integrated channel corridor. These facilities will be located along the channel corridor both to the north and south.

External flows from future upstream development will be treated by at-source controls to provide water quality treatment and to attenuate the post-development peak discharges to pre-development magnitudes before outletting to the proposed channel corridor.

The results of the preliminary hydrologic and hydraulic analyses completed by Stantec show:

- The proposed 30 m wide channel corridor provides sufficient hydraulic capacity to convey all design events up to and including the uncontrolled 250-year storm; and,
- The proposed channel corridor is sufficiently wide to accommodate a stable low flow swale that will be designed in accordance with natural channel design principles to mitigate the risk of channel and bank erosion.

The following recommendations should be incorporated into the channel corridor, SWM facility and subdivision designs:

- Erosion protection must be incorporated into the downstream side of the proposed road crossing embankments to mitigate the risk of failure during overtopping events;
- The proposed wetland compensation areas should be incorporated into the proposed channel corridor to verify that the proposed wetland receives sufficient flow; and
- The minimum property line elevation at all lots abutting the proposed integrated channel should not be less than the Colonel Talbot Road overtopping elevation, which is approximately 263.3 m to mitigate the risk of flooding caused by either a system failure or a flood event that exceeds the channel corridors design capacity.

The next steps for this design process are to complete the design process to bring all of the components of the integrated channel together. This includes sizing and locating the



Major Drainage and Stormwater Management Report Colonel Talbot Road Development Area

January 2024

SWM facilities, designing the channel, locating the trail system and integrating the wetland compensation areas that will be within the integrated channel system.


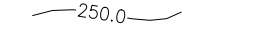
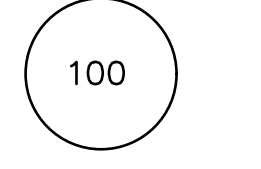
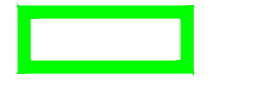



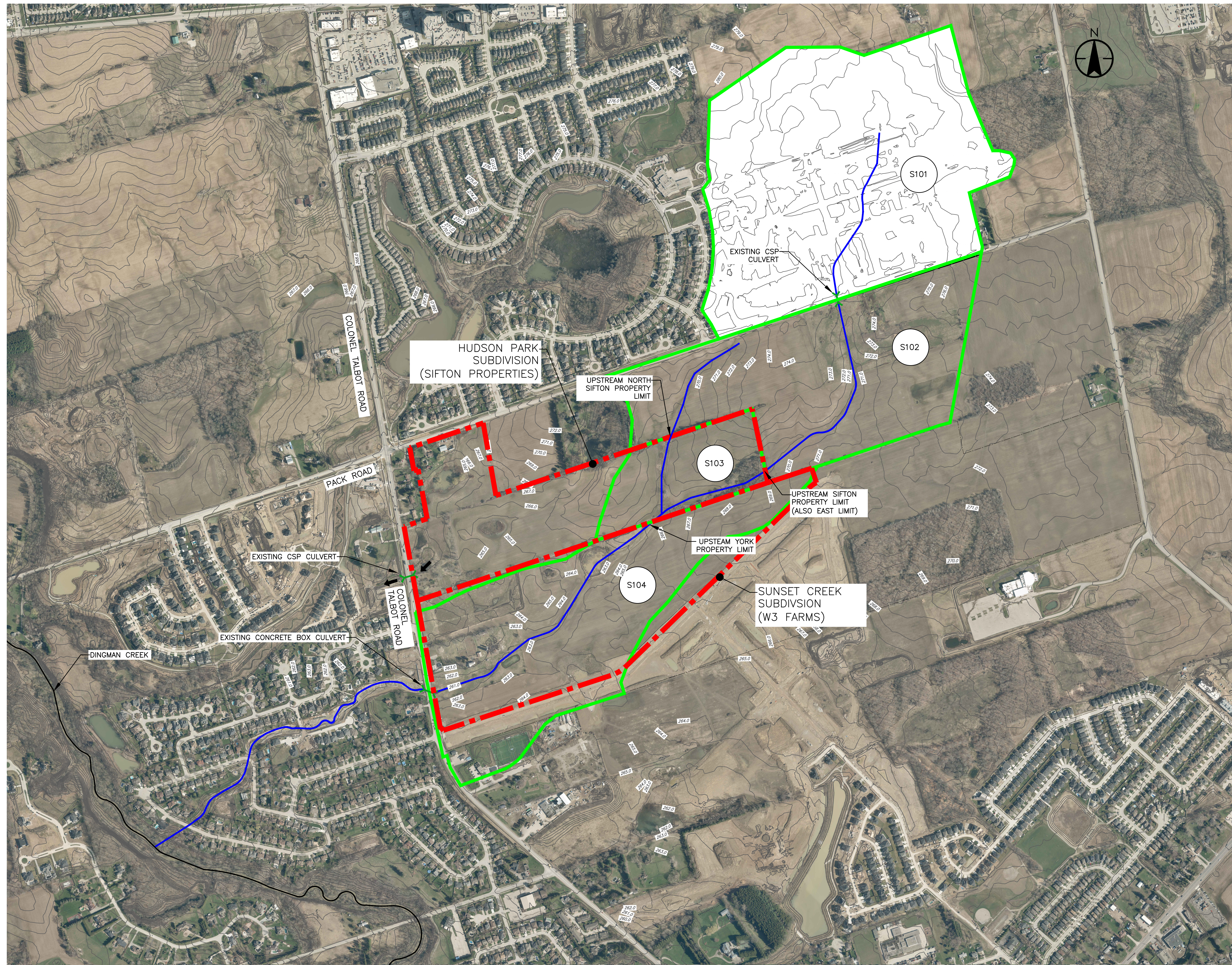
Drawings



Liability Note:
The Contractor shall verify and be responsible for all dimensions. DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.

Notes

-  SUBJECT SITE BOUNDARIES
-  ELEVATION CONTOURS
-  CATCHMENT ID
-  CATCHMENT BOUNDARY
-  EXISTING TRIBUTARY B1 CHANNEL ALIGNMENT



File Name: 16141470_int_channel_pre_dev
Dwn. Chkd. Dsgn. YY.MM.DD

Permit-Seal

Client/Project
SIFTON PROPERTIES LIMITED/W3 FARMS INC.

COLONEL TALBOT / W3 SUBDIVISION

London, ON Canada

Title
PRE-DEVELOPMENT
DRAINAGE AREAS

Project No. 161413835
Scale: HORZ - 1 : 5000
50 0 100m

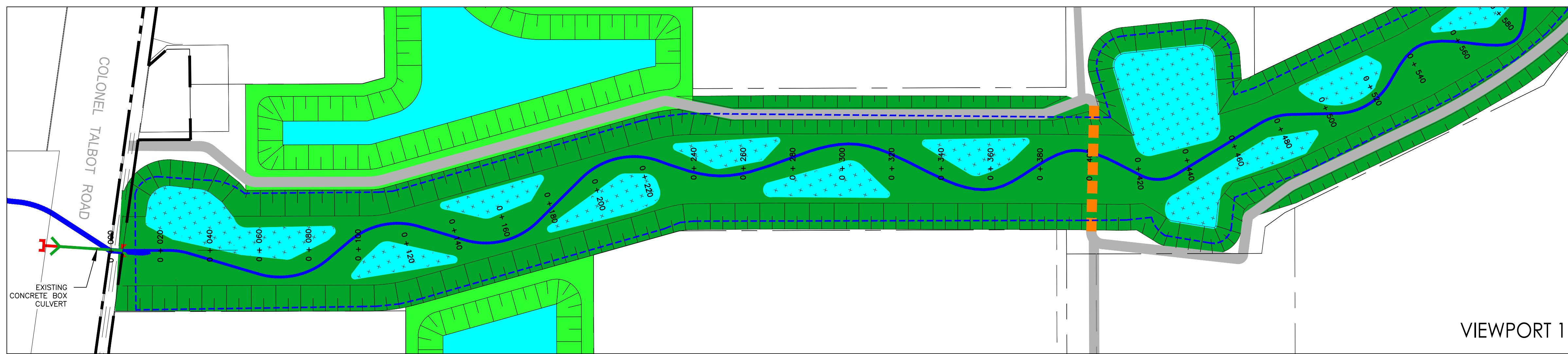
Drawing No. Sheet Revision

1 1 of 5 0

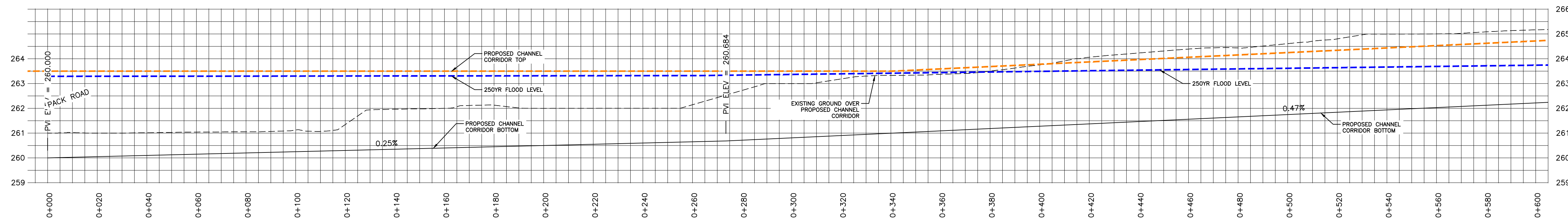
Liability Note:
The Contractor shall verify and be responsible for all dimensions.
DO NOT scale the drawing - any errors or omissions shall be reported to Stantec without delay.

Notes

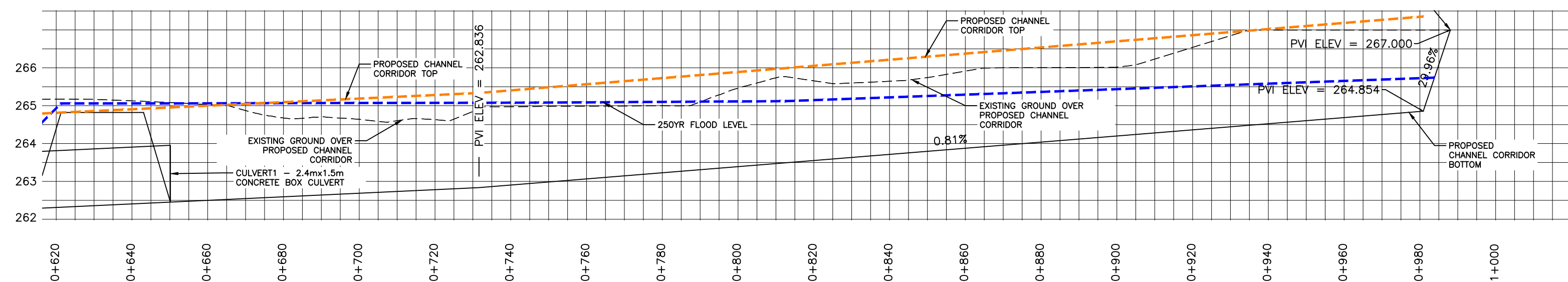
- CHANNEL CORRIDOR
- NATURAL ENVIRONMENT AREA
- PROPOSED LOW FLOW SWALE ALIGNMENT
- 250 YEAR FLOOD ELEVATION



VIEWPORT 1



VIEWPORT 2



V:\016\Projective\1614170\design\drawing\viewport\figure\1614170_int_channel_profile.dwg
2023-11-17 12:40:07 AM by: Chibb, Jason

ORIGINAL SHEET - AN3 D

File Name: 1614170_int_channel_profile
Dwn. Chkd. Dsgn. YY.MM.DD

Permit-Seal

Client/Project
SIFTON PROPERTIES LIMITED/W3 FARMS INC.

COLONEL TALBOT / W3 SUBDIVISION

London, ON Canada

Title
INTERGRATED CHANNEL PLAN & PROFILE

Project No.
1614170

Scale
HORZ - 1 : 1000
10 0 20m

Drawing No. Sheet Revision

4 4 of 5 0

APPENDIX A: Hydrologic Analysis Results



**161414170 - Sifton/W3 Integrated Channel
SCS Curve Number Determination**

Site Soils: Silty Clay

TABLE OF CURVE NUMBERS (CN's)									
Land Use	Hydrologic Soil Type								Manning's 'n'
	A	AB	B	BC	C	CD	D		
Meadow	50	54	58	64.5	71	74.5	78		0.40
Woodlot	50	55.3	60.5	67	73.5	76.8	80		0.40
Long Grass	55	60	65	72	79	81.5	84		0.30
Lawns	60	65.5	71	77	83	86	89		0.25
Pasture/Range	58	61.5	65	70.5	76	78.5	81		0.17
Crop	66	70	74	78	82	84	86		0.13
Fallow (Bare)	77	82	86	89	91	93	94		0.05
Wetland	50	50	50	50	50	50	50		0.15

HYDROLOGIC SOIL TYPE (%) - Existing Conditions								
Catchment	Hydrologic Soil Type							TOTAL
	A	AB	B	BC	C	CD	D	
Existing								
S101						100		100
Proposed								
100						100.0		100
301						100.0		100
600						100.0		100

LAND USE (%)									
Catchment	Meadow	Woodlot	Long Grass	Lawns	Pasture Range	Crop	Fallow (Bare)	Wetland	Total
	Existing								
S101						100			100
Proposed									
100				100					100
301		100							100
600	75							25	100

CURVE NUMBER (CN) - Existing Conditions									
Catchment	Meadow	Woodlot	Long Grass	Lawns	Pasture Range	Crop	Fallow (Bare)	Wetland	Weighted CN
	Existing								
S101	0.0	0.0	0.0	0.0	0.0	84.0	0.0	0.0	84.0
Proposed									
100	0.0	0.0	0.0	86.0	0.0	0.0	0.0	0.0	86.0
301	0.0	76.8	0.0	0.0	0.0	0.0	0.0	0.0	76.0
600	55.9	0.0	0.0	0.0	0.0	0.0	0.0	12.5	68.0

** post development catchments concerned with pervious CN values only

** AMC II assumed

** Hydrological Soil Group taken from MTO Drainage Manual for each soil type

**161414170 - Sifton/W3 Integrated Channel
SWMHYMO Parameters**

Site Soils: Silty Clay

Area Description	Catchment Number	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
	S101	DESIGN NASHYD	49.50	84	NA	NA	0.60	590	1.41	0.84
	S102	DESIGN NASHYD	32.80	84	NA	NA	1.15	485	1.03	0.62
	S103	DESIGN NASHYD	8.90	84	NA	NA	1.83	400	0.80	0.48
	S104	DESIGN NASHYD	33.50	84	NA	NA	0.92	575	1.21	0.72
Total			124.70							

Proposed Conditions

Area Description	Catchment Number	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
	100	DESIGN STANDHYD	4.08	86	0.55	0.45	1.00	300		
	200	DESIGN STANDHYD	7.53	86	0.55	0.45	1.00	550		
	300	DESIGN STANDHYD	10.33	86	0.55	0.45	1.00	610		
	301	DESIGN NASHYD	4.37	76	NA	NA	1.10	210	0.69	0.41
	302	DESIGN STANDHYD	4.18	86	0.55	0.45	1.00	210		
	400	DESIGN STANDHYD	5.25	86	0.55	0.45	1.00	250		
	401	DESIGN STANDHYD	3.22	86	0.55	0.45	1.00	250		
	402	DESIGN STANDHYD	10.47	86	0.55	0.45	1.00	350		
	500	DESIGN STANDHYD	3.14	86	0.55	0.45	1.00	250		
	501	DESIGN STANDHYD	2.93	86	0.55	0.45	1.00	250		
	502	DESIGN STANDHYD	5.45	86	0.55	0.45	1.00	600		
	EXT1	DESIGN STANDHYD	23.21	86	0.55	0.45	1.00	750		
	EXT2	DESIGN STANDHYD	9.50	86	0.55	0.45	1.00	400		
	EXT3	DESIGN STANDHYD	9.16	86	0.55	0.45	1.00	400		
	600	DESIGN NASHYD	0.99	68	NA	NA	0.95	140	0.59	0.35
	601	DESIGN NASHYD	3.54	68	NA	NA	0.81	350	0.98	0.59
	602	DESIGN NASHYD	3.61	68	NA	NA	0.40	600	1.62	0.97
Total			110.96							

Notes:

CN calculated for pervious areas only for DESIGN STANDHYD. CN is a weighed average for DESIGN NASHYD

TIMP Total percent impervious

XIMP Percent impervious directly connected

Length $L = [A * 10000 / 1.5]^{0.5}$

Time of Concentration calculated using the Airport Method $Tc = [3.26 (1.1 - C) L^{0.5}] / S^{0.33}$
 Where: C = Runoff Coefficient = 0.2 for undeveloped areas
 L = Length of Overland Flow (m)
 $S = (Area / 1.5)^{0.5}$
 S = Slope (%)

Time to Peak $Tp = 0.6Tc$

Subject: Volumetric Sizing
Project: Colonel Talbot Complete Corridor
Project No.: 161414170
Client: Sifton/York
Date: November 2, 2022

2 Yr Predev Flow 1.803 m³/s
100 Yr Predev Flow 8.208 m³/s

	Contributing Areas	Area (ha)	%	2 Yr Release Rate (m ³ /s)	100 Yr Release Rate (m ³ /s)	Modelled Pond Volume (m ³)	Pond Volume with Freeboard (m ³)
External Pond	EXT1, EXT2	32.71	29.5%	0.53	2.42	12000	14400
Pond 1	100	4.08	3.7%	0.07	0.30	2000	2400
Pond 2	200	7.53	6.8%	0.12	0.56	3000	3600
Pond 3	300, 301, 302	18.88	17.0%	0.31	1.40	5800	6960
Pond 4	400, 401, 402	18.94	17.1%	0.31	1.40	7000	8400
Pond 5	500, 501, 502	11.52	10.4%	0.19	0.85	5000	6000
Channel	600, 601, 602	8.14	7.3%	0.13	0.60		
EXT3	EXT3	9.16	8.3%	0.15	0.68	5000	
Totals		110.96	100.0%	1.80	8.21		41760


```

00001> 2 Metric units
00002> * Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
00003> * Date : 2022-11-14
00004> * Modeller : [AKK]
00005> * Company : Stantec Consulting Ltd. (London)
00006> * License # : 4730904
00007> *
00008> *
00009> *
00010> *
00011> * This model represents the hydrologic characteristics of the existing and
00012> * proposed conditions in the proposed subdivision.
00013> * Storm events modeled are:
00014> * 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
00015> *
00016> *
00017> *
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00023> *
00024> *
00025> * Existing Conditions to determine target release rates
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00050> *
00051> *
00052> *
00053> * External Pond Sizing, Cas EXT1 and EXT2
00054> *
00055> *
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00087> *
00088> *
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00090> *
00091> *
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```

```

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00137> *
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00140> *
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00176> *
00177> *
00178> *
00179> * Pond 4 Sizing, Cas 400, 401 and 402
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00181> *
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00214>
00215> [ 0.0 , 0.0 ]
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00218> [ -1 , -1 ] (max twenty pts)
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00221> *
00222> *
00223> *
00224> * Pond 5 Sizing, Cas 500, 501 and 502
00225> *
00226> *
00227> CALIB STANDHYD ID=[01], NHYD=["501"], DT=[1] (min), AREA=[2.93],
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00229> SCS curve number CN=[86],
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00231> LGP=[40], MNF=[0.24], SCP=[0] (min),
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00244> *
00245> CALIB STANDHYD ID=[03], NHYD=["502"], DT=[1] (min), AREA=[5.45],
00246> XIMP=[0.45], TIMP=[0.55], DWF=[0], LOSS=[2],
00247> SCS curve number CN=[86],
00248> Pervious surfaces: IAPER=[5], SLPP=[1] (%),
00249> LGP=[40], MNF=[0.24], SCP=[0] (min),
00250> Impervious surfaces: IAIMP=[2], SLPI=[1] (%),
00251> LGI=[600], MNI=[0.013], SCI=[0] (min),
00252> RAINFALL=[ , , , ] (mm/hr), END=-1
00253> *
00254> ADD HYD Idsum=[04], NHYD=["Pond5In"], IDs to add=[01+02+03]

```

```

00255> *%-----|-----|
00256> ROUTE RESERVOIR IDout=[05], NHYD=["Pond5"], IDin=[04],
00257> RDT=[1](min),
00258> TABLE of ( OUTFLOW-STORAGE ) values
00259>
00260> [ 0.0 , 0.0 ]
00261> [ 0.19 , 0.23 ]
00262> [ 0.85 , 0.50 ]
00263> [ -1 , -1 ] (max twenty pts)
00264> IDovf=["oops"], NHYDovf=[01]
00265> *%-----|-----|
00266> *#-----|
00267> *#
00268> *# EXT3 Sizing, Cas EXT3
00269> *#
00270> *#-----|
00271> CALIB STANDHYD ID=[01], NHYD=["EXT3"], DT=[1](min), AREA=[9.16],
00272> XIMP=[0.45], TIMP=[0.55], DWF=[0], LOSS=[2],
00273> SCS curve number CN=[86],
00274> Pervious surfaces: IAPer=[5], SLP=[1](%),
00275> LGP=[40], MNP=[0.24], SCP=[0](min),
00276> Impervious surfaces: IAimp=[2], SLP=[1](%),
00277> LGI=[40], MNI=[0.013], SCI=[0](min),
00278> RAINFALL=[ , , , ], END=-1
00279> *%-----|-----|
00280> COMPUTE DUALHYD IDin=[01], CINLET=[0.15](cms), NINLET=[1],
00281> MAJID=[02], MajNHYD=["noFlow"],
00282> MINID=[03], MinNHYD=["MinorEXT3"],
00283> TMJSTO=[5000](cu-m)
00284> *%-----|-----|
00285> *#-----|
00286> *#
00287> *# Flow Totals and Channel Runoff
00288> *#
00289> *#-----|
00290> ADD HYD IDsum=[01], NHYD=["Control"], IDs to add=[02+03+05+06+07+08+
00291> *%-----|
00292> CALIB NASHYD ID=[02], NHYD=["600"], DT=[1]min, AREA=[0.99](ha),
00293> DWF=[0](cms), CN/C=[68], IA=[5](mm),
00294> N=[3], TP=[0.35]hrs,
00295> RAINFALL=[ , , , ](mm/hr), END=-1
00296> *%-----|-----|
00297> CALIB NASHYD ID=[03], NHYD=["601"], DT=[1]min, AREA=[3.54](ha),
00298> DWF=[0](cms), CN/C=[68], IA=[5](mm),
00299> N=[3], TP=[0.59]hrs,
00300> RAINFALL=[ , , , ](mm/hr), END=-1
00301> *%-----|-----|
00302> CALIB NASHYD ID=[04], NHYD=["602"], DT=[1]min, AREA=[3.61](ha),
00303> DWF=[0](cms), CN/C=[68], IA=[5](mm),
00304> N=[3], TP=[0.97]hrs,
00305> RAINFALL=[ , , , ](mm/hr), END=-1
00306> *%-----|-----|
00307> ADD HYD IDsum=[05], NHYD=["PostTot"], IDs to add=[01+02+03+04]
00308> *%-----|
00309> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
00310> ["1dn5YR.3hr"]
00311> *%-----|-----|
00312> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
00313> ["1dn10YR.3hr"]
00314> *%-----|-----|
00315> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
00316> ["1dn25YR.3hr"]
00317> *%-----|-----|
00318> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
00319> ["1dn50YR.3hr"]
00320> *%-----|-----|
00321> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
00322> ["1dn100YR.3hr"]
00323> *%-----|-----|
00324> START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[250]
00325> ["1dn250YR.3hr"]
00326> *%-----|-----|
00327>
00328> FINISH
00329>
00330>
00331>
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00382>
00383>

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00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999 =====
00004> S W W M M H H Y Y M M O O 9 9 9 9
00005> SSSSS W W M M M H H H Y Y M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M O O 9 9 9 =====
00008> 9 9 9 9 # 4730904
00009> StormWater Management Hydrologic Model 999 999 =====
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTTHYMO-83 and OTTHYMO-89. *****
00016> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhymo@fsa.com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: Stantec Consulting Ltd. (Kitchener) *****
00025> ***** Kitchener SERIAL#:4730904 *****
00026> *****
00027> *****
00028> *****
00029> ***** PROGRAM ARRAY DIMENSIONS *****
00030> ***** Maximum value for ID numbers : 10 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034> *****
00035> *****
00036> ***** D E T A I L E D O U T P U T *****
00037> *****
00038> * DATE: 2022-11-14 TIME: 16:30:48 RUN COUNTER: 000087 *
00039> *****
00040> * Input filename: C:\MODELL-1\14170\SWMHYMO\swmf_vol.dat *
00041> * Output filename: C:\MODELL-1\14170\SWMHYMO\swmf_vol.out *
00042> * Summary filename: C:\MODELL-1\14170\SWMHYMO\swmf_vol.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048>
00049>
00050> 001:0001-----
00051> *****
00052> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
00053> *# Date : 2022-11-14
00054> *# Modeller : [AKK]
00055> *# Company : Stantec Consulting Ltd. (London)
00056> *# License # : 4730904
00057> *****
00058> *# *****
00059> *#
00060> *# This model represents the hydrologic characteristics of the existing and
00061> *# proposed conditions in the proposed subdivision.
00062> *# Storm events modeled are:
00063> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
00064> *#
00065> *# *****
00066> *# END OF RUN : 1
00067> *****
00068>
00069>
00070>
00071>
00072>
00073>
00074>
00075> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
00076> | TZERO = 00 hrs on | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
00077> | METOUT= 2 (output = METRIC)
00078> | NRUN = 002
00079> | NSTORM= 1
00080> | # 1=1dn2yr.3hr
00081> *****
00082>
00083> 002:0002-----
00084> *****
00085> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
00086> *# Date : 2022-11-14
00087> *# Modeller : [AKK]
00088> *# Company : Stantec Consulting Ltd. (London)
00089> *# License # : 4730904
00090> *****
00091> *# *****
00092> *#
00093> *# This model represents the hydrologic characteristics of the existing and
00094> *# proposed conditions in the proposed subdivision.
00095> *# Storm events modeled are:
00096> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
00097> *#
00098> *# *****
00099> *#
00100> 002:0002-----
00101>
00102> | READ STORM | Filename: 2-yr, 3hr Chicago Storm from 2021 London
00103> | Ptotal= 32.83 mm | Comments: 2-yr, 3hr Chicago Storm from 2021 London
00104>
00105> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
00106> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
00107> .08 2.574 | .83 14.974 | 1.58 7.501 | 2.33 3.414
00108> .17 2.812 | .92 35.641 | 1.67 6.585 | 2.42 3.229
00109> .25 3.105 | 1.00 108.068 | 1.75 5.876 | 2.50 3.064
00110> .33 3.472 | 1.08 46.277 | 1.83 5.310 | 2.58 2.917
00111> .42 3.949 | 1.17 25.470 | 1.92 4.849 | 2.67 2.784
00112> .50 4.594 | 1.25 17.290 | 2.00 4.465 | 2.75 2.663
00113> .58 5.517 | 1.33 13.030 | 2.08 4.141 | 2.83 2.554
00114> .67 6.947 | 1.42 10.448 | 2.17 3.864 | 2.92 2.454
00115> .75 9.460 | 1.50 8.726 | 2.25 3.624 | 3.00 2.362
00116>
00117>
00118> 002:0003-----
00119> *****
00120> *#
00121> *# Existing Conditions to determine target release rates
00122> *#
00123> *****
00124>
00125> | CALIB NASHYD | Area (ha)= 49.50 Curve Number (CN)=84.00
00126> | 01:S101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
00127> | U.H. Tp(hrs)= .840

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00128>
00129> Unit Hyd Qpeak (cms)= 2.251
00130>
00131> PEAK FLOW (cms)= .654 (i)
00132> TIME TO PEAK (hrs)= 2.167
00133> RUNOFF VOLUME (mm)= 10.165
00134> TOTAL RAINFALL (mm)= 32.834
00135> RUNOFF COEFFICIENT = .310
00136>
00137> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00138>
00139>
00140> 002:0004-----
00141>
00142> | CALIB NASHYD | Area (ha)= 32.80 Curve Number (CN)=84.00
00143> | 02:S102 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
00144> | U.H. Tp(hrs)= .620
00145>
00146> Unit Hyd Qpeak (cms)= 2.021
00147>
00148> PEAK FLOW (cms)= .534 (i)
00149> TIME TO PEAK (hrs)= 1.867
00150> RUNOFF VOLUME (mm)= 10.165
00151> TOTAL RAINFALL (mm)= 32.834
00152> RUNOFF COEFFICIENT = .310
00153>
00154> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00155>
00156>
00157> 002:0005-----
00158>
00159> | CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
00160> | 03:S103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
00161> | U.H. Tp(hrs)= .480
00162>
00163> Unit Hyd Qpeak (cms)= .708
00164>
00165> PEAK FLOW (cms)= .172 (i)
00166> TIME TO PEAK (hrs)= 1.667
00167> RUNOFF VOLUME (mm)= 10.165
00168> TOTAL RAINFALL (mm)= 32.834
00169> RUNOFF COEFFICIENT = .310
00170>
00171> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00172>
00173>
00174> 002:0006-----
00175>
00176> | CALIB NASHYD | Area (ha)= 33.50 Curve Number (CN)=84.00
00177> | 04:S104 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
00178> | U.H. Tp(hrs)= .720
00179>
00180> Unit Hyd Qpeak (cms)= 1.777
00181>
00182> PEAK FLOW (cms)= .492 (i)
00183> TIME TO PEAK (hrs)= 2.000
00184> RUNOFF VOLUME (mm)= 10.165
00185> TOTAL RAINFALL (mm)= 32.834
00186> RUNOFF COEFFICIENT = .310
00187>
00188> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00189>
00190>
00191> 002:0007-----
00192>
00193> | ADD HYD (Total ) | ID: NHYD | AREA | QPEAK | TPEAK | R.V. | DWF
00194> | (ha) | (cms) | (hrs) | (mm) | (cms) |
00195> | ID1 01:S101 | 49.50 | .654 | 2.17 | 10.17 | .000
00196> | +ID2 02:S102 | 32.80 | .534 | 1.87 | 10.17 | .000
00197> | +ID3 03:S103 | 8.90 | .172 | 1.67 | 10.17 | .000
00198> | +ID4 04:S104 | 33.50 | .492 | 2.00 | 10.17 | .000
00199> |
00200> | SUM 05:Total | 124.70 | 1.803 | 1.97 | 10.17 | .000
00201>
00202> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00203>
00204>
00205> 002:0008-----
00206> *****
00207> *#
00208> *# External Pond Sizing, CAs EXT1 and EXT2
00209> *#
00210> *****
00211>
00212> | CALIB STANDHYD | Area (ha)= 9.50
00213> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
00214>
00215> IMPERVIOUS PERVIOUS (i)
00216> Surface Area (ha)= 5.22 4.27
00217> Dep. Storage (mm)= 2.00 5.00
00218> Average Slope (%)= 1.00 1.00
00219> Length (m)= 400.00 40.00
00220> Mannings n = .013 .240
00221>
00222> Max.eff.Inten.(mm/hr)= 97.77 25.35
00223> over (min)= 6.00 21.00
00224> Storage Coeff. (min)= 5.92 (ii) 20.60 (ii)
00225> Unit Hyd. Tpeak (min)= 6.00 21.00
00226> Unit Hyd. peak (cms)= .19 .05
00227>
00228> PEAK FLOW (cms)= .79 .17
00229> TIME TO PEAK (hrs)= 1.07 1.40
00230> RUNOFF VOLUME (mm)= 30.83 13.20
00231> TOTAL RAINFALL (mm)= 32.83 32.83
00232> RUNOFF COEFFICIENT = .94 .644
00233>
00234> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00235> CN* = 86.0 Ia = Dep. Storage (Above)
00236> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00237> THAN THE STORAGE COEFFICIENT.
00238> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00239>
00240>
00241> 002:0009-----
00242>
00243> | CALIB STANDHYD | Area (ha)= 23.00
00244> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
00245>
00246> IMPERVIOUS PERVIOUS (i)
00247> Surface Area (ha)= 12.65 10.35
00248> Dep. Storage (mm)= 2.00 5.00
00249> Average Slope (%)= 1.00 1.00
00250> Length (m)= 750.00 40.00
00251> Mannings n = .013 .240
00252>
00253> Max.eff.Inten.(mm/hr)= 80.61 22.86
00254> over (min)= 9.00 25.00

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00255> Storage Coeff. (min)= 9.33 (ii) 24.63 (ii)
00256> Unit Hyd. Tpeak (min)= 9.00 25.00
00257> Unit Hyd. peak (cms)= .12 .05
00258>
00259> PEAK FLOW (cms)= 1.53 .37 *TOTALS*
00260> TIME TO PEAK (hrs)= 1.12 1.47 1.634 (iii)
00261> RUNOFF VOLUME (mm)= 30.83 13.20 21.137
00262> TOTAL RAINFALL (mm)= 32.83 32.83 32.834
00263> RUNOFF COEFFICIENT = .94 .40 .644
00264>
00265> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00266> CN* = 86.0 Ia = Dep. Storage (Above)
00267> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00268> THAN THE STORAGE COEFFICIENT.
00269> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00270>
00271>
00272> 002:0010-----
00273>
00274> | ADD HYD (ExPondIn ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00275> |-----|-----|-----|-----|-----|-----|
00276> | ID1 01:EXT2 | 9.50 .825 1.07 21.14 .000
00277> | +ID2 02:EXT1 | 23.00 1.634 1.13 21.14 .000
00278> |-----|-----|-----|-----|-----|
00279> | SUM 03:ExPondIn | 32.50 2.387 1.12 21.14 .000
00280>
00281> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00282>
00283>
00284> 002:0011-----
00285>
00286> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00287> | IN:03: (ExPond) |
00288> | OUT:10: (ExPond) |
00289>
00290> ===== OUTFLOW STORAGE TABLE =====
00291> OUTFLOW STORAGE | OUTFLOW STORAGE
00292> (cms) (ha.m.) | (cms) (ha.m.)
00293> .000 .0000E+00 | 2.420 .1200E+01
00294> .530 .4500E+00 | .000 .0000E+00
00295>
00296> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00297> (ha) (cms) (hrs) (mm)
00298> INFLOW >03: (ExPond) 32.50 2.387 1.117 21.137
00299> OUTFLOW<10: (ExPond) 32.50 .475 2.133 21.137
00300>
00301> PEAK FLOW REDUCTION [Qout/Qin] (%) = 19.886
00302> TIME SHIFT OF PEAK FLOW (min) = 61.00
00303> MAXIMUM STORAGE USED (ha.m.) = 4.030E+00
00304>
00305> 002:0012-----
00306> *#*****
00307> *# Pond 1 Sizing, Cas 100
00308> *#
00309> *#*****
00310>
00311> | CALIB STANDHYD | Area (ha)= 4.08
00312> | 01:100 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00313>
00314> IMPERVIOUS PERVIOUS (i)
00315> Surface Area (ha)= 2.24 1.84
00316> Dep. Storage (mm)= 2.00 5.00
00317> Average Slope (%) = 1.00 1.00
00318> Length (m) = 300.00 40.00
00319> Mannings n = .013 .240
00320>
00321> Max.eff.Inten.(mm/hr)= 108.07 26.83
00322> over (min) = 5.00 19.00
00323> Storage Coeff. (min)= 4.79 (ii) 19.14 (ii)
00324> Unit Hyd. Tpeak (min)= 5.00 19.00
00325> Unit Hyd. peak (cms)= .23 .06
00326>
00327> PEAK FLOW (cms)= .37 .08 *TOTALS*
00328> TIME TO PEAK (hrs)= 1.05 1.37 1.050
00329> RUNOFF VOLUME (mm)= 30.83 13.20 21.137
00330> TOTAL RAINFALL (mm)= 32.83 32.83 32.834
00331> RUNOFF COEFFICIENT = .94 .40 .644
00332>
00333> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00334> CN* = 86.0 Ia = Dep. Storage (Above)
00335> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00336> THAN THE STORAGE COEFFICIENT.
00337> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00338>
00339>
00340> 002:0013-----
00341>
00342> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00343> | IN:01: (100 ) |
00344> | OUT:09: (Pond1 ) |
00345>
00346> ===== OUTFLOW STORAGE TABLE =====
00347> OUTFLOW STORAGE | OUTFLOW STORAGE
00348> (cms) (ha.m.) | (cms) (ha.m.)
00349> .000 .0000E+00 | .300 .2000E+00
00350> .070 .7000E-01 | .000 .0000E+00
00351>
00352> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00353> (ha) (cms) (hrs) (mm)
00354> INFLOW >01: (100 ) 4.08 .386 1.050 21.137
00355> OUTFLOW<09: (Pond1 ) 4.08 .054 2.117 21.137
00356>
00357> PEAK FLOW REDUCTION [Qout/Qin] (%) = 13.934
00358> TIME SHIFT OF PEAK FLOW (min) = 64.00
00359> MAXIMUM STORAGE USED (ha.m.) = 5.382E-01
00360>
00361> 002:0014-----
00362> *#*****
00363> *# Pond 2 Sizing, Cas 200
00364> *#
00365> *#*****
00366>
00367> | CALIB STANDHYD | Area (ha)= 7.53
00368> | 01:200 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00369>
00370> IMPERVIOUS PERVIOUS (i)
00371> Surface Area (ha)= 4.14 3.39
00372> Dep. Storage (mm)= 2.00 5.00
00373> Average Slope (%) = 1.00 1.00
00374> Length (m) = 550.00 40.00
00375> Mannings n = .013 .240
00376>
00377> Max.eff.Inten.(mm/hr)= 90.41 24.64
00378> over (min) = 7.00 22.39
00379> Storage Coeff. (min)= 7.40 (ii) 22.25 (ii)
00380> Unit Hyd. Tpeak (min)= 7.00 22.00
00381> Unit Hyd. peak (cms)= .16 .05

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00382>
00383> *TOTALS*
00384> PEAK FLOW (cms)= .56 .13 1.597 (iii)
00385> TIME TO PEAK (hrs)= 1.08 1.42 1.083
00386> RUNOFF VOLUME (mm)= 30.83 13.20 21.137
00387> TOTAL RAINFALL (mm)= 32.83 32.83 32.834
00388> RUNOFF COEFFICIENT = .94 .40 .644
00389>
00390> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00391> CN* = 86.0 Ia = Dep. Storage (Above)
00392> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00393> THAN THE STORAGE COEFFICIENT.
00394> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00395>
00396> 002:0015-----
00397>
00398> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00399> | IN:01: (200 ) |
00400> | OUT<08: (Pond2 ) |
00401> ===== OUTFLOW STORAGE TABLE =====
00402> OUTFLOW STORAGE | OUTFLOW STORAGE
00403> (cms) (ha.m.) | (cms) (ha.m.)
00404> .000 .0000E+00 | .560 .3000E+00
00405> .120 .1500E+00 | .000 .0000E+00
00406>
00407> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00408> (ha) (cms) (hrs) (mm)
00409> INFLOW >01: (200 ) 7.53 .597 1.083 21.137
00410> OUTFLOW<08: (Pond2 ) 7.53 .084 2.367 21.137
00411>
00412> PEAK FLOW REDUCTION [Qout/Qin] (%) = 14.039
00413> TIME SHIFT OF PEAK FLOW (min) = 77.00
00414> MAXIMUM STORAGE USED (ha.m.) = 1.048E+00
00415>
00416> 002:0016-----
00417> *#*****
00418> *#
00419> *# Pond 3 Sizing, Cas 300, 301 and 302
00420> *#
00421> *#*****
00422>
00423> | CALIB STANDHYD | Area (ha)= 10.33
00424> | 01:300 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00425>
00426> IMPERVIOUS PERVIOUS (i)
00427> Surface Area (ha)= 5.68 4.65
00428> Dep. Storage (mm)= 2.00 5.00
00429> Average Slope (%) = 1.00 1.00
00430> Length (m) = 610.00 40.00
00431> Mannings n = .013 .240
00432>
00433> Max.eff.Inten.(mm/hr)= 84.90 23.99
00434> over (min) = 8.00 23.00
00435> Storage Coeff. (min)= 8.07 (ii) 23.08 (ii)
00436> Unit Hyd. Tpeak (min)= 8.00 23.00
00437> Unit Hyd. peak (cms)= .14 .05
00438>
00439> PEAK FLOW (cms)= .74 .17 *TOTALS*
00440> TIME TO PEAK (hrs)= 1.10 1.43 1.100
00441> RUNOFF VOLUME (mm)= 30.83 13.20 21.137
00442> TOTAL RAINFALL (mm)= 32.83 32.83 32.834
00443> RUNOFF COEFFICIENT = .94 .40 .644
00444>
00445> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00446> CN* = 86.0 Ia = Dep. Storage (Above)
00447> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00448> THAN THE STORAGE COEFFICIENT.
00449> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00450>
00451>
00452> 002:0017-----
00453>
00454> | CALIB STANDHYD | Area (ha)= 4.18
00455> | 02:302 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00456>
00457> IMPERVIOUS PERVIOUS (i)
00458> Surface Area (ha)= 2.30 1.88
00459> Dep. Storage (mm)= 2.00 5.00
00460> Average Slope (%) = 1.00 1.00
00461> Length (m) = 210.00 40.00
00462> Mannings n = .013 .240
00463>
00464> Max.eff.Inten.(mm/hr)= 108.07 27.62
00465> over (min) = 4.00 18.00
00466> Storage Coeff. (min)= 3.87 (ii) 18.05 (ii)
00467> Unit Hyd. Tpeak (min)= 4.00 18.00
00468> Unit Hyd. peak (cms)= .29 .06
00469>
00470> *TOTALS*
00471> PEAK FLOW (cms)= .41 .08 1.430 (iii)
00472> TIME TO PEAK (hrs)= 1.03 1.35 1.033
00473> RUNOFF VOLUME (mm)= 30.83 13.20 21.137
00474> TOTAL RAINFALL (mm)= 32.83 32.83 32.834
00475> RUNOFF COEFFICIENT = .94 .40 .644
00476>
00477> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00478> CN* = 86.0 Ia = Dep. Storage (Above)
00479> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00480> THAN THE STORAGE COEFFICIENT.
00481> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00482>
00483> 002:0018-----
00484>
00485> | CALIB NASHYD | Area (ha)= 4.37 Curve Number (CN)=76.00
00486> | 03:301 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
00487> | U.H. Tp (hrs)= .410
00488>
00489> Unit Hyd Qpeak (cms)= .407
00490>
00491> PEAK FLOW (cms)= .064 (i)
00492> TIME TO PEAK (hrs)= 1.583
00493> RUNOFF VOLUME (mm)= 7.171
00494> TOTAL RAINFALL (mm)= 32.834
00495> RUNOFF COEFFICIENT = .218
00496>
00497> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00498>
00499>
00500> 002:0019-----
00501>
00502> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
00503> |-----|-----|-----|-----|-----|-----|
00504> | ID1 01:300 | 10.33 .786 1.10 21.14 .000
00505> | +ID2 02:302 | 4.18 .430 1.03 21.14 .000
00506> | +ID3 03:301 | 4.37 .064 1.58 7.17 .000
00507> |-----|-----|-----|-----|-----|-----|
00508> | SUM 04:Pond3In | 18.88 1.141 1.08 17.90 .000

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00509>
00510> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00511>
00512>
-----
00513> 002:0020-----
00514>
00515> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00516> | IN>04:(Pond31) |
00517> | OUT<07:(Pond3) |
=====
00518> OUTFLOW STORAGE | OUTFLOW STORAGE
00519> (cms) (ha.m.) | (cms) (ha.m.)
00520> .000 .0000E+00 | 1.400 .5800E+00
00521> .310 .2500E+00 | .000 .0000E+00
00522>
00523> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00524> (ha) (cms) (hrs) (mm)
00525> INFLOW >04: (Pond31) 18.88 1.141 1.083 17.904
00526> OUTFLOW<07: (Pond3) 18.88 .240 2.150 17.904
00527>
00528> PEAK FLOW REDUCTION [Qout/Qin] (%) = 21.030
00529> TIME SHIFT OF PEAK FLOW (min) = 64.00
00530> MAXIMUM STORAGE USED (ha.m.) = 1935E+00
00531>
00532>
-----
00533> 002:0021-----
00534> *****
00535> *#
00536> *# Pond 4 Sizing, Cas 400, 401 and 402
00537> *#
00538> *****
00539>
00540> | CALIB STANDHYD | Area (ha) = 10.47
00541> | 01:402 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00542>
00543> IMPERVIOUS PERVIOUS (i)
00544> Surface Area (ha) = 5.76 4.71
00545> Dep. Storage (mm) = 2.00 5.00
00546> Average Slope (%) = 1.00 1.00
00547> Length (m) = 350.00 40.00
00548> Mannings n = .013 .240
00549>
00550> Max.eff.Inten.(mm/hr) = 108.07 26.83
00551> over (min) = 5.00 20.00
00552> Storage Coeff. (min) = 4.25 (ii) 19.76 (ii)
00553> Unit Hyd. Tpeak (min) = 5.00 20.00
00554> Unit Hyd. peak (cms) = .22 .06
00555>
00556> PEAK FLOW (cms) = .92 .19 *TOTALS*
00557> TIME TO PEAK (hrs) = 1.05 1.38 .958 (iii)
00558> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00559> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00560> RUNOFF COEFFICIENT = .94 .40 .644
00561>
00562> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00563> CN* = 86.0 Ia = Dep. Storage (Above)
00564> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00565> THAN THE STORAGE COEFFICIENT.
00566> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00567>
-----
00568> 002:0022-----
00569>
00570> | CALIB STANDHYD | Area (ha) = 3.22
00571> | 02:401 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00572>
00573> IMPERVIOUS PERVIOUS (i)
00574> Surface Area (ha) = 1.77 1.45
00575> Dep. Storage (mm) = 2.00 5.00
00576> Average Slope (%) = 1.00 1.00
00577> Length (m) = 250.00 40.00
00578> Mannings n = .013 .240
00579>
00580> Max.eff.Inten.(mm/hr) = 108.07 26.83
00581> over (min) = 4.00 19.00
00582> Storage Coeff. (min) = 4.29 (ii) 18.64 (ii)
00583> Unit Hyd. Tpeak (min) = 4.00 19.00
00584> Unit Hyd. peak (cms) = .27 .06
00585>
00586> PEAK FLOW (cms) = .31 .06 *TOTALS*
00587> TIME TO PEAK (hrs) = 1.03 1.37 1.033
00588> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00589> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00590> RUNOFF COEFFICIENT = .94 .40 .644
00591>
00592> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00593> CN* = 86.0 Ia = Dep. Storage (Above)
00594> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00595> THAN THE STORAGE COEFFICIENT.
00596> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00597>
-----
00598> 002:0023-----
00599>
00600> | CALIB STANDHYD | Area (ha) = 5.25
00601> | 03:400 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00602>
00603> IMPERVIOUS PERVIOUS (i)
00604> Surface Area (ha) = 2.89 2.36
00605> Dep. Storage (mm) = 2.00 5.00
00606> Average Slope (%) = 1.00 1.00
00607> Length (m) = 250.00 40.00
00608> Mannings n = .013 .240
00609>
00610> Max.eff.Inten.(mm/hr) = 108.07 26.83
00611> over (min) = 4.00 19.00
00612> Storage Coeff. (min) = 4.29 (ii) 18.64 (ii)
00613> Unit Hyd. Tpeak (min) = 4.00 19.00
00614> Unit Hyd. peak (cms) = .27 .06
00615>
00616> PEAK FLOW (cms) = .50 .10 *TOTALS*
00617> TIME TO PEAK (hrs) = 1.03 1.37 .521 (iii)
00618> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00619> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00620> RUNOFF COEFFICIENT = .94 .40 .644
00621>
00622> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00623> CN* = 86.0 Ia = Dep. Storage (Above)
00624> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00625> THAN THE STORAGE COEFFICIENT.
00626> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00627>
-----
00628> 002:0024-----
00629>
00630> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DMF
00631> (ha) (cms) (hrs) (mm) (cms)
00632> ID1 01:402 10.47 .958 1.05 21.14 .000
00633>

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00636> +ID2 02:401 3.22 .320 1.03 21.14 .000
00637> +ID3 03:400 5.25 .521 1.03 21.14 .000
00638>
00639> =====
00640> SUM 04:Pond4In 18.94 1.781 1.05 21.14 .000
00641>
00642> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00643>
-----
00644> 002:0025-----
00645>
00646> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00647> | IN>04:(Pond41) |
00648> | OUT<06:(Pond4) |
=====
00649> OUTFLOW STORAGE | OUTFLOW STORAGE
00650> (cms) (ha.m.) | (cms) (ha.m.)
00651> .000 .0000E+00 | 1.400 .7000E+00
00652> .310 .3000E+00 | .000 .0000E+00
00653>
00654> ROUTING RESULTS AREA QPEAK TPEAK R.V.
00655> (ha) (cms) (hrs) (mm)
00656> INFLOW >04: (Pond41) 18.94 1.781 1.050 21.137
00657> OUTFLOW<06: (Pond4) 18.94 .255 2.100 21.137
00658>
00659> PEAK FLOW REDUCTION [Qout/Qin] (%) = 14.343
00660> TIME SHIFT OF PEAK FLOW (min) = 63.00
00661> MAXIMUM STORAGE USED (ha.m.) = .2472E+00
00662>
00663>
-----
00664> 002:0026-----
00665>
00666> *#
00667> *# Pond 5 Sizing, Cas 500, 501 and 502
00668> *#
00669> *****
00670>
00671> | CALIB STANDHYD | Area (ha) = 2.93
00672> | 01:501 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00673>
00674> IMPERVIOUS PERVIOUS (i)
00675> Surface Area (ha) = 1.61 1.32
00676> Dep. Storage (mm) = 2.00 5.00
00677> Average Slope (%) = 1.00 1.00
00678> Length (m) = 250.00 40.00
00679> Mannings n = .013 .240
00680>
00681> Max.eff.Inten.(mm/hr) = 108.07 26.83
00682> over (min) = 4.00 19.00
00683> Storage Coeff. (min) = 4.29 (ii) 18.64 (ii)
00684> Unit Hyd. Tpeak (min) = 4.00 19.00
00685> Unit Hyd. peak (cms) = .27 .06
00686>
00687> PEAK FLOW (cms) = .28 .06 *TOTALS*
00688> TIME TO PEAK (hrs) = 1.03 1.37 1.033
00689> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00690> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00691> RUNOFF COEFFICIENT = .94 .40 .644
00692>
00693> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00694> CN* = 86.0 Ia = Dep. Storage (Above)
00695> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00696> THAN THE STORAGE COEFFICIENT.
00697> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00698>
-----
00699> 002:0027-----
00700>
00701> | CALIB STANDHYD | Area (ha) = 3.14
00702> | 02:500 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00703>
00704> IMPERVIOUS PERVIOUS (i)
00705> Surface Area (ha) = 1.73 1.41
00706> Dep. Storage (mm) = 2.00 5.00
00707> Average Slope (%) = 1.00 1.00
00708> Length (m) = 250.00 40.00
00709> Mannings n = .013 .240
00710>
00711> Max.eff.Inten.(mm/hr) = 108.07 26.83
00712> over (min) = 4.00 19.00
00713> Storage Coeff. (min) = 4.29 (ii) 18.64 (ii)
00714> Unit Hyd. Tpeak (min) = 4.00 19.00
00715> Unit Hyd. peak (cms) = .27 .06
00716>
00717> PEAK FLOW (cms) = .30 .06 *TOTALS*
00718> TIME TO PEAK (hrs) = 1.03 1.37 1.312 (iii)
00719> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00720> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00721> RUNOFF COEFFICIENT = .94 .40 .644
00722>
00723> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00724> CN* = 86.0 Ia = Dep. Storage (Above)
00725> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00726> THAN THE STORAGE COEFFICIENT.
00727> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00728>
-----
00729> 002:0028-----
00730>
00731> | CALIB STANDHYD | Area (ha) = 5.45
00732> | 03:502 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
00733>
00734> IMPERVIOUS PERVIOUS (i)
00735> Surface Area (ha) = 3.00 2.45
00736> Dep. Storage (mm) = 2.00 5.00
00737> Average Slope (%) = 1.00 1.00
00738> Length (m) = 600.00 40.00
00739> Mannings n = .013 .240
00740>
00741> Max.eff.Inten.(mm/hr) = 84.90 23.99
00742> over (min) = 8.00 23.00
00743> Storage Coeff. (min) = 7.99 (ii) 23.00 (ii)
00744> Unit Hyd. Tpeak (min) = 8.00 23.00
00745> Unit Hyd. peak (cms) = .14 .05
00746>
00747> PEAK FLOW (cms) = .39 .09 *TOTALS*
00748> TIME TO PEAK (hrs) = 1.10 1.43 4.16 (iii)
00749> RUNOFF VOLUME (mm) = 30.83 13.20 21.137
00750> TOTAL RAINFALL (mm) = 32.83 32.83 32.834
00751> RUNOFF COEFFICIENT = .94 .40 .644
00752>
00753> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00754> CN* = 86.0 Ia = Dep. Storage (Above)
00755> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00756> THAN THE STORAGE COEFFICIENT.
00757> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00758>
-----
00759> 002:0029-----
00760>
00761>
00762>

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00763> | ADD HYD (Pond5In ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
00764> |-----|-----|-----|-----|-----|-----|
00765> | IN:01:501 |          2.93      .291      1.03      21.14      .000
00766> | +ID2 02:500 |          3.14      .312      1.03      21.14      .000
00767> | +ID3 03:502 |          5.45      .416      1.10      21.14      .000
00768> |-----|-----|-----|-----|-----|-----|
00769> | SUM 04:Pond5In |        11.52      .949      1.05      21.14      .000
00770>
00771>
00772> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00773>
00774>
00775> 002:0030-----
00776>
00777> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
00778> | IN:04:(Pond5I) |
00779> | OUT:05:(Pond5) |
00780> |-----|-----|-----|-----|-----|-----|
00781> | OUTFLOW STORAGE | OUTFLOW STORAGE | OUTFLOW STORAGE |
00782> | (cms) (ha.m.) | (cms) (ha.m.) | (cms) (ha.m.) |
00783> | .000 .0000E+00 | .850 .5000E+00 | .000 .0000E+00 |
00784> |-----|-----|-----|-----|-----|-----|
00785> | ROUTING RESULTS | AREA      QPEAK      TPEAK      R.V.
00786> | (ha) (cms) (hrs) (mm) |
00787> | INFLOW >04: (Pond5I) |        11.52      .949      1.050      21.137
00788> | OUTFLOW<05: (Pond5) |         11.52      .132      2.300      21.137
00789>
00790> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 13.872
00791> | TIME SHIFT OF PEAK FLOW (min) = 75.00
00792> | MAXIMUM STORAGE USED (ha.m.) = .1593E+00
00793>
00794>
00795> 002:0031-----
00796> *****
00797> *#
00798> *# EXT3 Sizing, Cas EXT3
00799> *#
00800> *****
00801>
00802> | CALIB STANDHYD | Area (ha) = 9.16
00803> | 01:EXT3 DT= 1.00 | Total Imp(%) = 55.00 Dir. Conn.(%) = 45.00
00804>
00805> | IMPERVIOUS      PERVIOUS (i)
00806> | Surface Area (ha) = 5.04      4.12
00807> | Dep. Storage (mm) = 2.00      5.00
00808> | Average Slope (%) = 1.00      1.00
00809> | Length (m) = 400.00      40.00
00810> | Mannings n = .013      .240
00811>
00812> | Max.eff.Inten.(mm/hr) = 97.77      25.35
00813> | over (min) = 6.00      21.00
00814> | Storage Coeff. (min) = 5.92 (ii)      20.60 (ii)
00815> | Unit Hyd. Tpeak (min) = 6.00      21.00
00816> | Unit Hyd. peak (cms) = .19      .05
00817>
00818> | PEAK FLOW (cms) = .76      .17      .795 (iii)
00819> | TIME TO PEAK (hrs) = 1.07      1.40      1.067
00820> | RUNOFF VOLUME (mm) = 30.83      13.20      21.137
00821> | TOTAL RAINFALL (mm) = 32.83      32.83      32.834
00822> | RUNOFF COEFFICIENT = .94      .40      .644
00823>
00824> | (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00825> | CN* = 86.0 Ia = Dep. Storage (Above)
00826> | (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00827> | THAN THE STORAGE COEFFICIENT.
00828> | (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00829>
00830>
00831> 002:0032-----
00832>
00833> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
00834> | TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
00835> | Total minor system capacity = .150 (cms)
00836> | Total major system storage [TMJSTO] = 5000. (cu.m.)
00837>
00838> | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
00839> | (ha) (cms) (hrs) (mm) (cms) |
00840> | TOTAL HYD. 01:EXT3 |          9.16      .795      1.067      21.137      .000
00841> |-----|-----|-----|-----|-----|-----|
00842> | MAJOR SYST 02:noFlow |          .00      .000      .000      .000      .000
00843> | MINOR SYST 03:MinorE |          9.16      .150      .883      21.171      .000
00844>
00845> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00846>
00847> Maximum MAJOR SYSTEM storage used = 861. (cu.m.)
00848>
00849>
00850> 002:0033-----
00851> *****
00852> *#
00853> *# Flow Totals and Channel Runoff
00854> *#
00855> *****
00856>
00857> | ADD HYD (Control ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
00858> |-----|-----|-----|-----|-----|-----|
00859> | ID1 02:noFlow |          .00      .000      .00      .00      .000
00860> | +ID2 03:MinorEXT3 |          9.16      .150      .88      21.17      .000
00861> | +ID3 05:Pond5 |          11.52      .132      2.30      21.14      .000
00862> | +ID4 06:Pond4 |          18.94      .255      2.10      21.14      .000
00863> | +ID5 07:Pond3 |          18.88      .240      2.15      17.90      .000
00864> | +ID6 08:Pond2 |          7.53      .084      2.37      21.14      .000
00865> | +ID7 09:Pond1 |          4.08      .054      2.12      21.14      .000
00866> | +ID8 10:ExpFond |          32.50      .475      2.13      21.14      .000
00867> |-----|-----|-----|-----|-----|-----|
00868> | SUM 01:Control |        102.61      1.388      2.15      20.55      .000
00869>
00870> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00871>
00872>
00873> 002:0034-----
00874>
00875> | CALIB NASHYD | Area (ha) = .99 Curve Number (CN)=68.00
00876> | 02:600 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res.(N) = 3.00
00877> |-----|-----|-----|-----|-----|-----|
00878> | U.H. Tp(hrs) = .350
00879>
00880> | Unit Hyd Qpeak (cms) = .108
00881>
00882> | PEAK FLOW (cms) = .012 (i)
00883> | TIME TO PEAK (hrs) = 1.500
00884> | RUNOFF VOLUME (mm) = 5.257
00885> | TOTAL RAINFALL (mm) = 32.834
00886> | RUNOFF COEFFICIENT = .160
00887>
00888> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00889>

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00890> 002:0035-----
00891>
00892> | CALIB NASHYD | Area (ha) = 3.54 Curve Number (CN)=68.00
00893> | 03:601 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res.(N) = 3.00
00894> |-----|-----|-----|-----|-----|-----|
00895> | U.H. Tp(hrs) = .590
00896>
00897> | Unit Hyd Qpeak (cms) = .229
00898>
00899> | PEAK FLOW (cms) = .030 (i)
00900> | TIME TO PEAK (hrs) = 1.850
00901> | RUNOFF VOLUME (mm) = 5.257
00902> | TOTAL RAINFALL (mm) = 32.834
00903> | RUNOFF COEFFICIENT = .160
00904>
00905> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00906>
00907> 002:0036-----
00908>
00909> | CALIB NASHYD | Area (ha) = 3.61 Curve Number (CN)=68.00
00910> | 04:602 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res.(N) = 3.00
00911> |-----|-----|-----|-----|-----|-----|
00912> | U.H. Tp(hrs) = .970
00913>
00914> | Unit Hyd Qpeak (cms) = .142
00915>
00916> | PEAK FLOW (cms) = .022 (i)
00917> | TIME TO PEAK (hrs) = 2.383
00918> | RUNOFF VOLUME (mm) = 5.257
00919> | TOTAL RAINFALL (mm) = 32.834
00920> | RUNOFF COEFFICIENT = .160
00921>
00922> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00923>
00924> 002:0037-----
00925>
00926> | ADD HYD (PostTot ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
00927> |-----|-----|-----|-----|-----|-----|
00928> | ID1 01:Control |        102.61      1.388      2.15      20.55      .000
00929> | +ID2 02:600 |          .99      .012      1.50      5.26      .000
00930> | +ID3 03:601 |          3.54      .030      1.85      5.26      .000
00931> | +ID4 04:602 |          3.61      .022      2.38      5.26      .000
00932> |-----|-----|-----|-----|-----|-----|
00933> | SUM 05:PostTot |        110.75      1.443      2.13      19.42      .000
00934>
00935> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00936>
00937>
00938> 002:0038-----
00939> ** END OF RUN : 4
00940>
00941> *****
00942>
00943>
00944>
00945>
00946>
00947>
00948> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
00949> |-----|-----|-----|-----|-----|-----|
00950> | TZERO = .00 hrs on 0
00951> | METOUT= 2 (output = METRIC)
00952> | NRUN = 005
00953> | NSTORM= 1
00954> |-----|-----|-----|-----|-----|-----|
00955> | # 1=ldn5YR.3hr
00956>
00957> 005:0002-----
00958> *****
00959> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
00960> *# Date : 2022-11-14
00961> *# Modeller : [AKK]
00962> *# Company : Stantec Consulting Ltd. (London)
00963> *# License # : 4730904
00964> *****
00965> *#
00966> *# This model represents the hydrologic characteristics of the existing and
00967> *# proposed conditions in the proposed subdivision.
00968> *# Storm events modeled are:
00969> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
00970> *#
00971> *****
00972>
00973> 005:0002-----
00974>
00975> | READ STORM | Filename: 5-yr, 3hr Chicago Storm from London IDF
00976> | Ptotal= 44.19 mm | Comments: 5-yr, 3hr Chicago Storm from London IDF
00977>
00978>
00979> | TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN |
00980> | hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr |
00981> | .08 3.164 | .83 21.025 | 1.58 10.072 | 2.33 4.293
00982> | .17 3.481 | .92 50.463 | 1.67 8.751 | 2.42 4.042
00983> | .25 3.874 | 1.00 141.242 | 1.75 7.736 | 2.50 3.819
00984> | .33 4.373 | 1.08 65.260 | 1.83 6.932 | 2.58 3.620
00985> | .42 5.028 | 1.17 36.321 | 1.92 6.282 | 2.67 3.443
00986> | .50 5.925 | 1.25 24.430 | 2.00 5.745 | 2.75 3.282
00987> | .58 7.226 | 1.33 18.167 | 2.08 5.294 | 2.83 3.137
00988> | .67 9.274 | 1.42 14.372 | 2.17 4.910 | 2.92 3.005
00989> | .75 12.926 | 1.50 11.853 | 2.25 4.580 | 3.00 2.884
00990>
00991> 005:0003-----
00992> *****
00993> *#
00994> *# Existing Conditions to determine target release rates
00995> *#
00996> *****
00997>
00998> | CALIB NASHYD | Area (ha) = 49.50 Curve Number (CN)=84.00
00999> | 01:5101 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res.(N) = 3.00
10000> |-----|-----|-----|-----|-----|-----|
10001> | U.H. Tp(hrs) = .840
10002>
10003> | Unit Hyd Qpeak (cms) = 2.251
10004>
10005> | PEAK FLOW (cms) = 1.169 (i)
10006> | TIME TO PEAK (hrs) = 2.117
10007> | RUNOFF VOLUME (mm) = 17.536
10008> | TOTAL RAINFALL (mm) = 44.186
10009> | RUNOFF COEFFICIENT = .397
10010>
10011> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
10012>
10013> 005:0004-----
10014>
10015> | CALIB NASHYD | Area (ha) = 32.80 Curve Number (CN)=84.00
10016> | 02:5102 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res.(N) = 3.00

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01017> ----- U.H. Tp(hrs)= .620
01018>
01019> Unit Hyd Qpeak (cms)= 2.021
01020>
01021> PEAK FLOW (cms)= .963 (i)
01022> TIME TO PEAK (hrs)= 1.833
01023> RUNOFF VOLUME (mm)= 17.536
01024> TOTAL RAINFALL (mm)= 44.186
01025> RUNOFF COEFFICIENT = .397
01026>
01027> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
01029>
01030> 005:0005-----
01031>
01032> | CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
01033> | 03:S103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01034> | U.H. Tp(hrs)= .480
01035>
01036> Unit Hyd Qpeak (cms)= .708
01037>
01038> PEAK FLOW (cms)= .312 (i)
01039> TIME TO PEAK (hrs)= 1.650
01040> RUNOFF VOLUME (mm)= 17.536
01041> TOTAL RAINFALL (mm)= 44.186
01042> RUNOFF COEFFICIENT = .397
01043>
01044> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
01047> 005:0006-----
01048>
01049> | CALIB NASHYD | Area (ha)= 33.50 Curve Number (CN)=84.00
01050> | 04:S104 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01051> | U.H. Tp(hrs)= .720
01052>
01053> Unit Hyd Qpeak (cms)= 1.777
01054>
01055> PEAK FLOW (cms)= .884 (i)
01056> TIME TO PEAK (hrs)= 1.950
01057> RUNOFF VOLUME (mm)= 17.536
01058> TOTAL RAINFALL (mm)= 44.186
01059> RUNOFF COEFFICIENT = .397
01060>
01061> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
01064> 005:0007-----
01065>
01066> | ADD HYD (Total ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01067> | (ha) (cms) (hrs) (mm) (cms)
01068> | ID1 01:S101 49.50 1.169 2.12 17.54 .000
01069> | +ID2 02:S102 32.80 .963 1.83 17.54 .000
01070> | +ID3 03:S103 8.90 .312 1.65 17.54 .000
01071> | +ID4 04:S104 33.50 .884 1.95 17.54 .000
01072>
01073> SUM 05:Total 124.70 3.239 1.93 17.54 .000
01074>
01075> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01076>
01077>
01078> 005:0008-----
01079> *#*****
01080> *# External Pond Sizing, CAs EXT1 and EXT2
01081> *#
01082> *#
01083> *#*****
01084>
01085> | CALIB STANDHYD | Area (ha)= 9.50
01086> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01087> *#
01088> IMPERVIOUS PERVIOUS (i)
01089> Surface Area (ha)= 5.22 4.27
01090> Dep. Storage (mm)= 2.00 5.00
01091> Average Slope (%)= 1.00 1.00
01092> Length (m)= 400.00 40.00
01093> Mannings n = .013 .240
01094>
01095> Max.eff.Inten.(mm/hr)= 141.24 50.53
01096> over (min) 5.00 16.00
01097> Storage Coeff. (min)= 5.11 (ii) 16.25 (ii)
01098> Unit Hyd. Tpeak (min)= 5.00 16.00
01099> Unit Hyd. peak (cms)= .22 .07
01100> *#TOTALS*
01101> PEAK FLOW (cms)= 1.12 .35 1.226 (iii)
01102> TIME TO PEAK (hrs)= 1.05 1.30 1.050
01103> RUNOFF VOLUME (mm)= 42.19 21.75 30.944
01104> TOTAL RAINFALL (mm)= 44.19 44.19 44.186
01105> RUNOFF COEFFICIENT = .95 .49 .700
01106>
01107> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01108> CN* = 86.0 Ia = Dep. Storage (Above)
01109> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01110> THAN THE STORAGE COEFFICIENT.
01111> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01112>
01113>
01114> 005:0009-----
01115>
01116> | CALIB STANDHYD | Area (ha)= 23.00
01117> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01118> *#
01119> IMPERVIOUS PERVIOUS (i)
01120> Surface Area (ha)= 12.65 10.35
01121> Dep. Storage (mm)= 2.00 5.00
01122> Average Slope (%)= 1.00 1.00
01123> Length (m)= 750.00 40.00
01124> Mannings n = .013 .240
01125>
01126> Max.eff.Inten.(mm/hr)= 112.75 44.60
01127> over (min) 8.00 20.00
01128> Storage Coeff. (min)= 8.16 (ii) 19.87 (ii)
01129> Unit Hyd. Tpeak (min)= 8.00 20.00
01130> Unit Hyd. peak (cms)= .14 .06
01131> *#TOTALS*
01132> PEAK FLOW (cms)= 2.20 .74 2.488 (iii)
01133> TIME TO PEAK (hrs)= 1.10 1.37 1.117
01134> RUNOFF VOLUME (mm)= 42.18 21.74 30.944
01135> TOTAL RAINFALL (mm)= 44.19 44.19 44.186
01136> RUNOFF COEFFICIENT = .95 .49 .700
01137>
01138> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01139> CN* = 86.0 Ia = Dep. Storage (Above)
01140> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01141> THAN THE STORAGE COEFFICIENT.
01142> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01143>
01144>

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01144>
01145> 005:0010-----
01146>
01147> | ADD HYD (ExPondIn ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01148> | (ha) (cms) (hrs) (mm) (cms)
01149> | ID1 01:EXT2 9.50 1.226 1.05 30.94 .000
01150> | +ID2 02:EXT1 23.00 2.488 1.12 30.94 .000
01151>
01152> SUM 03:ExPondIn 32.50 3.619 1.10 30.94 .000
01153>
01154> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01155>
01156>
01157> 005:0011-----
01158>
01159> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01160> | IN>03: (ExPond) |
01161> | OUT<10: (ExPond) | ===== OUTFLOW STORAGE TABLE =====
01162> | OUTFLOW STORAGE | OUTFLOW STORAGE
01163> | (cms) (ha.m.) | (cms) (ha.m.)
01164> | .000 .0000E+00 | 2.420 .1200E+01
01165> | .530 .4500E+00 | .000 .0000E+00
01166>
01167> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01168> | (ha) (cms) (hrs) (mm)
01169> | INFLOW >03: (ExPond) 32.50 3.619 1.100 30.944
01170> | OUTFLOW<10: (ExPond) 32.50 .869 1.900 30.944
01171>
01172> PEAK FLOW REDUCTION [Qout/Qin] (%)= 24.003
01173> TIME SHIFT OF PEAK FLOW (min)= 48.00
01174> MAXIMUM STORAGE USED (ha.m.)= .5844E+00
01175>
01176>
01177> 005:0012-----
01178> *#*****
01179> *# Pond 1 Sizing, CAs 100
01180> *#
01181> *#
01182> *#*****
01183>
01184> | CALIB STANDHYD | Area (ha)= 4.08
01185> | 01:100 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01186> *#
01187> IMPERVIOUS PERVIOUS (i)
01188> Surface Area (ha)= 2.24 1.84
01189> Dep. Storage (mm)= 2.00 5.00
01190> Average Slope (%)= 1.00 1.00
01191> Length (m)= 300.00 40.00
01192> Mannings n = .013 .240
01193>
01194> Max.eff.Inten.(mm/hr)= 141.24 52.52
01195> over (min) 4.00 15.00
01196> Storage Coeff. (min)= 4.30 (ii) 15.27 (ii)
01197> Unit Hyd. Tpeak (min)= 4.00 15.00
01198> Unit Hyd. peak (cms)= .27 .07
01199> *#TOTALS*
01200> PEAK FLOW (cms)= .52 .15 1.561 (iii)
01201> TIME TO PEAK (hrs)= 1.03 1.28 1.033
01202> RUNOFF VOLUME (mm)= 42.19 21.75 30.944
01203> TOTAL RAINFALL (mm)= 44.19 44.19 44.186
01204> RUNOFF COEFFICIENT = .95 .49 .700
01205>
01206> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01207> CN* = 86.0 Ia = Dep. Storage (Above)
01208> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01209> THAN THE STORAGE COEFFICIENT.
01210> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01211>
01212>
01213> 005:0013-----
01214>
01215> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01216> | IN>01: (100 ) |
01217> | OUT<09: (Pond1 ) | ===== OUTFLOW STORAGE TABLE =====
01218> | OUTFLOW STORAGE | OUTFLOW STORAGE
01219> | (cms) (ha.m.) | (cms) (ha.m.)
01220> | .000 .0000E+00 | .300 .2000E+00
01221> | .070 .7000E-01 | .000 .0000E+00
01222>
01223> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01224> | (ha) (cms) (hrs) (mm)
01225> | INFLOW >01: (100 ) 4.08 .561 1.033 30.944
01226> | OUTFLOW<09: (Pond1 ) 4.08 .088 1.950 30.944
01227>
01228> PEAK FLOW REDUCTION [Qout/Qin] (%)= 15.672
01229> TIME SHIFT OF PEAK FLOW (min)= 55.00
01230> MAXIMUM STORAGE USED (ha.m.)= .8014E-01
01231>
01232>
01233> 005:0014-----
01234> *#*****
01235> *# Pond 2 Sizing, CAs 200
01236> *#
01237> *#
01238> *#*****
01239>
01240> | CALIB STANDHYD | Area (ha)= 7.53
01241> | 01:200 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01242> *#
01243> IMPERVIOUS PERVIOUS (i)
01244> Surface Area (ha)= 4.14 3.39
01245> Dep. Storage (mm)= 2.00 5.00
01246> Average Slope (%)= 1.00 1.00
01247> Length (m)= 550.00 40.00
01248> Mannings n = .013 .240
01249>
01250> Max.eff.Inten.(mm/hr)= 119.53 47.22
01251> over (min) 7.00 18.00
01252> Storage Coeff. (min)= 6.62 (ii) 18.06 (ii)
01253> Unit Hyd. Tpeak (min)= 7.00 18.00
01254> Unit Hyd. peak (cms)= .17 .06
01255> *#TOTALS*
01256> PEAK FLOW (cms)= .79 .26 .887 (iii)
01257> TIME TO PEAK (hrs)= 1.08 1.33 1.100
01258> RUNOFF VOLUME (mm)= 42.18 21.75 30.944
01259> TOTAL RAINFALL (mm)= 44.19 44.19 44.186
01260> RUNOFF COEFFICIENT = .95 .49 .700
01261>
01262> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01263> CN* = 86.0 Ia = Dep. Storage (Above)
01264> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01265> THAN THE STORAGE COEFFICIENT.
01266> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01267>
01268>
01269> 005:0015-----
01270>

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01271> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01272> | IN>01:(200 ) |
01273> | OUT<08:(Pond2 ) |
===== OUTFLOW STORAGE TABLE =====
01274> OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
01275> .000 .0000E+00 | .560 .3000E+00
01276> .120 .1500E+00 | .000 .0000E+00
01277>
01278>
ROUTING RESULTS AREA QPEAK TPEAK R.V.
01279> (ha) (cms) (hrs) (mm)
01280> INFLOW >01: (200 ) 7.53 .887 1.100 30.944
01281>
01282> OUTFLOW<08: (Pond2 ) 7.53 .137 2.150 30.944
01283>
01284>
01285> PEAK FLOW REDUCTION [Qout/Qin] (%) = 15.491
01286> TIME SHIFT OF PEAK FLOW (min) = 63.00
01287> MAXIMUM STORAGE USED (ha.m.) = .1560E+00
01288>
-----
01289> 005:0016-----
01290> *#*****
01291> *#
01292> *# Pond 3 Sizing, Cas 300, 301 and 302
01293> *#
01294> *#*****
01295>
01296> | CALIB STANDHYD | Area (ha) = 10.33
01297> | 01:300 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01298>
01299> IMPERVIOUS PERVIOUS (i)
01300> Surface Area (ha) = 5.68 4.65
01301> Dep. Storage (mm) = 2.00 5.00
01302> Average Slope (%) = 1.00 1.00
01303> Length (m) = 610.00 40.00
01304> Mannings n = .013 .240
01305>
01306> Max.eff.Inten.(mm/hr) = 119.53 45.84
01307> over (min) = 7.00 19.00
01308> Storage Coeff. (min) = 7.04 (ii) 18.62 (ii)
01309> Unit Hyd. Tpeak (min) = 7.00 19.00
01310> Unit Hyd. peak (cms) = .16 .06
01311>
01312> *#*****
01313> PEAK FLOW (cms) = 1.06 .35 1.183 (iii)
01314> TIME TO PEAK (hrs) = 1.08 1.35 1.100
01315> RUNOFF VOLUME (mm) = 44.19 21.75 30.944
01316> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01317> RUNOFF COEFFICIENT = .95 .49 .700
01318>
01319> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01320> CN* = 86.0 Ia = Dep. Storage (Above)
01321> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01322> THAN THE STORAGE COEFFICIENT.
01323> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01324>
-----
01325> 005:0017-----
01326>
01327> | CALIB STANDHYD | Area (ha) = 4.18
01328> | 02:302 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01329>
01330> IMPERVIOUS PERVIOUS (i)
01331> Surface Area (ha) = 2.30 1.88
01332> Dep. Storage (mm) = 2.00 5.00
01333> Average Slope (%) = 1.00 1.00
01334> Length (m) = 210.00 40.00
01335> Mannings n = .013 .240
01336>
01337> Max.eff.Inten.(mm/hr) = 141.24 54.10
01338> over (min) = 3.00 14.00
01339> Storage Coeff. (min) = 3.47 (ii) 14.31 (ii)
01340> Unit Hyd. Tpeak (min) = 3.00 14.00
01341> Unit Hyd. peak (cms) = .34 .08
01342>
01343> *#*****
01344> PEAK FLOW (cms) = .58 .16 .621 (iii)
01345> TIME TO PEAK (hrs) = 1.02 1.27 1.017
01346> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01347> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01348> RUNOFF COEFFICIENT = .95 .49 .700
01349>
01350> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01351> CN* = 86.0 Ia = Dep. Storage (Above)
01352> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01353> THAN THE STORAGE COEFFICIENT.
01354> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01355>
-----
01356> 005:0018-----
01357>
01358> | CALIB NASHYD | Area (ha) = 4.37 Curve Number (CN)=76.00
01359> | 03:301 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res. (N) = 3.00
01360> U.H. Tp (hrs) = .410
01361>
01362> Unit Hyd Qpeak (cms) = .407
01363>
01364> PEAK FLOW (cms) = .122 (i)
01365> TIME TO PEAK (hrs) = 1.567
01366> RUNOFF VOLUME (mm) = 12.861
01367> TOTAL RAINFALL (mm) = 44.186
01368> RUNOFF COEFFICIENT = .291
01369>
01370> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01371>
-----
01372> 005:0019-----
01373>
01374>
01375> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01376> (ha) (cms) (hrs) (mm) (cms)
01377> ID1 01:300 10.33 1.183 1.10 30.94 .000
01378> +ID2 02:302 4.18 .621 1.02 30.94 .000
01379> +ID3 03:301 4.37 .122 1.57 12.86 .000
01380>
01381> SUM 04:Pond3In 18.88 1.715 1.08 26.76 .000
01382>
01383> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01384>
-----
01385> 005:0020-----
01386>
01387>
01388> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01389> | IN>04:(Pond31) |
01390> | OUT<07:(Pond3 ) |
===== OUTFLOW STORAGE TABLE =====
01391> OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
01392> .000 .0000E+00 | 1.400 .5800E+00
01393> .310 .2500E+00 | .000 .0000E+00
01394>
01395>
ROUTING RESULTS AREA QPEAK TPEAK R.V.
01396> (ha) (cms) (hrs) (mm)
01397>

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01398> INFLOW >04: (Pond31) 18.88 1.715 1.083 26.758
01399> OUTFLOW<07: (Pond3 ) 18.88 .434 1.950 26.758
01400>
01401>
01402> PEAK FLOW REDUCTION [Qout/Qin] (%) = 25.322
01403> TIME SHIFT OF PEAK FLOW (min) = 52.00
01404> MAXIMUM STORAGE USED (ha.m.) = .2876E+00
01405>
-----
01406> 005:0021-----
01407> *#*****
01408> *#
01409> *# Pond 4 Sizing, Cas 400, 401 and 402
01410> *#
01411> *#*****
01412>
01413> | CALIB STANDHYD | Area (ha) = 10.47
01414> | 01:402 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01415>
01416> IMPERVIOUS PERVIOUS (i)
01417> Surface Area (ha) = 5.76 4.71
01418> Dep. Storage (mm) = 2.00 5.00
01419> Average Slope (%) = 1.00 1.00
01420> Length (m) = 350.00 40.00
01421> Mannings n = .013 .240
01422>
01423> Max.eff.Inten.(mm/hr) = 141.24 50.53
01424> over (min) = 5.00 16.00
01425> Storage Coeff. (min) = 4.72 (ii) 15.86 (ii)
01426> Unit Hyd. Tpeak (min) = 5.00 16.00
01427> Unit Hyd. peak (cms) = .23 .07
01428>
01429> PEAK FLOW (cms) = 1.27 .39 *#TOTALS*
01430> TIME TO PEAK (hrs) = 1.05 1.30 1.050
01431> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01432> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01433> RUNOFF COEFFICIENT = .95 .49 .700
01434>
01435> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01436> CN* = 86.0 Ia = Dep. Storage (Above)
01437> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01438> THAN THE STORAGE COEFFICIENT.
01439> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01440>
-----
01441> 005:0022-----
01442>
01443> | CALIB STANDHYD | Area (ha) = 3.22
01444> | 02:401 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01445>
01446> IMPERVIOUS PERVIOUS (i)
01447> Surface Area (ha) = 1.77 1.45
01448> Dep. Storage (mm) = 2.00 5.00
01449> Average Slope (%) = 1.00 1.00
01450> Length (m) = 250.00 40.00
01451> Mannings n = .013 .240
01452>
01453> Max.eff.Inten.(mm/hr) = 141.24 52.52
01454> over (min) = 4.00 15.00
01455> Storage Coeff. (min) = 3.86 (ii) 14.83 (ii)
01456> Unit Hyd. Tpeak (min) = 4.00 15.00
01457> Unit Hyd. peak (cms) = .29 .08
01458>
01459> *#*****
01460> PEAK FLOW (cms) = .42 .12 1.457 (iii)
01461> TIME TO PEAK (hrs) = 1.03 1.28 1.033
01462> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01463> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01464> RUNOFF COEFFICIENT = .95 .49 .700
01465>
01466> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01467> CN* = 86.0 Ia = Dep. Storage (Above)
01468> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01469> THAN THE STORAGE COEFFICIENT.
01470> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01471>
-----
01472> 005:0023-----
01473>
01474>
01475> | CALIB STANDHYD | Area (ha) = 5.25
01476> | 03:400 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01477>
01478> IMPERVIOUS PERVIOUS (i)
01479> Surface Area (ha) = 2.89 2.36
01480> Dep. Storage (mm) = 2.00 5.00
01481> Average Slope (%) = 1.00 1.00
01482> Length (m) = 250.00 40.00
01483> Mannings n = .013 .240
01484>
01485> Max.eff.Inten.(mm/hr) = 141.24 52.52
01486> over (min) = 4.00 15.00
01487> Storage Coeff. (min) = 3.86 (ii) 14.83 (ii)
01488> Unit Hyd. Tpeak (min) = 4.00 15.00
01489> Unit Hyd. peak (cms) = .29 .08
01490>
01491> *#*****
01492> PEAK FLOW (cms) = .69 .20 1.745 (iii)
01493> TIME TO PEAK (hrs) = 1.03 1.28 1.033
01494> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01495> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01496> RUNOFF COEFFICIENT = .95 .49 .700
01497>
01498> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01499> CN* = 86.0 Ia = Dep. Storage (Above)
01500> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01501> THAN THE STORAGE COEFFICIENT.
01502> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01503>
-----
01504> 005:0024-----
01505>
01506> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01507> (ha) (cms) (hrs) (mm) (cms)
01508> ID1 01:402 10.47 1.386 1.05 30.94 .000
01509> +ID2 02:401 3.22 .457 1.03 30.94 .000
01510> +ID3 03:400 5.25 .745 1.03 30.94 .000
01511>
01512> SUM 04:Pond4In 18.94 2.568 1.05 30.94 .000
01513>
01514> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01515>
-----
01516> 005:0025-----
01517>
01518>
01519> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01520> | IN>04:(Pond41) |
01521> | OUT<06:(Pond4 ) |
===== OUTFLOW STORAGE TABLE =====
01522> OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
01523> .000 .0000E+00 | 1.400 .7000E+00
01524>

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01525> .310 .3000E+00 | .000 .0000E+00
01526>
01527> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01528> (ha) (cms) (hrs) (mm)
01529> INFLOW >04: (Pond4I) 18.94 2.568 1.050 30.944
01530> OUTFLOW>06: (Pond4) 18.94 .472 1.867 30.944
01531>
01532> PEAK FLOW REDUCTION [Qout/Qin] (%) = 18.372
01533> TIME SHIFT OF PEAK FLOW (min) = 49.00
01534> MAXIMUM STORAGE USED (ha.m.) = .3594E+00
01535>
-----
01537> 005:0026-----
01538> *#*****
01539> *#
01540> *# Pond 5 Sizing, Cas 500, 501 and 502
01541> *#
01542> *#*****
01543>
01544> | CALIB STANDHYD | Area (ha) = 2.93
01545> | 01:501 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01546>
-----
01547> IMPERVIOUS PERVIOUS (i)
01548> Surface Area (ha) = 1.61 1.32
01549> Dep. Storage (mm) = 2.00 5.00
01550> Average Slope (%) = 1.00 1.00
01551> Length (m) = 250.00 40.00
01552> Mannings n = .013 .240
01553>
01554> Max.eff.Inten.(mm/hr) = 141.24 52.52
01555> over (min) = 4.00 15.00
01556> Storage Coeff. (min) = 3.86 (ii) 14.83 (ii)
01557> Unit Hyd. Tpeak (min) = 4.00 15.00
01558> Unit Hyd. peak (cms) = .29 .08
01559>
01560> *TOTALS*
01561> PEAK FLOW (cms) = .39 .11 .416 (iii)
01562> TIME TO PEAK (hrs) = 1.03 1.28 1.033
01563> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01564> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01565> RUNOFF COEFFICIENT = .95 .49 .700
01566>
01567> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01568> CN* = 86.0 Ia = Dep. Storage (Above)
01569> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01570> THAN THE STORAGE COEFFICIENT.
01571> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01572>
-----
01573> 005:0027-----
01574>
01575> | CALIB STANDHYD | Area (ha) = 3.14
01576> | 02:500 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01577>
-----
01578> IMPERVIOUS PERVIOUS (i)
01579> Surface Area (ha) = 1.73 1.41
01580> Dep. Storage (mm) = 2.00 5.00
01581> Average Slope (%) = 1.00 1.00
01582> Length (m) = 250.00 40.00
01583> Mannings n = .013 .240
01584>
01585> Max.eff.Inten.(mm/hr) = 141.24 52.52
01586> over (min) = 4.00 15.00
01587> Storage Coeff. (min) = 3.86 (ii) 14.83 (ii)
01588> Unit Hyd. Tpeak (min) = 4.00 15.00
01589> Unit Hyd. peak (cms) = .29 .08
01590>
01591> *TOTALS*
01592> PEAK FLOW (cms) = .41 .12 .446 (iii)
01593> TIME TO PEAK (hrs) = 1.03 1.28 1.033
01594> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01595> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01596> RUNOFF COEFFICIENT = .95 .49 .700
01597>
01598> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01599> CN* = 86.0 Ia = Dep. Storage (Above)
01600> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01601> THAN THE STORAGE COEFFICIENT.
01602> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01603>
-----
01604> 005:0028-----
01605>
01606> | CALIB STANDHYD | Area (ha) = 5.45
01607> | 03:502 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01608>
-----
01609> IMPERVIOUS PERVIOUS (i)
01610> Surface Area (ha) = 3.00 2.45
01611> Dep. Storage (mm) = 2.00 5.00
01612> Average Slope (%) = 1.00 1.00
01613> Length (m) = 600.00 40.00
01614> Mannings n = .013 .240
01615>
01616> Max.eff.Inten.(mm/hr) = 119.53 47.22
01617> over (min) = 7.00 18.00
01618> Storage Coeff. (min) = 6.97 (ii) 18.42 (ii)
01619> Unit Hyd. Tpeak (min) = 7.00 18.00
01620> Unit Hyd. peak (cms) = .16 .06
01621>
01622> *TOTALS*
01623> PEAK FLOW (cms) = .56 .19 .632 (iii)
01624> TIME TO PEAK (hrs) = 1.08 1.33 1.100
01625> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01626> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01627> RUNOFF COEFFICIENT = .95 .49 .700
01628>
01629> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01630> CN* = 86.0 Ia = Dep. Storage (Above)
01631> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01632> THAN THE STORAGE COEFFICIENT.
01633> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01634>
-----
01635> 005:0029-----
01636>
01637> | ADD HYD (Pond5In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01638> (ha) (cms) (hrs) (mm) (cms)
01639> ID1 01:501 2.93 .416 1.03 30.94 .000
01640> +ID2 02:500 3.14 .446 1.03 30.94 .000
01641> +ID3 03:502 5.45 .632 1.10 30.94 .000
01642>
01643> SUM 04:Pond5In 11.52 1.421 1.05 30.94 .000
01644>
01645> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01646>
-----
01647>
01648> 005:0030-----
01649>
01650> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01651> | IN>04: (Pond5I) |

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01652> | OUT<05: (Pond5 ) | ===== OUTFLOW STORAGE TABLE =====
01653> OUTFLOW STORAGE | OUTFLOW STORAGE
01654> (cms) (ha.m.) | (cms) (ha.m.)
01655> .000 .000E+00 | .850 .500E+00
01656> .190 .2300E+00 | .000 .0000E+00
01657>
01658> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01659> (ha) (cms) (hrs) (mm)
01660> INFLOW >04: (Pond5I) 11.52 1.421 1.050 30.944
01661> OUTFLOW<05: (Pond5) 11.52 .210 2.117 30.944
01662>
01663> PEAK FLOW REDUCTION [Qout/Qin] (%) = 14.770
01664> TIME SHIFT OF PEAK FLOW (min) = 64.00
01665> MAXIMUM STORAGE USED (ha.m.) = .2381E+00
01666>
-----
01667>
01668> 005:0031-----
01669> *#*****
01670> *#
01671> *# EXT3 Sizing, Cas EXT3
01672> *#
01673> *#*****
01674>
01675> | CALIB STANDHYD | Area (ha) = 9.16
01676> | 01:EXT3 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
01677>
-----
01678> IMPERVIOUS PERVIOUS (i)
01679> Surface Area (ha) = 5.04 4.12
01680> Dep. Storage (mm) = 2.00 5.00
01681> Average Slope (%) = 1.00 1.00
01682> Length (m) = 400.00 40.00
01683> Mannings n = .013 .240
01684>
01685> Max.eff.Inten.(mm/hr) = 141.24 50.53
01686> over (min) = 5.00 16.00
01687> Storage Coeff. (min) = 5.11 (ii) 16.25 (ii)
01688> Unit Hyd. Tpeak (min) = 5.00 16.00
01689> Unit Hyd. peak (cms) = .22 .07
01690>
01691> *TOTALS*
01692> PEAK FLOW (cms) = 1.08 .34 1.182 (iii)
01693> TIME TO PEAK (hrs) = 1.05 1.30 1.050
01694> RUNOFF VOLUME (mm) = 42.19 21.75 30.944
01695> TOTAL RAINFALL (mm) = 44.19 44.19 44.186
01696> RUNOFF COEFFICIENT = .95 .49 .700
01697>
01698> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01699> CN* = 86.0 Ia = Dep. Storage (Above)
01700> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01701> THAN THE STORAGE COEFFICIENT.
01702> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01703>
-----
01704> 005:0032-----
01705>
01706> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
01707> | TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
01708> | | Total minor system capacity = .150 (cms)
01709> | | Total major system storage [TMJSTO] = 5000.(cu.m.)
01710>
01711> ID: NHYD AREA QPEAK TPEAK R.V. DWF
01712> (ha) (cms) (hrs) (mm) (cms)
01713> TOTAL HYD. 01:EXT3 9.16 1.182 1.050 30.944 .000
01714>
01715> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
01716> MINOR SYST 03:MinorE 9.16 .150 .817 31.036 .000
01717>
01718> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01719>
01720> Maximum MAJOR SYSTEM storage used = 1634.(cu.m.)
01721>
01722>
-----
01723> 005:0033-----
01724> *#*****
01725> *#
01726> *# Flow Totals and Channel Runoff
01727> *#
01728> *#*****
01729>
01730> | ADD HYD (Control ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01731> (ha) (cms) (hrs) (mm) (cms)
01732> ID1 02:noFlow .00 .000 .000 .00 .000
01733> +ID2 03:MinorEXT3 9.16 .150 .82 31.04 .000
01734> +ID3 05:Pond5 11.52 .210 2.12 30.94 .000
01735> +ID4 06:Pond4 18.94 .472 1.87 30.94 .000
01736> +ID5 07:Pond3 18.88 .434 1.95 26.76 .000
01737> +ID6 08:Pond2 7.53 .137 2.15 30.94 .000
01738> +ID7 09:Pond1 4.08 .088 1.95 30.94 .000
01739> +ID8 10:ExPond 32.50 .869 1.90 30.94 .000
01740>
01741> SUM 01:Control 102.61 2.348 1.95 30.18 .000
01742>
01743> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01744>
01745>
-----
01746> 005:0034-----
01747>
01748> | CALIB NASHYD | Area (ha) = .99 Curve Number (CN)=68.00
01749> | 02:600 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res. (N) = 3.00
01750> | U.H. Tp(hrs) = .350
01751>
01752> Unit Hyd Qpeak (cms) = .108
01753>
01754> PEAK FLOW (cms) = .023 (i)
01755> TIME TO PEAK (hrs) = 1.483
01756> RUNOFF VOLUME (mm) = 9.674
01757> TOTAL RAINFALL (mm) = 44.186
01758> RUNOFF COEFFICIENT = .219
01759>
01760> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01761>
01762>
-----
01763> 005:0035-----
01764>
01765> | CALIB NASHYD | Area (ha) = 3.54 Curve Number (CN)=68.00
01766> | 03:601 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res. (N) = 3.00
01767> | U.H. Tp(hrs) = .590
01768>
01769> Unit Hyd Qpeak (cms) = .229
01770>
01771> PEAK FLOW (cms) = .058 (i)
01772> TIME TO PEAK (hrs) = 1.817
01773> RUNOFF VOLUME (mm) = 9.675
01774> TOTAL RAINFALL (mm) = 44.186
01775> RUNOFF COEFFICIENT = .219
01776>
01777> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01778>

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01779> 005:0036-----
01780> CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
01781> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01782> | U.H. Tp(hrs)= .970
01783>
01784> Unit Hyd Qpeak (cms)= .142
01785>
01786> PEAK FLOW (cms)= .042 (i)
01787> TIME TO PEAK (hrs)= 2.317
01788> RUNOFF VOLUME (mm)= 9.675
01789> TOTAL RAINFALL (mm)= 44.186
01790> RUNOFF COEFFICIENT = .219
01791>
01792> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01793>
01794>
01795>
01796> 005:0037-----
01797> ADD HYD (PostTot ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01798> | (ha) (cms) (hrs) (mm) (cms)
01799> | ID1 01:Control 102.61 2.348 1.95 30.18 .000
01800> | +ID2 02:600 .99 .023 1.48 9.67 .000
01801> | ID3 03:601 3.54 0.58 1.82 9.67 .000
01802> | +ID4 04:602 3.61 .042 2.32 9.67 .000
01803>
01804> SUM 05:PostTot 110.75 2.456 1.95 28.67 .000
01805>
01806>
01807> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01808>
01809>
01810>
01811> 005:0038-----
01812>
01813> 005:0002-----
01814> ** END OF RUN : 9
01815>
01816>
01817>
01818>
01819>
01820>
01821>
01822>
01823> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
01824> | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
01825> | TZERO = .00 hrs on 0
01826> | METOUT= 2 (output = METRIC)
01827> | NRUN = 010
01828> | NSTORM= 1
01829> | # 1=ldn10YR.3hr
01830>
01831> 010:0002-----
01832>
01833> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
01834> *# Date : 2022-11-14
01835> *# Modeller : [AKK]
01836> *# Company : Stantec Consulting Ltd. (London)
01837> *# License # : 4730904
01838> *#
01839> *#
01840> *#
01841> *# This model represents the hydrologic characteristics of the existing and
01842> *# proposed conditions in the proposed subdivision.
01843> *# Storm events modeled are:
01844> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
01845> *#
01846> *#
01847>
01848> 010:0002-----
01849>
01850> | READ STORM | Filename: 10-yr, 3hr Chicago Storm from London IDF
01851> | Ptotal= 52.05 mm | Comments: 10-yr, 3hr Chicago Storm from London IDF
01852>
01853>
01854> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01855> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01856> .08 3.462 | .83 25.620 | 1.58 11.888 | 2.33 4.796
01857> .17 8.833 | .92 61.474 | 1.67 10.245 | 2.42 4.496
01858> .25 4.297 | 1.00 162.470 | 1.75 8.987 | 2.50 4.231
01859> .33 4.891 | 1.08 79.139 | 1.83 7.997 | 2.58 3.997
01860> .42 5.677 | 1.17 44.600 | 1.92 7.200 | 2.67 3.788
01861> .50 6.765 | 1.25 29.885 | 2.00 6.545 | 2.75 3.600
01862> .58 8.360 | 1.33 22.041 | 2.08 5.998 | 2.83 3.430
01863> .67 10.895 | 1.42 17.275 | 2.17 5.535 | 2.92 3.276
01864> .75 15.461 | 1.50 14.115 | 2.25 5.139 | 3.00 3.135
01865>
01866> 010:0003-----
01867>
01868> *#
01869> *# Existing Conditions to determine target release rates
01870> *#
01871> *#
01872>
01873> | CALIB NASHYD | Area (ha)= 49.50 Curve Number (CN)=84.00
01874> | 01:S101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01875> | U.H. Tp(hrs)= .840
01876>
01877> Unit Hyd Qpeak (cms)= 2.251
01878>
01879> PEAK FLOW (cms)= 1.577 (i)
01880> TIME TO PEAK (hrs)= 2.083
01881> RUNOFF VOLUME (mm)= 23.193
01882> TOTAL RAINFALL (mm)= 52.045
01883> RUNOFF COEFFICIENT = .446
01884>
01885> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01886>
01887>
01888> 010:0004-----
01889>
01890> | CALIB NASHYD | Area (ha)= 32.80 Curve Number (CN)=84.00
01891> | 02:S102 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01892> | U.H. Tp(hrs)= .620
01893>
01894> Unit Hyd Qpeak (cms)= 2.021
01895>
01896> PEAK FLOW (cms)= 1.306 (i)
01897> TIME TO PEAK (hrs)= 1.817
01898> RUNOFF VOLUME (mm)= 23.193
01899> TOTAL RAINFALL (mm)= 52.045
01900> RUNOFF COEFFICIENT = .446
01901>
01902> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01903>
01904>
01905> 010:0005-----

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01906>
01907> CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
01908> | 03:S103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01909> | U.H. Tp(hrs)= .480
01910>
01911> Unit Hyd Qpeak (cms)= .708
01912>
01913> PEAK FLOW (cms)= .425 (i)
01914> TIME TO PEAK (hrs)= 1.633
01915> RUNOFF VOLUME (mm)= 23.193
01916> TOTAL RAINFALL (mm)= 52.045
01917> RUNOFF COEFFICIENT = .446
01918>
01919> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01920>
01921>
01922> 010:0006-----
01923>
01924> | CALIB NASHYD | Area (ha)= 33.50 Curve Number (CN)=84.00
01925> | 04:S104 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
01926> | U.H. Tp(hrs)= .720
01927>
01928> Unit Hyd Qpeak (cms)= 1.777
01929>
01930> PEAK FLOW (cms)= 1.196 (i)
01931> TIME TO PEAK (hrs)= 1.933
01932> RUNOFF VOLUME (mm)= 23.193
01933> TOTAL RAINFALL (mm)= 52.045
01934> RUNOFF COEFFICIENT = .446
01935>
01936> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01937>
01938>
01939> 010:0007-----
01940>
01941> | ADD HYD (Total ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
01942> | (ha) (cms) (hrs) (mm) (cms)
01943> | ID1 01:S101 49.50 1.577 2.08 23.19 .000
01944> | +ID2 02:S102 32.80 1.306 1.82 23.19 .000
01945> | +ID3 03:S103 8.90 .425 1.63 23.19 .000
01946> | +ID4 04:S104 33.50 1.196 1.93 23.19 .000
01947>
01948> SUM 05:Total 124.70 4.383 1.92 23.19 .000
01949>
01950> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01951>
01952>
01953> 010:0008-----
01954> *#
01955> *#
01956> *# External Pond Sizing, CAS EXT1 and EXT2
01957> *#
01958> *#
01959>
01960> | CALIB STANDHYD | Area (ha)= 9.50
01961> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01962>
01963> IMPERVIOUS PERVIOUS (i)
01964> Surface Area (ha)= 5.22 4.27
01965> Dep. Storage (mm)= 2.00 5.00
01966> Average Slope (%)= 1.00 1.00
01967> Length (m)= 400.00 40.00
01968> Mannings n = .013 .240
01969>
01970> Max.eff.Inten.(mm/hr)= 162.47 68.91
01971> over (min)= 5.00 15.00
01972> Storage Coeff. (min)= 4.83 (ii) 14.67 (ii)
01973> Unit Hyd. Tpeak (min)= 5.00 15.00
01974> Unit Hyd. peak (cms)= .23 .08
01975>
01976> PEAK FLOW (cms)= 1.33 .49 *TOTALS*
01977> TIME TO PEAK (hrs)= 1.05 1.27 1.506 (iii)
01978> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
01979> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
01980> RUNOFF COEFFICIENT = .96 .54 .730
01981>
01982> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
01983> CN* = 86.0 Ia = Dep. Storage (Above)
01984> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01985> THAN THE STORAGE COEFFICIENT.
01986> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01987>
01988>
01989> 010:0009-----
01990>
01991> | CALIB STANDHYD | Area (ha)= 23.00
01992> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
01993>
01994> IMPERVIOUS PERVIOUS (i)
01995> Surface Area (ha)= 12.65 10.35
01996> Dep. Storage (mm)= 2.00 5.00
01997> Average Slope (%)= 1.00 1.00
01998> Length (m)= 750.00 40.00
01999> Mannings n = .013 .240
02000>
02001> Max.eff.Inten.(mm/hr)= 131.22 61.96
02002> over (min)= 8.00 18.00
02003> Storage Coeff. (min)= 7.68 (ii) 17.95 (ii)
02004> Unit Hyd. Tpeak (min)= 8.00 18.00
02005> Unit Hyd. peak (cms)= .15 .06
02006>
02007> PEAK FLOW (cms)= 2.65 1.05 3.134 (iii)
02008> TIME TO PEAK (hrs)= 1.10 1.33 1.117
02009> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02010> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02011> RUNOFF COEFFICIENT = .96 .54 .730
02012>
02013> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02014> CN* = 86.0 Ia = Dep. Storage (Above)
02015> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02016> THAN THE STORAGE COEFFICIENT.
02017> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02018>
02019>
02020> 010:0010-----
02021>
02022> | ADD HYD (ExPondIn ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02023> | (ha) (cms) (hrs) (mm) (cms)
02024> | ID1 01:EXT2 9.50 1.506 1.07 37.99 .000
02025> | +ID2 02:EXT1 23.00 3.134 1.12 37.99 .000
02026>
02027> SUM 03:ExPondIn 32.50 4.537 1.12 37.99 .000
02028>
02029> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02030>
02031>
02032> 010:0011-----

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02033>-----
02034> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02035> | IN>03:(EkPond) |
02036> | OUT<09:(ExPond) |
02037>-----
02038> | OUTFLOW STORAGE | OUTFLOW STORAGE
02039> | (cms) (ha.m.) | (cms) (ha.m.)
02040> | .000 .0000E+00 | 2.420 .1200E+01
02041> | .530 .4500E+00 | .000 .0000E+00
02042>-----
02043> | ROUTING RESULTS | AREA QPEAK TPEAK R.V.
02044> | (ha) (cms) (hrs) (mm)
02045> | INFLOW >03: (EkPond) 32.50 4.537 1.117 37.985
02046> | OUTFLOW<10: (ExPond) 32.50 1.183 1.817 37.985
02047>-----
02048> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 26.086
02049> | TIME SHIFT OF PEAK FLOW (min) = 42.00
02050> | MAXIMUM STORAGE USED (ha.m.) = 7.093E+00
02051>-----
02052> 010:0012-----
02053> *#-----
02054> *#
02055> *# Pond 1 Sizing, Cas 100
02056> *#
02057> *#-----
02058>-----
02059> | CALIB STANDHYD | Area (ha) = 4.08
02060> | 01:100 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
02061>-----
02062> | IMPERVIOUS PERVIOUS (i)
02063> | Surface Area (ha) = 2.24 1.84
02064> | Dep. Storage (mm) = 2.00 5.00
02065> | Average Slope (%) = 1.00 1.00
02066> | Length (m) = 300.00 40.00
02067> | Mannings n = .013 .240
02068>-----
02069> | Max.eff.Inten.(mm/hr) = 162.47 70.97
02070> | over (min) 4.00 14.00
02071> | Storage Coeff. (min) = 4.07 (ii) 13.79 (ii)
02072> | Unit Hyd. Tpeak (min) = 4.00 14.00
02073> | Unit Hyd. peak (cms) = .28 .08
02074>-----
02075> | PEAK FLOW (cms) = .61 .22 .683 (iii)
02076> | TIME TO PEAK (hrs) = 1.03 1.25 1.033
02077> | RUNOFF VOLUME (mm) = 50.04 28.12 37.985
02078> | TOTAL RAINFALL (mm) = 52.05 52.05 52.045
02079> | RUNOFF COEFFICIENT = .96 .54 .730
02080>-----
02081> | (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02082> | CN* = 86.0 Ia = Dep. Storage (Above)
02083> | (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02084> | THAN THE STORAGE COEFFICIENT.
02085> | (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02086>-----
02087>-----
02088> 010:0013-----
02089> *#-----
02090> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02091> | IN>01:(100 ) |
02092> | OUT<09:(Pond1 ) |
02093>-----
02094> | OUTFLOW STORAGE | OUTFLOW STORAGE
02095> | (cms) (ha.m.) | (cms) (ha.m.)
02096> | .000 .0000E+00 | .300 .2000E+00
02097> | .070 .7000E+01 | .000 .0000E+00
02098>-----
02099> | ROUTING RESULTS | AREA QPEAK TPEAK R.V.
02100> | (ha) (cms) (hrs) (mm)
02101> | INFLOW >01: (100 ) 4.08 .683 1.033 37.985
02102> | OUTFLOW<09: (Pond1 ) 4.08 .119 1.850 37.985
02103>-----
02104> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 17.460
02105> | TIME SHIFT OF PEAK FLOW (min) = 49.00
02106> | MAXIMUM STORAGE USED (ha.m.) = 9.784E-01
02107>-----
02108> 010:0014-----
02109> *#-----
02110> *#
02111> *# Pond 2 Sizing, Cas 200
02112> *#
02113> *#-----
02114>-----
02115> | CALIB STANDHYD | Area (ha) = 7.53
02116> | 01:200 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
02117>-----
02118> | IMPERVIOUS PERVIOUS (i)
02119> | Surface Area (ha) = 4.14 3.39
02120> | Dep. Storage (mm) = 2.00 5.00
02121> | Average Slope (%) = 1.00 1.00
02122> | Length (m) = 550.00 40.00
02123> | Mannings n = .013 .240
02124>-----
02125> | Max.eff.Inten.(mm/hr) = 148.58 66.30
02126> | over (min) 6.00 16.00
02127> | Storage Coeff. (min) = 6.06 (ii) 16.06 (ii)
02128> | Unit Hyd. Tpeak (min) = 6.00 16.00
02129> | Unit Hyd. peak (cms) = .19 .07
02130>-----
02131> | PEAK FLOW (cms) = .96 .37 .1117 (iii)
02132> | TIME TO PEAK (hrs) = 1.07 1.30 1.083
02133> | RUNOFF VOLUME (mm) = 50.04 28.12 37.985
02134> | TOTAL RAINFALL (mm) = 52.05 52.05 52.045
02135> | RUNOFF COEFFICIENT = .96 .54 .730
02136>-----
02137> | (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02138> | CN* = 86.0 Ia = Dep. Storage (Above)
02139> | (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02140> | THAN THE STORAGE COEFFICIENT.
02141> | (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02142>-----
02143>-----
02144> 010:0015-----
02145> *#-----
02146> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02147> | IN>01:(200 ) |
02148> | OUT<08:(Pond2 ) |
02149>-----
02150> | OUTFLOW STORAGE | OUTFLOW STORAGE
02151> | (cms) (ha.m.) | (cms) (ha.m.)
02152> | .000 .0000E+00 | .560 .3000E+00
02153> | .120 .1500E+00 | .000 .0000E+00
02154>-----
02155> | ROUTING RESULTS | AREA QPEAK TPEAK R.V.
02156> | (ha) (cms) (hrs) (mm)
02157> | INFLOW >01: (200 ) 7.53 1.117 1.083 37.985
02158> | OUTFLOW<08: (Pond2 ) 7.53 .220 1.917 37.985
02159>-----
02160> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 19.718

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02160>-----
02161> | TIME SHIFT OF PEAK FLOW (min) = 50.00
02162> | MAXIMUM STORAGE USED (ha.m.) = 1.842E+00
02163>-----
02164> 010:0016-----
02165> *#-----
02166> *#
02167> *# Pond 3 Sizing, Cas 300, 301 and 302
02168> *#
02169> *#-----
02170>-----
02171> | CALIB STANDHYD | Area (ha) = 10.33
02172> | 01:300 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
02173>-----
02174> | IMPERVIOUS PERVIOUS (i)
02175> | Surface Area (ha) = 5.68 4.65
02176> | Dep. Storage (mm) = 2.00 5.00
02177> | Average Slope (%) = 1.00 1.00
02178> | Length (m) = 610.00 40.00
02179> | Mannings n = .013 .240
02180>-----
02181> | Max.eff.Inten.(mm/hr) = 138.66 63.99
02182> | over (min) 7.00 17.00
02183> | Storage Coeff. (min) = 6.63 (ii) 16.77 (ii)
02184> | Unit Hyd. Tpeak (min) = 7.00 17.00
02185> | Unit Hyd. peak (cms) = .17 .07
02186>-----
02187> | PEAK FLOW (cms) = 1.27 .49 1.483 (iii)
02188> | TIME TO PEAK (hrs) = 1.08 1.32 1.100
02189> | RUNOFF VOLUME (mm) = 50.04 28.12 37.985
02190> | TOTAL RAINFALL (mm) = 52.05 52.05 52.045
02191> | RUNOFF COEFFICIENT = .96 .54 .730
02192>-----
02193> | (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02194> | CN* = 86.0 Ia = Dep. Storage (Above)
02195> | (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02196> | THAN THE STORAGE COEFFICIENT.
02197> | (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02198>-----
02199>-----
02200> 010:0017-----
02201> *#-----
02202> | CALIB STANDHYD | Area (ha) = 4.18
02203> | 02:302 DT= 1.00 | Total Imp (%) = 55.00 Dir. Conn. (%) = 45.00
02204>-----
02205> | IMPERVIOUS PERVIOUS (i)
02206> | Surface Area (ha) = 2.30 1.88
02207> | Dep. Storage (mm) = 2.00 5.00
02208> | Average Slope (%) = 1.00 1.00
02209> | Length (m) = 210.00 40.00
02210> | Mannings n = .013 .240
02211>-----
02212> | Max.eff.Inten.(mm/hr) = 162.47 73.37
02213> | over (min) 3.00 13.00
02214> | Storage Coeff. (min) = 3.28 (ii) 12.88 (ii)
02215> | Unit Hyd. Tpeak (min) = 3.00 13.00
02216> | Unit Hyd. peak (cms) = .35 .09
02217>-----
02218> | PEAK FLOW (cms) = .68 .23 .750 (iii)
02219> | TIME TO PEAK (hrs) = 1.02 1.23 1.017
02220> | RUNOFF VOLUME (mm) = 50.04 28.12 37.985
02221> | TOTAL RAINFALL (mm) = 52.05 52.05 52.045
02222> | RUNOFF COEFFICIENT = .96 .54 .730
02223>-----
02224> | (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02225> | CN* = 86.0 Ia = Dep. Storage (Above)
02226> | (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02227> | THAN THE STORAGE COEFFICIENT.
02228> | (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02229>-----
02230>-----
02231> 010:0018-----
02232> *#-----
02233> | CALIB NASHYD | Area (ha) = 4.37 Curve Number (CN)=76.00
02234> | 03:301 DT= 1.00 | Ia (mm) = 5.000 # of Linear Res. (N) = 3.00
02235> | U.H. Tp (hrs) = .410
02236>-----
02237> | Unit Hyd Qpeak (cms) = .407
02238>-----
02239> | PEAK FLOW (cms) = .170 (i)
02240> | TIME TO PEAK (hrs) = 1.550
02241> | RUNOFF VOLUME (mm) = 17.392
02242> | TOTAL RAINFALL (mm) = 52.045
02243> | RUNOFF COEFFICIENT = .334
02244>-----
02245> | (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02246>-----
02247>-----
02248> 010:0019-----
02249> *#-----
02250> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DMF
02251> | Id1 01:300 10.33 1.483 1.10 37.99 .000
02252> | +ID2 02:302 4.18 .750 1.02 37.99 .000
02253> | +ID3 03:301 4.37 .170 1.55 17.39 .000
02254>-----
02255> | SUM 04:Pond3In 18.88 2.148 1.10 33.22 .000
02256>-----
02257>-----
02258> | NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02259>-----
02260>-----
02261> 010:0020-----
02262> *#-----
02263> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02264> | IN>04:(Pond3I) |
02265> | OUT<07:(Pond3 ) |
02266>-----
02267> | OUTFLOW STORAGE | OUTFLOW STORAGE
02268> | (cms) (ha.m.) | (cms) (ha.m.)
02269> | .000 .0000E+00 | 1.400 .5800E+00
02270> | .310 .2500E+00 | .000 .0000E+00
02271>-----
02272> | ROUTING RESULTS | AREA QPEAK TPEAK R.V.
02273> | (ha) (cms) (hrs) (mm)
02274> | INFLOW >04: (Pond3I) 18.88 2.148 1.100 33.219
02275> | OUTFLOW<07: (Pond3 ) 18.88 .624 1.833 33.219
02276>-----
02277> | PEAK FLOW REDUCTION [Qout/Qin] (%) = 29.054
02278> | TIME SHIFT OF PEAK FLOW (min) = 44.00
02279> | MAXIMUM STORAGE USED (ha.m.) = .3451E+00
02280>-----
02281> 010:0021-----
02282> *#-----
02283> *#
02284> *# Pond 4 Sizing, Cas 400, 401 and 402
02285> *#
02286> *#-----

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02287> -----
02288> | CALIB STANDHYD | Area (ha)= 10.47
02289> | 01:402 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02290> -----
02291> IMPERVIOUS PERVIOUS (i)
02292> Surface Area (ha)= 5.76 4.71
02293> Dep. Storage (mm)= 2.00 5.00
02294> Average Slope (%)= 1.00 1.00
02295> Length (m)= 350.00 40.00
02296> Mannings n = .013 .240
02297> -----
02298> Max.eff.Inten.(mm/hr)= 162.47 70.97
02299> over (min) 4.00 14.00
02300> Storage Coeff. (min)= 4.46 (ii) 14.19 (ii)
02301> Unit Hyd. Tpeak (min)= 4.00 14.00
02302> Unit Hyd. peak (cms)= .26 .08
02303> -----
02304> PEAK FLOW (cms)= 1.53 .55 *TOTALS*
02305> TIME TO PEAK (hrs)= 1.03 1.27 1.708 (iii)
02306> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02307> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02308> RUNOFF COEFFICIENT = .96 .54 .730
02309> -----
02310> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02311> CN* = 86.0 Ia = Dep. Storage (Above)
02312> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02313> THAN THE STORAGE COEFFICIENT.
02314> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02315> -----
02316> 010:0022-----
02317> -----
02318> | CALIB STANDHYD | Area (ha)= 3.22
02319> | 02:401 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02320> -----
02321> IMPERVIOUS PERVIOUS (i)
02322> Surface Area (ha)= 1.77 1.45
02323> Dep. Storage (mm)= 2.00 5.00
02324> Average Slope (%)= 1.00 1.00
02325> Length (m)= 250.00 40.00
02326> Mannings n = .013 .240
02327> -----
02328> Max.eff.Inten.(mm/hr)= 162.47 73.37
02329> over (min) 4.00 13.00
02330> Storage Coeff. (min)= 3.65 (ii) 13.24 (ii)
02331> Unit Hyd. Tpeak (min)= 4.00 13.00
02332> Unit Hyd. peak (cms)= .30 .09
02333> -----
02334> PEAK FLOW (cms)= .50 .18 *TOTALS*
02335> TIME TO PEAK (hrs)= 1.03 1.23 1.033
02336> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02337> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02338> RUNOFF COEFFICIENT = .96 .54 .730
02339> -----
02340> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02341> CN* = 86.0 Ia = Dep. Storage (Above)
02342> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02343> THAN THE STORAGE COEFFICIENT.
02344> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02345> -----
02346> 010:0023-----
02347> -----
02348> | CALIB STANDHYD | Area (ha)= 5.25
02349> | 03:400 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02350> -----
02351> IMPERVIOUS PERVIOUS (i)
02352> Surface Area (ha)= 2.89 2.36
02353> Dep. Storage (mm)= 2.00 5.00
02354> Average Slope (%)= 1.00 1.00
02355> Length (m)= 250.00 40.00
02356> Mannings n = .013 .240
02357> -----
02358> Max.eff.Inten.(mm/hr)= 162.47 73.37
02359> over (min) 4.00 13.00
02360> Storage Coeff. (min)= 3.65 (ii) 13.24 (ii)
02361> Unit Hyd. Tpeak (min)= 4.00 13.00
02362> Unit Hyd. peak (cms)= .30 .09
02363> -----
02364> PEAK FLOW (cms)= .82 .29 *TOTALS*
02365> TIME TO PEAK (hrs)= 1.03 1.23 1.033
02366> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02367> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02368> RUNOFF COEFFICIENT = .96 .54 .730
02369> -----
02370> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02371> CN* = 86.0 Ia = Dep. Storage (Above)
02372> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02373> THAN THE STORAGE COEFFICIENT.
02374> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02375> -----
02376> 010:0024-----
02377> -----
02378> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02379> | ID1 01:402 (ha) (cms) (hrs) (mm) (cms)
02380> +ID2 02:401 3.22 .561 1.03 37.99 .000
02381> +ID3 03:400 5.25 .914 1.03 37.99 .000
02382> -----
02383> SUM 04:Pond4In 18.94 3.180 1.03 37.99 .000
02384> -----
02385> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02386> -----
02387> 010:0025-----
02388> -----
02389> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02390> | IN<04:(Pond4I) |
02391> | OUT<06:(Pond4 ) |
02392> ===== OUTFLOW STORAGE TABLE =====
02393> OUTFLOW STORAGE OUTFLOW STORAGE
02394> (cms) (ha.m.) | (cms) (ha.m.)
02395> .000 .0000E+00 | 1.400 .7000E+00
02396> .310 .3000E+00 | .000 .0000E+00
02397> -----
02398> ROUTING RESULTS AREA QPEAK TPEAK R.V.
02399> (ha) (cms) (hrs) (mm)
02400> INFLOW >04: (Pond4I) 18.94 3.180 1.033 37.985
02401> OUTFLOW<06: (Pond4 ) 18.94 .669 1.750 37.985
02402> -----
02403> PEAK FLOW REDUCTION [Qout/Qin] (%) = 21.045
02404> TIME SHIFT OF PEAK FLOW (min) = 43.00
02405> MAXIMUM STORAGE USED (ha.m.) = .4319E+00
02406> -----
02407> -----
02408> -----
02409> -----
02410> -----
02411> -----
02412> 010:0026-----
02413> *-----

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02414> *#
02415> *# Pond 5 Sizing, Cas 500, 501 and 502
02416> *#
02417> -----
02418> -----
02419> | CALIB STANDHYD | Area (ha)= 2.93
02420> | 01:501 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02421> -----
02422> IMPERVIOUS PERVIOUS (i)
02423> Surface Area (ha)= 1.61 1.32
02424> Dep. Storage (mm)= 2.00 5.00
02425> Average Slope (%)= 1.00 1.00
02426> Length (m)= 250.00 40.00
02427> Mannings n = .013 .240
02428> -----
02429> Max.eff.Inten.(mm/hr)= 162.47 73.37
02430> over (min) 4.00 13.00
02431> Storage Coeff. (min)= 3.65 (ii) 13.24 (ii)
02432> Unit Hyd. Tpeak (min)= 4.00 13.00
02433> Unit Hyd. peak (cms)= .30 .09
02434> -----
02435> PEAK FLOW (cms)= .46 .16 *TOTALS*
02436> TIME TO PEAK (hrs)= 1.03 1.23 1.033
02437> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02438> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02439> RUNOFF COEFFICIENT = .96 .54 .730
02440> -----
02441> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02442> CN* = 86.0 Ia = Dep. Storage (Above)
02443> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02444> THAN THE STORAGE COEFFICIENT.
02445> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02446> -----
02447> 010:0027-----
02448> -----
02449> | CALIB STANDHYD | Area (ha)= 3.14
02450> | 02:500 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02451> -----
02452> IMPERVIOUS PERVIOUS (i)
02453> Surface Area (ha)= 1.73 1.41
02454> Dep. Storage (mm)= 2.00 5.00
02455> Average Slope (%)= 1.00 1.00
02456> Length (m)= 250.00 40.00
02457> Mannings n = .013 .240
02458> -----
02459> Max.eff.Inten.(mm/hr)= 162.47 73.37
02460> over (min) 4.00 13.00
02461> Storage Coeff. (min)= 3.65 (ii) 13.24 (ii)
02462> Unit Hyd. Tpeak (min)= 4.00 13.00
02463> Unit Hyd. peak (cms)= .30 .09
02464> -----
02465> PEAK FLOW (cms)= .49 .17 *TOTALS*
02466> TIME TO PEAK (hrs)= 1.03 1.23 1.033
02467> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02468> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02469> RUNOFF COEFFICIENT = .96 .54 .730
02470> -----
02471> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02472> CN* = 86.0 Ia = Dep. Storage (Above)
02473> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02474> THAN THE STORAGE COEFFICIENT.
02475> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02476> -----
02477> 010:0028-----
02478> -----
02479> | CALIB STANDHYD | Area (ha)= 5.45
02480> | 03:502 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02481> -----
02482> IMPERVIOUS PERVIOUS (i)
02483> Surface Area (ha)= 3.00 2.45
02484> Dep. Storage (mm)= 2.00 5.00
02485> Average Slope (%)= 1.00 1.00
02486> Length (m)= 600.00 40.00
02487> Mannings n = .013 .240
02488> -----
02489> Max.eff.Inten.(mm/hr)= 148.58 66.30
02490> over (min) 6.00 16.00
02491> Storage Coeff. (min)= 6.39 (ii) 16.38 (ii)
02492> Unit Hyd. Tpeak (min)= 6.00 16.00
02493> Unit Hyd. peak (cms)= .18 .07
02494> -----
02495> PEAK FLOW (cms)= .68 .26 *TOTALS*
02496> TIME TO PEAK (hrs)= 1.07 1.30 1.083
02497> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02498> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02499> RUNOFF COEFFICIENT = .96 .54 .730
02500> -----
02501> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02502> CN* = 86.0 Ia = Dep. Storage (Above)
02503> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02504> THAN THE STORAGE COEFFICIENT.
02505> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02506> -----
02507> 010:0029-----
02508> -----
02509> | ADD HYD (Pond5In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02510> | ID1 01:501 (ha) (cms) (hrs) (mm) (cms)
02511> +ID2 02:500 2.93 .510 1.03 37.99 .000
02512> +ID3 03:502 5.45 .796 1.08 37.99 .000
02513> -----
02514> SUM 04:Pond5In 11.52 1.800 1.05 37.99 .000
02515> -----
02516> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02517> -----
02518> 010:0030-----
02519> -----
02520> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
02521> | IN<04:(Pond5I) |
02522> | OUT<05:(Pond5 ) |
02523> ===== OUTFLOW STORAGE TABLE =====
02524> OUTFLOW STORAGE OUTFLOW STORAGE
02525> (cms) (ha.m.) | (cms) (ha.m.)
02526> .000 .0000E+00 | 1.850 .5000E+00
02527> .190 .2300E+00 | .000 .0000E+00
02528> -----
02529> ROUTING RESULTS AREA QPEAK TPEAK R.V.
02530> (ha) (cms) (hrs) (mm)
02531> INFLOW >04: (Pond5I) 11.52 1.800 1.050 37.985
02532> OUTFLOW<05: (Pond5 ) 11.52 .323 1.900 37.985
02533> -----
02534> PEAK FLOW REDUCTION [Qout/Qin] (%) = 17.948
02535> TIME SHIFT OF PEAK FLOW (min) = 51.00
02536> MAXIMUM STORAGE USED (ha.m.) = .2845E+00
02537> -----
02538> -----
02539> -----
02540> -----

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02541>
02542>-----
02543> 010:0031-----
02544> *-----
02545> *#
02546> *# EXT3 Sizing, Cas EXT3
02547> *#
02548> *#-----
02549>
02550> | CALIB STANDHYD | Area (ha)= 9.16
02551> | 01:EXT3 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
02552>-----
02553> IMPERVIOUS PERVIOUS (i)
02554> Surface Area (ha)= 5.04 4.12
02555> Dep. Storage (mm)= 2.00 5.00
02556> Average Slope (%)= 1.00 1.00
02557> Length (m)= 400.00 40.00
02558> Mannings n = .013 .240
02559>
02560> Max.eff.Inten.(mm/hr)= 162.47 68.91
02561> over (min) 5.00 15.00
02562> Storage Coeff. (min)= 4.83 (ii) 14.67 (iii)
02563> Unit Hyd. Tpeak (min)= 5.00 15.00
02564> Unit Hyd. peak (cms)= .23 .08
02565>
02566> PEAK FLOW (cms)= 1.28 .47 *TOTALS*
02567> TIME TO PEAK (hrs)= 1.05 1.27 1.452 (iii)
02568> RUNOFF VOLUME (mm)= 50.04 28.12 37.985
02569> TOTAL RAINFALL (mm)= 52.05 52.05 52.045
02570> RUNOFF COEFFICIENT = .96 .54 .730
02571>
02572> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
02573> CN* = 86.0 Ia = Dep. Storage (ABOVE)
02574> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02575> THAN THE STORAGE COEFFICIENT.
02576> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02577>-----
02578>
02579> 010:0032-----
02580>
02581> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
02582> | TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
02583> | | Total minor system capacity = .150 (cms)
02584> | | Total major system storage [TMJSTO] = 5000.(cu.m.)
02585>-----
02586> ID: NHYD AREA QPEAK TPEAK R.V. DWF
02587> (ha) (cms) (hrs) (mm) (cms)
02588> TOTAL HYD. 01:EXT3 9.16 1.452 1.067 37.985 .000
02589>-----
02590> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
02591> MINOR SYST 03:MinorE 9.16 .150 .783 38.072 .000
02592>
02593> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02594>
02595> Maximum MAJOR SYSTEM storage used = 2220.(cu.m.)
02596>
02597>-----
02598> 010:0033-----
02599> *#-----
02600> *#
02601> *# Flow Totals and Channel Runoff
02602> *#-----
02603> *#-----
02604>
02605> | ADD HYD (Control ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02606> (ha) (cms) (hrs) (mm) (cms)
02607> ID1 02:noFlow .00 .000 .00 .00 .000
02608> +ID2 03:MinorEXT3 9.16 .150 .78 38.07 .000
02609> +ID3 05:Pond4 11.52 .323 1.90 37.98 .000
02610> +ID4 06:Pond4 18.94 .669 1.75 37.98 .000
02611> +ID5 07:Pond3 18.88 .624 1.83 32.22 .000
02612> +ID6 08:Pond2 7.53 .220 1.92 37.98 .000
02613> +ID7 09:Pond1 4.08 .119 1.85 37.98 .000
02614> +ID8 10:ExPond 32.50 1.183 1.82 37.99 .000
02615>-----
02616> SUM 01:Control 102.61 3.282 1.83 37.12 .000
02617>
02618> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02619>
02620>-----
02621> 010:0034-----
02622>
02623> | CALIB NASHYD | Area (ha)= .99 Curve Number (CN)=68.00
02624> | 02:600 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02625> | U.H. Tp(hrs)= .350
02626>-----
02627> Unit Hyd Qpeak (cms)= .108
02628>
02629> PEAK FLOW (cms)= .032 (i)
02630> TIME TO PEAK (hrs)= 1.483
02631> RUNOFF VOLUME (mm)= 13.287
02632> TOTAL RAINFALL (mm)= 52.045
02633> RUNOFF COEFFICIENT = .255
02634>
02635> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02636>
02637>-----
02638> 010:0035-----
02639>
02640> | CALIB NASHYD | Area (ha)= 3.54 Curve Number (CN)=68.00
02641> | 03:601 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02642> | U.H. Tp(hrs)= .590
02643>-----
02644> Unit Hyd Qpeak (cms)= .229
02645>
02646> PEAK FLOW (cms)= .081 (i)
02647> TIME TO PEAK (hrs)= 1.800
02648> RUNOFF VOLUME (mm)= 13.287
02649> TOTAL RAINFALL (mm)= 52.045
02650> RUNOFF COEFFICIENT = .255
02651>
02652> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02653>
02654>-----
02655> 010:0036-----
02656>
02657> | CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
02658> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02659> | U.H. Tp(hrs)= .970
02660>-----
02661> Unit Hyd Qpeak (cms)= .142
02662>
02663> PEAK FLOW (cms)= .058 (i)
02664> TIME TO PEAK (hrs)= 2.300
02665> RUNOFF VOLUME (mm)= 13.287
02666> TOTAL RAINFALL (mm)= 52.045
02667> RUNOFF COEFFICIENT = .255

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02668>
02669> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02670>-----
02671>
02672> 010:0037-----
02673>
02674> | ADD HYD (PostTot ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
02675> (ha) (cms) (hrs) (mm) (cms)
02676> ID1 01:Control 102.61 3.282 1.83 37.12 .000
02677> +ID2 02:600 .99 .032 1.48 13.29 .000
02678> +ID3 03:601 3.54 .081 1.80 13.29 .000
02679> +ID4 04:602 3.61 .058 2.30 13.29 .000
02680>-----
02681> SUM 05:PostTot 110.75 3.436 1.83 35.36 .000
02682>
02683> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02684>-----
02685>
02686> 010:0038-----
02687>
02688> 010:0002-----
02689>
02690> 010:0002-----
02691> ** END OF RUN : 24
02692>-----
02693> *-----
02694>
02695>-----
02696>
02697>-----
02698>
02699>-----
02700> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
02701> | | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
02702> TZERO = .00 hrs on 0
02703> METOUT= 2 (output = METRIC)
02704> NRUN = 025
02705> NSTORM= 1
02706> # 1=1dn25Yr.3hr
02707>-----
02708> 025:0002-----
02709> *#-----
02710> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
02711> *# Date : 2022-11-14
02712> *# Modeller : [AKK]
02713> *# Company : Stantec Consulting Ltd. (London)
02714> *# License # : 4730904
02715> *#-----
02716> *#-----
02717> *#
02718> *# This model represents the hydrologic characteristics of the existing and
02719> *# proposed conditions in the proposed subdivision.
02720> *# Storm events modeled are:
02721> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
02722> *#-----
02723> *#-----
02724>-----
02725> 025:0002-----
02726>
02727> | READ STORM | Filename: 25-yr, 3hr Chicago Storm from London IDF
02728> | Ptotal= 61.48 mm | Comments: 25-yr, 3hr Chicago Storm from London IDF
02729>-----
02730> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
02731> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
02732> .08 3.863 | .83 30.802 | 1.58 13.993 | 2.33 5.432
02733> .17 4.298 | .92 74.085 | 1.67 11.991 | 2.42 5.077
02734> .25 4.843 | 1.00 190.819 | 1.75 10.465 | 2.50 4.766
02735> .33 5.545 | 1.08 95.197 | 1.83 9.267 | 2.58 4.490
02736> .42 6.481 | 1.17 53.926 | 1.92 8.306 | 2.67 4.244
02737> .50 7.783 | 1.25 36.022 | 2.00 7.519 | 2.75 4.024
02738> .58 9.705 | 1.33 26.421 | 2.08 6.864 | 2.83 3.826
02739> .67 12.783 | 1.42 20.579 | 2.17 6.312 | 2.92 3.646
02740> .75 18.359 | 1.50 16.712 | 2.25 5.840 | 3.00 3.483
02741>-----
02742>-----
02743> 025:0003-----
02744> *#-----
02745> *#
02746> *# Existing Conditions to determine target release rates
02747> *#-----
02748> *#-----
02749>-----
02750> | CALIB NASHYD | Area (ha)= 49.50 Curve Number (CN)=84.00
02751> | 01:3101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02752> | U.H. Tp(hrs)= .840
02753>-----
02754> Unit Hyd Qpeak (cms)= 2.251
02755>
02756> PEAK FLOW (cms)= 2.102 (i)
02757> TIME TO PEAK (hrs)= 2.067
02758> RUNOFF VOLUME (mm)= 30.422
02759> TOTAL RAINFALL (mm)= 61.481
02760> RUNOFF COEFFICIENT = .495
02761>
02762> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02763>-----
02764>-----
02765> 025:0004-----
02766>
02767> | CALIB NASHYD | Area (ha)= 32.80 Curve Number (CN)=84.00
02768> | 02:3102 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02769> | U.H. Tp(hrs)= .620
02770>-----
02771> Unit Hyd Qpeak (cms)= 2.021
02772>
02773> PEAK FLOW (cms)= 1.747 (i)
02774> TIME TO PEAK (hrs)= 1.800
02775> RUNOFF VOLUME (mm)= 30.422
02776> TOTAL RAINFALL (mm)= 61.481
02777> RUNOFF COEFFICIENT = .495
02778>
02779> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02780>-----
02781>-----
02782> 025:0005-----
02783>
02784> | CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
02785> | 03:3103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
02786> | U.H. Tp(hrs)= .480
02787>-----
02788> Unit Hyd Qpeak (cms)= .708
02789>
02790> PEAK FLOW (cms)= .570 (i)
02791> TIME TO PEAK (hrs)= 1.617
02792> RUNOFF VOLUME (mm)= 30.422
02793> TOTAL RAINFALL (mm)= 61.481
02794> RUNOFF COEFFICIENT = .495

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03303> Length (m) = 250.00 40.00
03304> Mannings n = .013 .240
03305>
03306> Max.eff.Inten.(mm/hr)= 190.82 99.45
03307> over (min) 3.00 12.00
03308> Storage Coeff. (min)= 3.42 (ii) 11.92 (ii)
03309> Unit Hyd. Tpeak (min)= 3.00 12.00
03310> Unit Hyd. peak (cms)= .34 .09
03311>
03312> PEAK FLOW (cms)= .56 .22 *TOTALS*
03313> TIME TO PEAK (hrs)= 1.02 1.22 1.017 (.634 (iii))
03314> RUNOFF VOLUME (mm)= 59.48 36.10 46.624
03315> TOTAL RAINFALL (mm)= 61.48 61.48 61.481
03316> RUNOFF COEFFICIENT = .97 .59 .758
03317>
03318> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03319> CN* = 86.0 Ia = Dep. Storage (Above)
03320> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03321> THAN THE STORAGE COEFFICIENT.
03322> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03323>
03324> -----
03325> 025:0027-----
03326>
03327> | CALIB STANDHYD | Area (ha)= 3.14
03328> | 02:500 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03329>
03330> IMPERVIOUS PERVIOUS (i)
03331> Surface Area (ha)= 1.73 1.41
03332> Dep. Storage (mm)= 2.00 5.00
03333> Average Slope (%)= 1.00 1.00
03334> Length (m)= 250.00 40.00
03335> Mannings n = .013 .240
03336>
03337> Max.eff.Inten.(mm/hr)= 190.82 99.45
03338> over (min) 3.00 12.00
03339> Storage Coeff. (min)= 3.42 (ii) 11.92 (ii)
03340> Unit Hyd. Tpeak (min)= 3.00 12.00
03341> Unit Hyd. peak (cms)= .34 .09
03342>
03343> PEAK FLOW (cms)= .60 .24 *TOTALS*
03344> TIME TO PEAK (hrs)= 1.02 1.22 1.017 (.679 (iii))
03345> RUNOFF VOLUME (mm)= 59.48 36.10 46.624
03346> TOTAL RAINFALL (mm)= 61.48 61.48 61.481
03347> RUNOFF COEFFICIENT = .97 .59 .758
03348>
03349> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03350> CN* = 86.0 Ia = Dep. Storage (Above)
03351> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03352> THAN THE STORAGE COEFFICIENT.
03353> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03354>
03355> -----
03356> 025:0028-----
03357>
03358> | CALIB STANDHYD | Area (ha)= 5.45
03359> | 03:502 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03360>
03361> IMPERVIOUS PERVIOUS (i)
03362> Surface Area (ha)= 3.00 2.45
03363> Dep. Storage (mm)= 2.00 5.00
03364> Average Slope (%)= 1.00 1.00
03365> Length (m)= 600.00 40.00
03366> Mannings n = .013 .240
03367>
03368> Max.eff.Inten.(mm/hr)= 174.88 89.79
03369> over (min) 6.00 15.00
03370> Storage Coeff. (min)= 5.99 (ii) 14.84 (ii)
03371> Unit Hyd. Tpeak (min)= 6.00 15.00
03372> Unit Hyd. peak (cms)= .19 .08
03373>
03374> PEAK FLOW (cms)= .83 .37 *TOTALS*
03375> TIME TO PEAK (hrs)= 1.07 1.27 1.083 (1.004 (iii))
03376> RUNOFF VOLUME (mm)= 59.48 36.10 46.624
03377> TOTAL RAINFALL (mm)= 61.48 61.48 61.481
03378> RUNOFF COEFFICIENT = .97 .59 .758
03379>
03380> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03381> CN* = 86.0 Ia = Dep. Storage (Above)
03382> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03383> THAN THE STORAGE COEFFICIENT.
03384> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03385>
03386> -----
03387> 025:0029-----
03388>
03389> | ADD HYD (Pond5In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
03390> | ID1 01:501 | (ha) (cms) (hrs) (mm) (cms)
03391> | +ID2 02:500 | 2.93 .634 1.02 46.62 .000
03392> | +ID3 03:502 | 3.14 .679 1.02 46.62 .000
03393> | +ID3 03:502 | 5.45 1.004 1.08 46.62 .000
03394>
03395> SUM 04:Pond5In 11.52 2.197 1.03 46.62 .000
03396>
03397> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03398>
03399> -----
03400> 025:0030-----
03401>
03402> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
03403> | IN>04:(Pond5I) |
03404> | OUT<05:(Pond5 ) |
03405>
03406> ===== OUTFLOW STORAGE TABLE =====
03407> OUTFLOW STORAGE | OUTFLOW STORAGE
03408> (cms) (ha.m.) | (cms) (ha.m.)
03409> .000 .000E+00 | .850 .5000E+00
03410> .190 .2300E+00 | .000 .0000E+00
03411>
03412> ROUTING RESULTS AREA QPEAK TPEAK R.V.
03413> (ha) (cms) (hrs) (mm)
03414> INFLOW >04: (Pond5I) 11.52 2.197 1.033 46.624
03415> OUTFLOW<05: (Pond5 ) 11.52 .459 1.800 46.624
03416>
03417> PEAK FLOW REDUCTION [Qout/Qin] (%) = 20.882
03418> TIME SHIFT OF PEAK FLOW (min)= 46.00
03419> MAXIMUM STORAGE USED (ha.m.)=.3400E+00
03420>
03421> -----
03422> 025:0031-----
03423> *****
03424> *#
03425> *# EXT3 Sizing, Cas EXT3
03426> *#
03427> -----
03428> | CALIB STANDHYD | Area (ha)= 9.16
03429> | 01:EXT3 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03430>

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03431> IMPERVIOUS PERVIOUS (i)
03432> Surface Area (ha)= 5.04 4.12
03433> Dep. Storage (mm)= 2.00 5.00
03434> Average Slope (%)= 1.00 1.00
03435> Length (m)= 400.00 40.00
03436> Mannings n = .013 .240
03437>
03438> Max.eff.Inten.(mm/hr)= 190.82 95.71
03439> over (min) 5.00 13.00
03440> Storage Coeff. (min)= 4.53 (ii) 13.16 (ii)
03441> Unit Hyd. Tpeak (min)= 5.00 13.00
03442> Unit Hyd. peak (cms)= .24 .09
03443>
03444> PEAK FLOW (cms)= 1.55 .66 *TOTALS*
03445> TIME TO PEAK (hrs)= 1.05 1.23 1.067 (1.849 (iii))
03446> RUNOFF VOLUME (mm)= 59.48 36.10 46.624
03447> TOTAL RAINFALL (mm)= 61.48 61.48 61.481
03448> RUNOFF COEFFICIENT = .97 .59 .758
03449>
03450> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03451> CN* = 86.0 Ia = Dep. Storage (Above)
03452> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03453> THAN THE STORAGE COEFFICIENT.
03454> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03455>
03456> -----
03457> 025:0032-----
03458>
03459> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
03460> | TotalHyd 01:EXT3 | Number of inlets in system [MINLET] = 1
03461> | | Total major system storage [TMJSTO] = .150 (cms)
03462> | | = 5000.(cu.m.)
03463>
03464> ID: NHYD AREA QPEAK TPEAK R.V. DWF
03465> (ha) (cms) (hrs) (mm) (cms)
03466> TOTAL HYD. 01:EXT3 9.16 1.849 1.067 46.624 .000
03467>
03468> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
03469> MINOR SYST 03:MinorE 9.16 .150 .733 46.692 .000
03470>
03471> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03472>
03473> Maximum MAJOR SYSTEM storage used = 2956.(cu.m.)
03474>
03475> -----
03476> 025:0033-----
03477> *****
03478> *# Flow Totals and Channel Runoff
03479> *#
03480> *****
03481>
03482> | ADD HYD (Control ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
03483> | ID1 02:noFlow | (ha) (cms) (hrs) (mm) (cms)
03484> | +ID2 03:MinorEXT3 | .00 .000 .00 .00 .000
03485> | +ID3 05:Pond5 | 9.16 .150 .73 46.69 .000
03486> | +ID4 06:Pond4 | 11.52 .459 1.80 46.62 .000
03487> | +ID5 07:Pond3 | 18.88 .857 1.75 41.23 .000
03488> | +ID6 08:Pond2 | 7.53 .321 1.78 46.62 .000
03489> | +ID7 09:Pond1 | 4.08 .158 1.78 46.62 .000
03490> | +ID8 10:ExPond | 32.50 1.575 1.75 46.62 .000
03491>
03492> SUM 01:Control 102.61 4.425 1.75 45.64 .000
03493>
03494> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03495>
03496> -----
03497> 025:0034-----
03498> *****
03499>
03500> | CALIB NASHYD | Area (ha)= .99 Curve Number (CN)=68.00
03501> | 02:600 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03502> | U.H. Tp(hrs)= .350
03503>
03504> Unit Hyd Qpeak (cms) = .108
03505>
03506> PEAK FLOW (cms) = .045 (i)
03507> TIME TO PEAK (hrs) = 1.483
03508> RUNOFF VOLUME (mm) = 18.124
03509> TOTAL RAINFALL (mm) = 61.481
03510> RUNOFF COEFFICIENT = .295
03511>
03512> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03513>
03514> -----
03515> 025:0035-----
03516>
03517> | CALIB NASHYD | Area (ha)= 3.54 Curve Number (CN)=68.00
03518> | 03:601 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03519> | U.H. Tp(hrs)= .590
03520>
03521> Unit Hyd Qpeak (cms) = .229
03522>
03523> PEAK FLOW (cms) = .113 (i)
03524> TIME TO PEAK (hrs) = 1.800
03525> RUNOFF VOLUME (mm) = 18.124
03526> TOTAL RAINFALL (mm) = 61.481
03527> RUNOFF COEFFICIENT = .295
03528>
03529> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03530>
03531> -----
03532> 025:0036-----
03533>
03534> | CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
03535> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03536> | U.H. Tp(hrs)= .970
03537>
03538> Unit Hyd Qpeak (cms) = .142
03539>
03540> PEAK FLOW (cms) = .090 (i)
03541> TIME TO PEAK (hrs) = 2.283
03542> RUNOFF VOLUME (mm) = 18.124
03543> TOTAL RAINFALL (mm) = 61.481
03544> RUNOFF COEFFICIENT = .295
03545>
03546> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03547>
03548> -----
03549> 025:0037-----
03550>
03551> | ADD HYD (PostTot ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
03552> | ID1 01:Control | (ha) (cms) (hrs) (mm) (cms)
03553> | +ID2 02:600 | 102.61 4.425 1.75 45.64 .000
03554> | +ID3 03:601 | .99 .045 1.48 18.12 .000
03555> | +ID3 03:601 | 3.54 .113 1.80 18.12 .000
03556> | +ID4 04:602 | 3.61 .080 2.28 18.12 .000

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03557> =====
03558> SUM 05:PostTot      110.75  4.636  1.75  43.62  .000
03559>
03560> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03561>
03562> -----
03563> 025:0038-----
03564>
03565> 025:0002-----
03566>
03567> 025:0002-----
03568>
03569> 025:0002-----
03570> ** END OF RUN : 49
03571>
03572> *****
03573>
03574>
03575>
03576>
03577>
03578> -----
03579> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
03580> | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
03581> | TZERO = .00 hrs on 0
03582> | METOUT= 2 (output = METRIC)
03583> | NRUN = 050
03584> | NSTORM= 1
03585> | # 1=1dn50YR.3hr
03586>
03587> 050:0002-----
03588> #*****
03589> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
03590> *# Date : 2022-11-14
03591> *# Modeller : [AKK]
03592> *# Company : Stantec Consulting Ltd. (London)
03593> *# License # : 4730904
03594> *#*****
03595> *#*****
03596> *#
03597> *# This model represents the hydrologic characteristics of the existing and
03598> *# proposed conditions in the proposed subdivision.
03599> *# Storm events modeled are:
03600> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
03601> *#
03602> *#*****
03603>
03604> 050:0002-----
03605>
03606> | READ STORM | Filename: 50-yr, 3hr Chicago Storm from London IDF
03607> | Ptotal= 68.72 mm | Comments: 50-yr, 3hr Chicago Storm from London IDF
03608>
03609>
03610>
03611>
03612>
03613>
03614>
03615>
03616>
03617>
03618>
03619>
03620>
03621>
03622> 050:0003-----
03623> #*****
03624> *#
03625> *# Existing Conditions to determine target release rates
03626> *#
03627> *#*****
03628>
03629> | CALIB NASHYD | Area (ha)= 49.50 Curve Number (CN)=84.00
03630> | 01:S101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03631> | U.H. Tp(hrs)= .840
03632>
03633> Unit Hyd Qpeak (cms)= 2.251
03634>
03635> PEAK FLOW (cms)= 2.513 (i)
03636> TIME TO PEAK (hrs)= 2.067
03637> RUNOFF VOLUME (mm)= 36.218
03638> TOTAL RAINFALL (mm)= 68.719
03639> RUNOFF COEFFICIENT = .527
03640>
03641> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03642>
03643> -----
03644> 050:0004-----
03645>
03646> | CALIB NASHYD | Area (ha)= 32.80 Curve Number (CN)=84.00
03647> | 02:S102 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03648> | U.H. Tp(hrs)= .620
03649>
03650> Unit Hyd Qpeak (cms)= 2.021
03651>
03652> PEAK FLOW (cms)= 2.091 (i)
03653> TIME TO PEAK (hrs)= 1.800
03654> RUNOFF VOLUME (mm)= 36.218
03655> TOTAL RAINFALL (mm)= 68.719
03656> RUNOFF COEFFICIENT = .527
03657>
03658> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03659>
03660> -----
03661> 050:0005-----
03662>
03663> | CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
03664> | 03:S103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03665> | U.H. Tp(hrs)= .480
03666>
03667> Unit Hyd Qpeak (cms)= .708
03668>
03669> PEAK FLOW (cms)= .683 (i)
03670> TIME TO PEAK (hrs)= 1.617
03671> RUNOFF VOLUME (mm)= 36.218
03672> TOTAL RAINFALL (mm)= 68.719
03673> RUNOFF COEFFICIENT = .527
03674>
03675> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03676>
03677> -----
03678> 050:0006-----
03679>
03680> | CALIB NASHYD | Area (ha)= 33.50 Curve Number (CN)=84.00
03681> | 04:S104 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03682> | U.H. Tp(hrs)= .720
03683>

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03684> Unit Hyd Qpeak (cms)= 1.777
03685>
03686> PEAK FLOW (cms)= 1.911 (i)
03687> TIME TO PEAK (hrs)= 1.917
03688> RUNOFF VOLUME (mm)= 36.218
03689> TOTAL RAINFALL (mm)= 68.719
03690> RUNOFF COEFFICIENT = .527
03691>
03692> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03693>
03694> -----
03695> 050:0007-----
03696>
03697> | ADD HYD (Total ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
03698> | (ha) (cms) (hrs) (mm) (cms)
03699> | ID1 01:S101 49.50 2.513 2.07 36.22 .000
03700> | +ID2 02:S102 32.80 2.091 1.80 36.22 .000
03701> | +ID3 03:S103 8.90 .683 1.62 36.22 .000
03702> | +ID4 04:S104 33.50 1.911 1.92 36.22 .000
03703> | =====
03704> | SUM 05:Total 124.70 7.005 1.88 36.22 .000
03705>
03706> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03707>
03708> -----
03709> 050:0008-----
03710> #*****
03711> *#
03712> *# External Pond Sizing, CAs EXT1 and EXT2
03713> *#
03714> *#*****
03715>
03716> | CALIB STANDHYD | Area (ha)= 9.50
03717> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03718>
03719>
03720> IMPERVIOUS PERVIOUS (i)
03721> Surface Area (ha)= 5.22 4.27
03722> Dep. Storage (mm)= 2.00 5.00
03723> Average Slope (%)= 1.00 1.00
03724> Length (m)= 400.00 40.00
03725> Mannings n = .013 .240
03726>
03727> Max.eff.Inten.(mm/hr)= 211.98 117.07
03728> over (min)= 4.00 12.00
03729> Storage Coeff. (min)= 4.35 (ii) 12.31 (ii)
03730> Unit Hyd. Tpeak (min)= 4.00 12.00
03731> Unit Hyd. peak (cms)= .27 .09
03732>
03733> *TOTALS*
03734> PEAK FLOW (cms)= 1.84 .84 2.219 (iii)
03735> TIME TO PEAK (hrs)= 1.03 1.22 1.050
03736> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03737> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03738> RUNOFF COEFFICIENT = .97 .62 .776
03739>
03740> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03741> CN* = 86.0 Ia = Dep. Storage (Above)
03742> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03743> THAN THE STORAGE COEFFICIENT.
03744> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03745>
03746> -----
03747> 050:0009-----
03748>
03749> | CALIB STANDHYD | Area (ha)= 23.00
03750> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03751>
03752>
03753> IMPERVIOUS PERVIOUS (i)
03754> Surface Area (ha)= 12.65 10.35
03755> Dep. Storage (mm)= 2.00 5.00
03756> Average Slope (%)= 1.00 1.00
03757> Length (m)= 750.00 40.00
03758> Mannings n = .013 .240
03759>
03760> Max.eff.Inten.(mm/hr)= 181.83 105.54
03761> over (min)= 7.00 15.00
03762> Storage Coeff. (min)= 6.74 (ii) 15.04 (ii)
03763> Unit Hyd. Tpeak (min)= 7.00 15.00
03764> Unit Hyd. peak (cms)= .17 .08
03765>
03766> *TOTALS*
03767> PEAK FLOW (cms)= 3.71 1.82 4.718 (iii)
03768> TIME TO PEAK (hrs)= 1.08 1.27 1.100
03769> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03770> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03771> RUNOFF COEFFICIENT = .97 .62 .776
03772>
03773> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03774> CN* = 86.0 Ia = Dep. Storage (Above)
03775> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03776> THAN THE STORAGE COEFFICIENT.
03777> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03778>
03779> -----
03780> 050:0010-----
03781>
03782> | ADD HYD (ExPondIn ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
03783> | (ha) (cms) (hrs) (mm) (cms)
03784> | ID1 01:EXT2 9.50 2.219 1.05 53.36 .000
03785> | +ID2 02:EXT1 23.00 4.718 1.10 53.36 .000
03786> | =====
03787> | SUM 03:ExPondIn 32.50 6.847 1.10 53.36 .000
03788>
03789> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03790>
03791> -----
03792> 050:0011-----
03793>
03794> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
03795> | IN>03: (ExPond) |
03796> | OUT<10: (ExPond) | ===== OUTFLOW STORAGE TABLE =====
03797>
03798> OUTFLOW STORAGE | OUTFLOW STORAGE
03799> (cms) (ha.m.) | (cms) (ha.m.)
03800> .000 .0000E+00 | 2.420 .1200E+01
03801> .530 .4500E+00 | .000 .0000E+00
03802>
03803> ROUTING RESULTS AREA QPEAK TPEAK R.V.
03804> (ha) (cms) (hrs) (mm)
03805> INFLOW >03: (ExPond) 32.50 6.847 1.100 53.355
03806> OUTFLOW<10: (ExPond) 32.50 1.871 1.717 53.355
03807>
03808> PEAK FLOW REDUCTION [Qout/Qin] (%) = 27.326
03809> TIME SHIFT OF PEAK FLOW (min) = 37.000
03810> MAXIMUM STORAGE USED (ha.m.) = .9822E+00
03811>
03812> -----
03813> 050:0012-----
03814> #*****
03815> *#

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03811> *# Pond 1 Sizing, CAs 100
03812> *#
03813> *#-----
03814>
03815> | CALIB STANDHYD | Area (ha)= 4.08
03816> | 01:100 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03817> -----
03818> IMPERVIOUS PERVIOUS (i)
03819> Surface Area (ha)= 2.24 1.84
03820> Dep. Storage (mm)= 2.00 5.00
03821> Average Slope (%)= 1.00 1.00
03822> Length (m)= 300.00 40.00
03823> Mannings n = .013 .240
03824>
03825> Max.eff.Inten.(mm/hr)= 211.98 117.07
03826> over (min) 4.00 12.00
03827> Storage Coeff. (min)= 3.66 (ii) 11.62 (ii)
03828> Unit Hyd. Tpeak (min)= 4.00 12.00
03829> Unit Hyd. peak (cms)= .30 .10
03830>
03831> PEAK FLOW (cms)= .83 .37 *.TOTALS*
03832> TIME TO PEAK (hrs)= 1.03 1.20 1.050 (iii)
03833> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03834> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03835> RUNOFF COEFFICIENT = .97 .62 .776
03836>
03837> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03838> CN* = 86.0 Ia = Dep. Storage (Above)
03839> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03840> THAN THE STORAGE COEFFICIENT.
03841> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03842>
03843> -----
03844> 050:0013-----
03845>
03846> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
03847> | IN>01:(100 ) |
03848> | OUT<09:(Pond1) |
03849> ===== OUTFLOW STORAGE TABLE =====
03850> OUTFLOW STORAGE | OUTFLOW STORAGE
03851> (cms) (ha.m.) | (cms) (ha.m.)
03852> .000 .0000E+00 | .300 .2000E+00
03853> .070 .7000E-01 | .000 .0000E+00
03854>
03855> ROUTING RESULTS AREA QPEAK TPEAK R.V.
03856> (ha) (cms) (hrs) (mm)
03857> INFLOW >01: (100 ) 4.08 .988 1.050 53.355
03858> OUTFLOW<09: (Pond1) 4.08 .187 1.750 53.355
03859>
03860> PEAK FLOW REDUCTION [Qout/Qin] (%) = 18.937
03861> TIME SHIFT OF PEAK FLOW (min) = 42.00
03862> MAXIMUM STORAGE USED (ha.m.) = .1362E+00
03863>
03864> 050:0014-----
03865> *#-----
03866> *#
03867> *# Pond 2 Sizing, CAs 200
03868> *#
03869> *#-----
03870>
03871> | CALIB STANDHYD | Area (ha)= 7.53
03872> | 01:200 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03873> -----
03874> IMPERVIOUS PERVIOUS (i)
03875> Surface Area (ha)= 4.14 3.39
03876> Dep. Storage (mm)= 2.00 5.00
03877> Average Slope (%)= 1.00 1.00
03878> Length (m)= 550.00 40.00
03879> Mannings n = .013 .240
03880>
03881> Max.eff.Inten.(mm/hr)= 211.98 112.60
03882> over (min) 5.00 13.00
03883> Storage Coeff. (min)= 5.26 (ii) 13.35 (ii)
03884> Unit Hyd. Tpeak (min)= 5.00 13.00
03885> Unit Hyd. peak (cms)= .22 .09
03886>
03887> PEAK FLOW (cms)= 1.35 .64 *.TOTALS*
03888> TIME TO PEAK (hrs)= 1.05 1.23 1.067 (iii)
03889> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03890> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03891> RUNOFF COEFFICIENT = .97 .62 .776
03892>
03893> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03894> CN* = 86.0 Ia = Dep. Storage (Above)
03895> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03896> THAN THE STORAGE COEFFICIENT.
03897> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03898>
03899> -----
03900> 050:0015-----
03901>
03902> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
03903> | IN>01:(200 ) |
03904> | OUT<08:(Pond2) |
03905> ===== OUTFLOW STORAGE TABLE =====
03906> OUTFLOW STORAGE | OUTFLOW STORAGE
03907> (cms) (ha.m.) | (cms) (ha.m.)
03908> .000 .0000E+00 | .560 .3000E+00
03909> .120 .1500E+00 | .000 .0000E+00
03910>
03911> ROUTING RESULTS AREA QPEAK TPEAK R.V.
03912> (ha) (cms) (hrs) (mm)
03913> INFLOW >01: (200 ) 7.53 1.667 1.067 53.355
03914> OUTFLOW<08: (Pond2) 7.53 .397 1.733 53.355
03915>
03916> PEAK FLOW REDUCTION [Qout/Qin] (%) = 23.826
03917> TIME SHIFT OF PEAK FLOW (min) = 40.00
03918> MAXIMUM STORAGE USED (ha.m.) = .2445E+00
03919>
03920> 050:0016-----
03921> *#-----
03922> *#
03923> *# Pond 3 Sizing, CAs 300, 301 and 302
03924> *#
03925> *#-----
03926>
03927> | CALIB STANDHYD | Area (ha)= 10.33
03928> | 01:300 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03929> -----
03930> IMPERVIOUS PERVIOUS (i)
03931> Surface Area (ha)= 5.68 4.65
03932> Dep. Storage (mm)= 2.00 5.00
03933> Average Slope (%)= 1.00 1.00
03934> Length (m)= 610.00 40.00
03935> Mannings n = .013 .240
03936>
03937> Max.eff.Inten.(mm/hr)= 194.39 108.81

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03938> over (min) 6.00 14.00
03939> Storage Coeff. (min)= 5.80 (ii) 13.99 (ii)
03940> Unit Hyd. Tpeak (min)= 6.00 14.00
03941> Unit Hyd. peak (cms)= .19 .08
03942>
03943> PEAK FLOW (cms)= 1.77 .85 *.TOTALS*
03944> TIME TO PEAK (hrs)= 1.07 1.25 1.083 (iii)
03945> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03946> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03947> RUNOFF COEFFICIENT = .97 .62 .776
03948>
03949> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03950> CN* = 86.0 Ia = Dep. Storage (Above)
03951> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03952> THAN THE STORAGE COEFFICIENT.
03953> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03954>
03955> -----
03956> 050:0017-----
03957>
03958> | CALIB STANDHYD | Area (ha)= 4.18
03959> | 02:302 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
03960> -----
03961> IMPERVIOUS PERVIOUS (i)
03962> Surface Area (ha)= 2.30 1.88
03963> Dep. Storage (mm)= 2.00 5.00
03964> Average Slope (%)= 1.00 1.00
03965> Length (m)= 210.00 40.00
03966> Mannings n = .013 .240
03967>
03968> Max.eff.Inten.(mm/hr)= 211.98 122.38
03969> over (min) 3.00 11.00
03970> Storage Coeff. (min)= 2.95 (ii) 10.77 (ii)
03971> Unit Hyd. Tpeak (min)= 3.00 11.00
03972> Unit Hyd. peak (cms)= .38 .10
03973>
03974> PEAK FLOW (cms)= .92 .40 *.TOTALS*
03975> TIME TO PEAK (hrs)= 1.02 1.18 1.017 (iii)
03976> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
03977> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
03978> RUNOFF COEFFICIENT = .97 .62 .776
03979>
03980> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
03981> CN* = 86.0 Ia = Dep. Storage (Above)
03982> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03983> THAN THE STORAGE COEFFICIENT.
03984> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03985>
03986> -----
03987> 050:0018-----
03988>
03989> | CALIB NASHYD | Area (ha)= 4.37 Curve Number (CN)=76.00
03990> | 03:301 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
03991> U.H. Tp(hrs)= .410
03992>
03993> Unit Hyd Qpeak (cms)= .407
03994>
03995> PEAK FLOW (cms)= .284 (i)
03996> TIME TO PEAK (hrs)= 1.550
03997> RUNOFF VOLUME (mm)= 28.209
03998> TOTAL RAINFALL (mm)= 68.719
03999> RUNOFF COEFFICIENT = .410
04000>
04001> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04002>
04003> -----
04004> 050:0019-----
04005>
04006> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04007> (ha) (cms) (hrs) (mm) (cms)
04008> ID1 01:300 10.33 2.223 1.08 53.36 .000
04009> +ID2 02:302 4.18 1.076 1.02 53.36 .000
04010> +ID3 03:301 4.37 .284 1.55 28.21 .000
04011> =====
04012> SUM 04:Pond3In 18.88 3.247 1.08 47.53 .000
04013>
04014> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04015>
04016> -----
04017> 050:0020-----
04018>
04019> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04020> | IN>04:(Pond3) |
04021> | OUT<07:(Pond3 ) |
04022> ===== OUTFLOW STORAGE TABLE =====
04023> OUTFLOW STORAGE | OUTFLOW STORAGE
04024> (cms) (ha.m.) | (cms) (ha.m.)
04025> .000 .0000E+00 | 1.400 .5800E+00
04026> .310 .2500E+00 | .000 .0000E+00
04027>
04028> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04029> (ha) (cms) (hrs) (mm)
04030> INFLOW >04: (Pond3) 18.88 3.247 1.083 47.535
04031> OUTFLOW<07: (Pond3 ) 18.88 1.034 1.717 47.535
04032>
04033> PEAK FLOW REDUCTION [Qout/Qin] (%) = 31.848
04034> TIME SHIFT OF PEAK FLOW (min) = 38.00
04035> MAXIMUM STORAGE USED (ha.m.) = .4693E+00
04036>
04037> 050:0021-----
04038> *#-----
04039> *#
04040> *# Pond 4 Sizing, CAs 400, 401 and 402
04041> *#
04042> *#-----
04043>
04044> | CALIB STANDHYD | Area (ha)= 10.47
04045> | 01:402 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04046> -----
04047> IMPERVIOUS PERVIOUS (i)
04048> Surface Area (ha)= 5.76 4.71
04049> Dep. Storage (mm)= 2.00 5.00
04050> Average Slope (%)= 1.00 1.00
04051> Length (m)= 350.00 40.00
04052> Mannings n = .013 .240
04053>
04054> Max.eff.Inten.(mm/hr)= 211.98 117.07
04055> over (min) 4.00 12.00
04056> Storage Coeff. (min)= 4.01 (ii) 11.97 (ii)
04057> Unit Hyd. Tpeak (min)= 4.00 12.00
04058> Unit Hyd. peak (cms)= .28 .09
04059>
04060> PEAK FLOW (cms)= 2.08 .94 *.TOTALS*
04061> TIME TO PEAK (hrs)= 1.03 1.20 1.050 (iii)
04062> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04063> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04064> RUNOFF COEFFICIENT = .97 .62 .776

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04065>
04066> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04067> CN* = 86.0 Ia = Dep. Storage (Above)
04068> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04069> THAN THE STORAGE COEFFICIENT.
04070> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04071>
-----
04072>
04073> 050:0022-----
04074>
04075> | CALIB STANDHYD | Area (ha)= 3.22
04076> | 02:401 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04077>
-----
04078>
04079> IMPERVIOUS PERVIOUS (i)
04080> Surface Area (ha)= 1.77 1.45
04081> Dep. Storage (mm)= 2.00 5.00
04082> Average Slope (%)= 1.00 1.00
04083> Length (m)= 250.00 40.00
04084> Mannings n = .013 .240
04085> Max.eff.Inten.(mm/hr)= 211.98 122.38
04086> over (min) 3.00 11.00
04087> Storage Coeff. (min)= 3.28 (ii) 11.10 (ii)
04088> Unit Hyd. Tpeak (min)= 3.00 11.00
04089> Unit Hyd. peak (cms)= .35 .10
04090>
04091> PEAK FLOW (cms)= .69 .30 *TOTALS*
04092> TIME TO PEAK (hrs)= 1.02 1.18 .808 (iii)
04093> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04094> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04095> RUNOFF COEFFICIENT = .97 .62 .776
04096>
04097> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04098> CN* = 86.0 Ia = Dep. Storage (Above)
04099> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04100> THAN THE STORAGE COEFFICIENT.
04101> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04102>
-----
04103>
04104> 050:0023-----
04105>
04106> | CALIB STANDHYD | Area (ha)= 5.25
04107> | 03:400 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04108>
-----
04109>
04110> IMPERVIOUS PERVIOUS (i)
04111> Surface Area (ha)= 2.89 2.36
04112> Dep. Storage (mm)= 2.00 5.00
04113> Average Slope (%)= 1.00 1.00
04114> Length (m)= 250.00 40.00
04115> Mannings n = .013 .240
04116> Max.eff.Inten.(mm/hr)= 211.98 122.38
04117> over (min) 3.00 11.00
04118> Storage Coeff. (min)= 3.28 (ii) 11.10 (ii)
04119> Unit Hyd. Tpeak (min)= 3.00 11.00
04120> Unit Hyd. peak (cms)= .35 .10
04121>
04122> PEAK FLOW (cms)= 1.13 .49 *TOTALS*
04123> TIME TO PEAK (hrs)= 1.02 1.18 1.318 (iii)
04124> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04125> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04126> RUNOFF COEFFICIENT = .97 .62 .776
04127>
04128> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04129> CN* = 86.0 Ia = Dep. Storage (Above)
04130> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04131> THAN THE STORAGE COEFFICIENT.
04132> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04133>
-----
04134>
04135> 050:0024-----
04136>
04137> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04138> | | | (ha) (cms) (hrs) (mm) (cms)
04139> | ID1 01:402 | 10.47 2.490 1.05 53.36 .000
04140> | +ID2 02:401 | 3.22 .808 1.02 53.36 .000
04141> | +ID3 03:400 | 5.25 1.318 1.02 53.36 .000
04142>
04143> SUM 04:Pond4In 18.94 4.600 1.03 53.36 .000
04144>
04145> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04146>
-----
04147>
04148> 050:0025-----
04149>
04150> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04151> | IN>04:(Pond4I) |
04152> | OUT<06:(Pond4 ) |
04153>
-----
04154>
04155> ===== OUTFLOW STORAGE TABLE =====
04156> OUTFLOW STORAGE | OUTFLOW STORAGE
04157> (cms) (ha.m.) | (cms) (ha.m.)
04158> .000 .0000E+00 | 1.400 .7000E+00
04159> .310 .3000E+00 | 1.000 .0000E+00
04160>
04161>
04162> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04163> (ha) (cms) (hrs) (mm)
04164> INFLOW >04: (Pond4I) 18.94 4.600 1.033 53.355
04165> OUTFLOW<06: (Pond4 ) 18.94 1.097 1.633 53.355
04166>
04167> PEAK FLOW REDUCTION [Qout/Qin] (%) = 23.858
04168> TIME SHIFT OF PEAK FLOW (min)= 36.00
04169> MAXIMUM STORAGE USED (ha.m.)=.5890E+00
04170>
-----
04171>
04172> 050:0026-----
04173>
04174> | CALIB STANDHYD | Area (ha)= 2.93
04175> | 01:501 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04176>
-----
04177>
04178> IMPERVIOUS PERVIOUS (i)
04179> Surface Area (ha)= 1.61 1.32
04180> Dep. Storage (mm)= 2.00 5.00
04181> Average Slope (%)= 1.00 1.00
04182> Length (m)= 250.00 40.00
04183> Mannings n = .013 .240
04184> Max.eff.Inten.(mm/hr)= 211.98 122.38
04185> over (min) 3.00 11.00
04186> Storage Coeff. (min)= 3.28 (ii) 11.10 (ii)
04187> Unit Hyd. Tpeak (min)= 3.00 11.00
04188> Unit Hyd. peak (cms)= .35 .10
04189>
04190> PEAK FLOW (cms)= .63 .27 *TOTALS*
04191> TIME TO PEAK (hrs)= 1.02 1.18 .736 (iii)

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04192> TIME TO PEAK (hrs)= 1.02 1.18 1.017
04193> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04194> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04195> RUNOFF COEFFICIENT = .97 .62 .776
04196>
04197> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04198> CN* = 86.0 Ia = Dep. Storage (Above)
04199> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04200> THAN THE STORAGE COEFFICIENT.
04201> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04202>
-----
04203>
04204> 050:0027-----
04205>
04206> | CALIB STANDHYD | Area (ha)= 3.14
04207> | 02:500 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04208>
-----
04209>
04210> IMPERVIOUS PERVIOUS (i)
04211> Surface Area (ha)= 1.73 1.41
04212> Dep. Storage (mm)= 2.00 5.00
04213> Average Slope (%)= 1.00 1.00
04214> Length (m)= 250.00 40.00
04215> Mannings n = .013 .240
04216> Max.eff.Inten.(mm/hr)= 211.98 122.38
04217> over (min) 3.00 11.00
04218> Storage Coeff. (min)= 3.28 (ii) 11.10 (ii)
04219> Unit Hyd. Tpeak (min)= 3.00 11.00
04220> Unit Hyd. peak (cms)= .35 .10
04221>
04222> PEAK FLOW (cms)= .67 .29 *TOTALS*
04223> TIME TO PEAK (hrs)= 1.02 1.18 1.788 (iii)
04224> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04225> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04226> RUNOFF COEFFICIENT = .97 .62 .776
04227>
04228> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04229> CN* = 86.0 Ia = Dep. Storage (Above)
04230> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04231> THAN THE STORAGE COEFFICIENT.
04232> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04233>
-----
04234>
04235> 050:0028-----
04236>
04237> | CALIB STANDHYD | Area (ha)= 5.45
04238> | 03:502 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04239>
-----
04240>
04241> IMPERVIOUS PERVIOUS (i)
04242> Surface Area (ha)= 3.00 2.45
04243> Dep. Storage (mm)= 2.00 5.00
04244> Average Slope (%)= 1.00 1.00
04245> Length (m)= 600.00 40.00
04246> Mannings n = .013 .240
04247> Max.eff.Inten.(mm/hr)= 194.39 108.81
04248> over (min) 6.00 14.00
04249> Storage Coeff. (min)= 5.74 (ii) 13.94 (ii)
04250> Unit Hyd. Tpeak (min)= 6.00 14.00
04251> Unit Hyd. peak (cms)= .19 .08
04252>
04253> PEAK FLOW (cms)= .94 .45 *TOTALS*
04254> TIME TO PEAK (hrs)= 1.07 1.25 1.176 (iii)
04255> RUNOFF VOLUME (mm)= 66.72 42.42 1.083
04256> TOTAL RAINFALL (mm)= 68.72 68.72 53.355
04257> RUNOFF COEFFICIENT = .97 .62 68.719
04258>
04259> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04260> CN* = 86.0 Ia = Dep. Storage (Above)
04261> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04262> THAN THE STORAGE COEFFICIENT.
04263> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04264>
-----
04265>
04266> 050:0029-----
04267>
04268> | ADD HYD (Pond5In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04269> | | | (ha) (cms) (hrs) (mm) (cms)
04270> | ID1 01:501 | 2.93 .736 1.02 53.36 .000
04271> | +ID2 02:500 | 3.14 .788 1.02 53.36 .000
04272> | +ID3 03:502 | 5.45 1.176 1.08 53.36 .000
04273>
04274> SUM 04:Pond5In 11.52 2.572 1.08 53.36 .000
04275>
04276> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04277>
-----
04278>
04279> 050:0030-----
04280>
04281> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04282> | IN>04:(Pond5I) |
04283> | OUT<05:(Pond5 ) |
04284>
-----
04285>
04286> ===== OUTFLOW STORAGE TABLE =====
04287> OUTFLOW STORAGE | OUTFLOW STORAGE
04288> (cms) (ha.m.) | (cms) (ha.m.)
04289> .000 .0000E+00 | 1.850 .5000E+00
04290> .190 .2300E+00 | .000 .0000E+00
04291>
04292>
04293> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04294> (ha) (cms) (hrs) (mm)
04295> INFLOW >04: (Pond5I) 11.52 2.572 1.083 53.355
04296> OUTFLOW<05: (Pond5 ) 11.52 .563 1.733 53.355
04297>
04298> PEAK FLOW REDUCTION [Qout/Qin] (%) = 21.873
04299> TIME SHIFT OF PEAK FLOW (min)= 39.00
04300> MAXIMUM STORAGE USED (ha.m.)=.3825E+00
04301>
-----
04302>
04303> 050:0031-----
04304>
04305> | CALIB STANDHYD | Area (ha)= 9.16
04306> | 01:EXT3 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04307>
-----
04308>
04309> IMPERVIOUS PERVIOUS (i)
04310> Surface Area (ha)= 5.04 4.12
04311> Dep. Storage (mm)= 2.00 5.00
04312> Average Slope (%)= 1.00 1.00
04313> Length (m)= 400.00 40.00
04314> Mannings n = .013 .240
04315> Max.eff.Inten.(mm/hr)= 211.98 117.07
04316> over (min) 4.00 12.00
04317> Storage Coeff. (min)= 4.35 (ii) 12.31 (ii)

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04319> Unit Hyd. Tpeak (min)= 4.00 12.00
04320> Unit Hyd. peak (cms)= .27 .09
04321>
04322> PEAK FLOW (cms)= 1.78 .81 *TOTALS+
04323> TIME TO PEAK (hrs)= 1.03 1.22 2.139 (iii)
04324> RUNOFF VOLUME (mm)= 66.72 42.42 53.355
04325> TOTAL RAINFALL (mm)= 68.72 68.72 68.719
04326> RUNOFF COEFFICIENT = .97 .62 .776
04327>
04328> (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
04329> CN* = 86.0 Ia = Dep. Storage (Above)
04330>
04331> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04332> THAN THE STORAGE COEFFICIENT.
04333> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04334>
04335> 050:0032-----
04336> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
04337> | TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
04338> |-----| Total minor system capacity = .150 (cms)
04339> | Total major system storage [TMJSTO] = 5000. (cu.m.)
04340>
04341> ID: NHYD AREA QPEAK TPEAK R.V. DWF
04342> (ha) (cms) (hrs) (mm) (cms)
04343>
04344> TOTAL HYD. 01:EXT3 9.16 2.139 1.050 53.355 .000
04345>
04346> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
04347> MINOR SYST 03:MinorE 9.16 1.500 .700 53.452 .000
04348>
04349> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04350>
04351> Maximum MAJOR SYSTEM storage used = 3520. (cu.m.)
04352>
04353> 050:0033-----
04354> *****
04355> **
04356> ** Flow Totals and Channel Runoff
04357> **
04358> **
04359> *****
04360>
04361> | ADD HYD (Control ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04362> (ha) (cms) (hrs) (mm) (cms)
04363>
04364> ID1 02:noFlow .00 .000 .00 .00 .000
04365> ID2 03:MinorEXT3 9.16 .150 .70 53.45 .000
04366> ID3 05:Pond5 11.52 .563 1.73 53.35 .000
04367> ID4 06:Pond4 18.94 1.097 1.63 53.35 .000
04368> ID5 07:Pond3 18.88 1.034 1.72 47.53 .000
04369> ID6 08:Pond2 7.53 .397 1.73 53.35 .000
04370> ID7 09:Pond1 4.08 .187 1.75 53.35 .000
04371> ID8 10:ExtPond 32.50 1.871 1.72 53.35 .000
04372>
04373> SUM 01:Control 102.61 5.293 1.70 52.29 .000
04374>
04375> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04376>
04377> 050:0034-----
04378>
04379> | CALIB NASHYD | Area (ha)= .99 Curve Number (CN)=68.00
04380> | 02:600 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04381> |-----| U.H. Tp (hrs)= .350
04382>
04383> Unit Hyd Peak (cms)= .108
04384>
04385> PEAK FLOW (cms)= .055 (i)
04386> TIME TO PEAK (hrs)= 1.467
04387> RUNOFF VOLUME (mm)= 22.156
04388> TOTAL RAINFALL (mm)= 68.719
04389> RUNOFF COEFFICIENT = .322
04390>
04391> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04392>
04393> 050:0035-----
04394>
04395> | CALIB NASHYD | Area (ha)= 3.54 Curve Number (CN)=68.00
04396> | 03:601 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04397> |-----| U.H. Tp (hrs)= .590
04398>
04399> Unit Hyd Peak (cms)= .229
04400>
04401> PEAK FLOW (cms)= .139 (i)
04402> TIME TO PEAK (hrs)= 1.783
04403> RUNOFF VOLUME (mm)= 22.156
04404> TOTAL RAINFALL (mm)= 68.719
04405> RUNOFF COEFFICIENT = .322
04406>
04407> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04408>
04409> 050:0036-----
04410>
04411> | CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
04412> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04413> |-----| U.H. Tp (hrs)= .970
04414>
04415> Unit Hyd Peak (cms)= .142
04416>
04417> PEAK FLOW (cms)= .098 (i)
04418> TIME TO PEAK (hrs)= 2.267
04419> RUNOFF VOLUME (mm)= 22.156
04420> TOTAL RAINFALL (mm)= 68.719
04421> RUNOFF COEFFICIENT = .322
04422>
04423> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04424>
04425> 050:0037-----
04426>
04427> | ADD HYD (PostTot ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04428> (ha) (cms) (hrs) (mm) (cms)
04429>
04430> ID1 01:Control 102.61 5.293 1.70 52.29 .000
04431> ID2 02:600 .99 .055 1.47 22.16 .000
04432> ID3 03:601 3.54 .139 1.78 22.16 .000
04433> ID4 04:602 3.61 .098 2.27 22.16 .000
04434>
04435> SUM 05:PostTot 110.75 5.550 1.72 50.08 .000
04436>
04437> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04438>
04439>
04440>
04441> 050:0038-----
04442>
04443>
04444> 050:0002-----
04445>

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04446> 050:0002-----
04447>
04448> 050:0002-----
04449>
04450> 050:0002-----
04451> ** END OF RUN : 99
04452>
04453> *****
04454>
04455>
04456>
04457>
04458>
04459>
04460> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
04461> | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
04462> TZERO = .00 hrs on 0
04463> METOUT= 2 (output = METRIC)
04464> NRUN = 100
04465> NSTORM= 1
04466> # 1=ldn100YR.3hr
04467>
04468> 100:0002-----
04469>
04470> ** Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
04471> ** Date : 2022-11-14
04472> ** Modeller : [AKK]
04473> ** Company : Stantec Consulting Ltd. (London)
04474> ** License # : 4730904
04475> **
04476> *****
04477> **
04478> ** This model represents the hydrologic characteristics of the existing and
04479> ** proposed conditions in the proposed subdivision.
04480> ** Storm events modeled are:
04481> ** 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
04482> **
04483> *****
04484>
04485> 100:0002-----
04486>
04487> | READ STORM | Filename: 100-yr, 3hr Chicago Storm from London ID
04488> | Ptotal= 75.83 mm | Comments: 100-yr, 3hr Chicago Storm from London ID
04489>
04490> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
04491> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
04492> .08 4.623 | .83 38.591 | 1.58 17.341 | 2.33 6.569
04493> .17 5.160 | .92 92.413 | 1.67 14.811 | 2.42 6.127
04494> .25 5.836 | 1.00 232.243 | 1.75 12.884 | 2.50 5.740
04495> .33 6.709 | 1.08 118.408 | 1.83 11.375 | 2.58 5.398
04496> .42 7.878 | 1.17 87.596 | 1.92 10.166 | 2.67 5.094
04497> .50 9.510 | 1.25 45.175 | 2.00 9.178 | 2.75 4.822
04498> .58 11.928 | 1.33 33.066 | 2.08 8.357 | 2.83 4.577
04499> .67 15.813 | 1.42 25.678 | 2.17 7.666 | 2.92 4.356
04500> .75 22.868 | 1.50 20.783 | 2.25 7.077 | 3.00 4.155
04501>
04502>
04503> 100:0003-----
04504> *****
04505> **
04506> ** Existing Conditions to determine target release rates
04507> **
04508> *****
04509>
04510> | CALIB NASHYD | Area (ha)= 49.50 Curve Number (CN)=84.00
04511> | 01:s101 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04512> |-----| U.H. Tp (hrs)= .840
04513>
04514> Unit Hyd Peak (cms)= 2.251
04515>
04516> PEAK FLOW (cms)= 2.942 (i)
04517> TIME TO PEAK (hrs)= 2.050
04518> RUNOFF VOLUME (mm)= 42.085
04519> TOTAL RAINFALL (mm)= 75.831
04520> RUNOFF COEFFICIENT = .555
04521>
04522> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04523>
04524>
04525> 100:0004-----
04526>
04527> | CALIB NASHYD | Area (ha)= 32.80 Curve Number (CN)=84.00
04528> | 02:s102 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04529> |-----| U.H. Tp (hrs)= .620
04530>
04531> Unit Hyd Peak (cms)= 2.021
04532>
04533> PEAK FLOW (cms)= 2.452 (i)
04534> TIME TO PEAK (hrs)= 1.783
04535> RUNOFF VOLUME (mm)= 42.085
04536> TOTAL RAINFALL (mm)= 75.831
04537> RUNOFF COEFFICIENT = .555
04538>
04539> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04540>
04541>
04542> 100:0005-----
04543>
04544> | CALIB NASHYD | Area (ha)= 8.90 Curve Number (CN)=84.00
04545> | 03:s103 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04546> |-----| U.H. Tp (hrs)= .480
04547>
04548> Unit Hyd Peak (cms)= .708
04549>
04550> PEAK FLOW (cms)= .801 (i)
04551> TIME TO PEAK (hrs)= 1.617
04552> RUNOFF VOLUME (mm)= 42.085
04553> TOTAL RAINFALL (mm)= 75.831
04554> RUNOFF COEFFICIENT = .555
04555>
04556> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04557>
04558>
04559> 100:0006-----
04560>
04561> | CALIB NASHYD | Area (ha)= 33.50 Curve Number (CN)=84.00
04562> | 04:s104 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
04563> |-----| U.H. Tp (hrs)= .720
04564>
04565> Unit Hyd Peak (cms)= 1.777
04566>
04567> PEAK FLOW (cms)= 2.239 (i)
04568> TIME TO PEAK (hrs)= 1.917
04569> RUNOFF VOLUME (mm)= 42.085
04570> TOTAL RAINFALL (mm)= 75.831
04571> RUNOFF COEFFICIENT = .555
04572>

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04573> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04574> -----
04575> 100:0007-----
04576> | ADD HYD (Total ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
04577> |-----|-----|-----|-----|-----|-----|
04580> | ID1 01:S101      |          |          |          |          |
04581> | +ID2 02:S102     |          |          |          |          |
04582> | +ID3 03:S103     |          |          |          |          |
04583> | +ID4 04:S104     |          |          |          |          |
04584> |-----|-----|-----|-----|-----|
04585> | SUM 05:Total     | 124.70  | 8.208   | 1.88   | 42.08  | .000
04586>
04587> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04588> -----
04589> 100:0008-----
04590> *#-----
04591> *# External Pond Sizing, Cas EXT1 and EXT2
04592> *#-----
04593> *#-----
04594> *#-----
04595> *#-----
04596> *#-----
04597> | CALIB STANDHYD   | Area (ha)= 9.50
04598> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04599> -----
04600>
04601> IMPERVIOUS      PERVIOUS (i)
04602> Surface Area (ha)= 5.22      4.27
04603> Dep. Storage (mm)= 2.00      5.00
04604> Average Slope (%)= 1.00      1.00
04605> Length (m)= 400.00          40.00
04606> Mannings n = .013          .240
04607>
04608> Max.eff.Inten.(mm/hr)= 232.24  134.99
04609> over (min) 4.00 12.00
04610> Storage Coeff. (min)= 4.19 (ii) 11.71 (ii)
04611> Unit Hyd. Tpeak (min)= 4.00 12.00
04612> Unit Hyd. peak (cms)= .27 .10
04613>
04614> PEAK FLOW (cms)= 2.05 1.00 *TOTALS*
04615> TIME TO PEAK (hrs)= 1.03 1.20 2.510 (iii)
04616> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
04617> TOTAL RAINFALL (mm)= 75.83 75.83 75.831
04618> RUNOFF COEFFICIENT = .97 .64 .792
04619>
04620> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04621> CN* = 86.0 Ia = Dep. Storage (Above)
04622> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04623> THAN THE STORAGE COEFFICIENT.
04624> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04625> -----
04626> 100:0009-----
04627> | CALIB STANDHYD   | Area (ha)= 23.00
04628> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04629> -----
04630>
04631> IMPERVIOUS      PERVIOUS (i)
04632> Surface Area (ha)= 12.65     10.35
04633> Dep. Storage (mm)= 2.00      5.00
04634> Average Slope (%)= 1.00      1.00
04635> Length (m)= 750.00          40.00
04636> Mannings n = .013          .240
04637>
04638> Max.eff.Inten.(mm/hr)= 213.27  125.44
04639> over (min) 6.00 14.00
04640> Storage Coeff. (min)= 6.32 (ii) 14.07 (ii)
04641> Unit Hyd. Tpeak (min)= 6.00 14.00
04642> Unit Hyd. peak (cms)= .18 .08
04643>
04644> PEAK FLOW (cms)= 4.21 2.19 *TOTALS*
04645> TIME TO PEAK (hrs)= 1.07 1.25 5.435 (iii)
04646> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
04647> TOTAL RAINFALL (mm)= 75.83 75.83 75.831
04648> RUNOFF COEFFICIENT = .97 .64 .792
04649>
04650> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04651> CN* = 86.0 Ia = Dep. Storage (Above)
04652> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04653> THAN THE STORAGE COEFFICIENT.
04654> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04655> -----
04656> 100:0010-----
04657> | ADD HYD (ExPondIn ) | ID: NHYD      AREA   QPEAK   TPEAK   R.V.   DWF
04658> |-----|-----|-----|-----|-----|
04661> | ID1 01:EXT2      |          |          |          |          |
04662> | +ID2 02:EXT1     |          |          |          |          |
04663> |-----|-----|-----|-----|-----|
04664> | SUM 03:ExPondIn  | 32.50  | 7.863   | 1.08   | 60.04  | .000
04665>
04666> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04667> -----
04668> 100:0011-----
04669> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04670> | IN>03:(ExPond) |
04671> | OUT<10:(ExPond) |
04672> |-----|-----|-----|-----|-----|
04673> |=====|=====|=====|=====|=====|
04674> | OUTFLOW | STORAGE | OUTFLOW | STORAGE |
04675> | (cms) | (ha.m.) | (cms) | (ha.m.) |
04676> | .530 | .4500E+00 | .000 | .0000E+00 |
04677>
04678> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04679> (ha) (cms) (hrs) (mm)
04680> INFLOW >03: (ExPond) 32.50 7.863 1.083 60.037
04681> OUTFLOW <10: (ExPond) 32.50 2.176 1.683 60.036
04682>
04683> PEAK FLOW REDUCTION [Qout/Qin] (%) = 27.676
04684> TIME SHIFT OF PEAK FLOW (min) = 36.00
04685> MAXIMUM STORAGE USED (ha.m.) = .1103E+01
04686> -----
04687> 100:0012-----
04688> *#-----
04689> *# Pond 1 Sizing, Cas 100
04690> *#-----
04691> *#-----
04692> *#-----
04693> *#-----
04694> *#-----
04695> | CALIB STANDHYD   | Area (ha)= 4.08
04696> | 01:100 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04697> -----
04698>
04699> IMPERVIOUS      PERVIOUS (i)

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04700> Surface Area (ha)= 2.24 1.84
04701> Dep. Storage (mm)= 2.00 5.00
04702> Average Slope (%)= 1.00 1.00
04703> Length (m)= 300.00 40.00
04704> Mannings n = .013 .240
04705>
04706> Max.eff.Inten.(mm/hr)= 232.24 141.12
04707> over (min) 4.00 11.00
04708> Storage Coeff. (min)= 3.53 (ii) 10.91 (ii)
04709> Unit Hyd. Tpeak (min)= 4.00 11.00
04710> Unit Hyd. peak (cms)= .31 .10
04711>
04712> PEAK FLOW (cms)= .92 .45 *TOTALS*
04713> TIME TO PEAK (hrs)= 1.03 1.18 1.050
04714> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
04715> TOTAL RAINFALL (mm)= 75.83 75.83 75.831
04716> RUNOFF COEFFICIENT = .97 .64 .792
04717>
04718> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04719> CN* = 86.0 Ia = Dep. Storage (Above)
04720> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04721> THAN THE STORAGE COEFFICIENT.
04722> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04723> -----
04724> 100:0013-----
04725> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04726> | IN>01:(100 ) |
04727> | OUT<09:(Pond1) |
04728> |-----|-----|-----|-----|-----|
04729> |=====|=====|=====|=====|=====|
04730> | OUTFLOW | STORAGE | OUTFLOW | STORAGE |
04731> | (cms) | (ha.m.) | (cms) | (ha.m.) |
04732> | .000 | .0000E+00 | .300 | .2000E+00 |
04733> | .070 | .7000E-01 | .000 | .0000E+00 |
04734>
04735> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04736> (ha) (cms) (hrs) (mm)
04737> INFLOW >01: (100 ) 4.08 1.139 1.050 60.037
04738> OUTFLOW <09: (Pond1) 4.08 .217 1.717 60.036
04739>
04740> PEAK FLOW REDUCTION [Qout/Qin] (%) = 19.094
04741> TIME SHIFT OF PEAK FLOW (min) = 40.00
04742> MAXIMUM STORAGE USED (ha.m.) = .1533E+00
04743> -----
04744> 100:0014-----
04745> *#-----
04746> *# Pond 2 Sizing, Cas 200
04747> *#-----
04748> *#-----
04749> *#-----
04750> *#-----
04751> | CALIB STANDHYD   | Area (ha)= 7.53
04752> | 01:200 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04753> -----
04754>
04755> IMPERVIOUS      PERVIOUS (i)
04756> Surface Area (ha)= 4.14 3.39
04757> Dep. Storage (mm)= 2.00 5.00
04758> Average Slope (%)= 1.00 1.00
04759> Length (m)= 550.00          40.00
04760> Mannings n = .013          .240
04761>
04762> Max.eff.Inten.(mm/hr)= 232.24  129.83
04763> over (min) 5.00 13.00
04764> Storage Coeff. (min)= 5.07 (ii) 12.71 (ii)
04765> Unit Hyd. Tpeak (min)= 5.00 13.00
04766> Unit Hyd. peak (cms)= .22 .09
04767>
04768> PEAK FLOW (cms)= 1.50 .76 *TOTALS*
04769> TIME TO PEAK (hrs)= 1.05 1.22 1.890 (iii)
04770> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
04771> TOTAL RAINFALL (mm)= 75.83 75.83 75.831
04772> RUNOFF COEFFICIENT = .97 .64 .792
04773>
04774> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04775> CN* = 86.0 Ia = Dep. Storage (Above)
04776> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04777> THAN THE STORAGE COEFFICIENT.
04778> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04779> -----
04780> 100:0015-----
04781> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04782> | IN>01:(200 ) |
04783> | OUT<08:(Pond2) |
04784> |-----|-----|-----|-----|-----|
04785> |=====|=====|=====|=====|=====|
04786> | OUTFLOW | STORAGE | OUTFLOW | STORAGE |
04787> | (cms) | (ha.m.) | (cms) | (ha.m.) |
04788> | .000 | .0000E+00 | .560 | .3000E+00 |
04789> | .120 | .1500E+00 | .000 | .0000E+00 |
04790>
04791> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04792> (ha) (cms) (hrs) (mm)
04793> INFLOW >01: (200 ) 7.53 1.890 1.067 60.037
04794> OUTFLOW <08: (Pond2) 7.53 .475 1.683 60.036
04795>
04796> PEAK FLOW REDUCTION [Qout/Qin] (%) = 25.133
04797> TIME SHIFT OF PEAK FLOW (min) = 37.00
04798> MAXIMUM STORAGE USED (ha.m.) = .2710E+00
04799> -----
04800> 100:0016-----
04801> *#-----
04802> *# Pond 3 Sizing, Cas 300, 301 and 302
04803> *#-----
04804> *#-----
04805> *#-----
04806> *#-----
04807> *#-----
04808> | CALIB STANDHYD   | Area (ha)= 10.33
04809> | 01:300 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04810> -----
04811>
04812> IMPERVIOUS      PERVIOUS (i)
04813> Surface Area (ha)= 5.68 4.65
04814> Dep. Storage (mm)= 2.00 5.00
04815> Average Slope (%)= 1.00 1.00
04816> Length (m)= 610.00          40.00
04817> Mannings n = .013          .240
04818>
04819> Max.eff.Inten.(mm/hr)= 232.24  129.83
04820> over (min) 5.00 13.00
04821> Storage Coeff. (min)= 5.40 (ii) 13.04 (ii)
04822> Unit Hyd. Tpeak (min)= 5.00 13.00
04823> Unit Hyd. peak (cms)= .21 .09
04824>
04825> PEAK FLOW (cms)= 2.02 1.03 *TOTALS*
04826> TIME TO PEAK (hrs)= 1.05 1.23 1.067
04827> RUNOFF VOLUME (mm)= 73.83 48.75 60.037

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04827> TOTAL RAINFALL (mm)= 75.83 75.83 75.831
04828> RUNOFF COEFFICIENT = .97 .64 .792
04829>
04830> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04831> CN* = 86.0 Ia = Dep. Storage (Above)
04832> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04833> THAN THE STORAGE COEFFICIENT.
04834> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04835>
-----
04837> 100:0017-----
04838>
04839> | CALIB STANDHYD | Area (ha)= 4.18
04840> | 02:302 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04841>
04842>
04843> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
04844> Dep. Storage (mm)= 2.00 5.00
04845> Average Slope (%)= 1.00 1.00
04846> Length (m)= 210.00 40.00
04847> Mannings n = .013 .240
04848>
04849> Max.eff.Inten.(mm/hr)= 232.24 148.53
04850> over (min)= 3.00 10.00
04851> Storage Coeff. (min)= 2.85 (ii) 10.08 (ii)
04852> Unit Hyd. Tpeak (min)= 3.00 10.00
04853> Unit Hyd. peak (cms)= .39 .11
04854>
04855> PEAK FLOW (cms)= 1.02 .48 *TOTALS*
04856> TIME TO PEAK (hrs)= 1.02 1.17 1.232 (iii)
04857> RUNOFF VOLUME (mm)= 73.83 48.75 1.017
04858> TOTAL RAINFALL (mm)= 75.83 48.75 60.037
04859> RUNOFF COEFFICIENT = .97 .64 .792
04860>
04861> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04862> CN* = 86.0 Ia = Dep. Storage (Above)
04863> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04864> THAN THE STORAGE COEFFICIENT.
04865> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04866>
-----
04867> 100:0018-----
04868>
04869> | CALIB NASHYD | Area (ha)= 4.37 Curve Number (CN)=76.00
04870> | 03:301 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
04871> | U.H. Tp(hrs)= .410
04872>
04873>
04874> Unit Hyd Qpeak (cms)= .407
04875>
04876> PEAK FLOW (cms)= .339 (i)
04877> TIME TO PEAK (hrs)= 1.533
04878> RUNOFF VOLUME (mm)= 33.216
04879> TOTAL RAINFALL (mm)= 75.831
04880> RUNOFF COEFFICIENT = .438
04881>
04882> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04883>
-----
04884> 100:0019-----
04885>
04886> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
04887> | ID1 01:300 10.33 2.549 1.07 60.04 .000
04888> | +ID2 02:302 4.18 1.232 1.02 60.04 .000
04889> | +ID3 03:301 4.37 339 1.53 33.22 .000
04890>
04891>
04892>
04893> SUM 04:Pond3In 18.88 3.749 1.08 53.83 .000
04894>
04895> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04896>
-----
04897> 100:0020-----
04898>
04899> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04900> | IN<04:(Pond3I) |
04901> | OUT<07:(Pond3) |
04902> | ===== OUTFLOW STORAGE TABLE =====
04903> | OUTFLOW STORAGE | OUTFLOW STORAGE
04904> | (cms) (ha.m.) | (cms) (ha.m.)
04905> | .000 .0000E+00 | 1.400 .5800E+00
04906> | .310 .2500E+00 | .000 .0000E+00
04907>
04908>
04909> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04910> (ha) (cms) (hrs) (mm)
04911> INFLOW >04: (Pond3I) 18.88 3.749 1.083 53.829
04912> OUTFLOW<07: (Pond3) 18.88 1.216 1.683 53.829
04913>
04914> PEAK FLOW REDUCTION [Qout/Qin] (%) = 32.437
04915> TIME SHIFT OF PEAK FLOW (min) = 36.00
04916> MAXIMUM STORAGE USED (ha.m.) = 5243E+00
04917>
-----
04918> 100:0021-----
04919> *#*****
04920> *#
04921> *# Pond 4 Sizing, CAs 400, 401 and 402
04922> *#
04923> *#*****
04924>
04925> | CALIB STANDHYD | Area (ha)= 10.47
04926> | 01:402 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04927>
04928>
04929> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
04930> Dep. Storage (mm)= 2.00 5.00
04931> Average Slope (%)= 1.00 1.00
04932> Length (m)= 350.00 40.00
04933> Mannings n = .013 .240
04934>
04935> Max.eff.Inten.(mm/hr)= 232.24 141.12
04936> over (min)= 4.00 11.00
04937> Storage Coeff. (min)= 3.87 (ii) 11.25 (ii)
04938> Unit Hyd. Tpeak (min)= 4.00 11.00
04939> Unit Hyd. peak (cms)= .29 .10
04940>
04941> PEAK FLOW (cms)= 2.31 1.13 *TOTALS*
04942> TIME TO PEAK (hrs)= 1.03 1.18 2.872 (iii)
04943> RUNOFF VOLUME (mm)= 73.83 48.75 1.050
04944> TOTAL RAINFALL (mm)= 75.83 48.75 60.037
04945> RUNOFF COEFFICIENT = .97 .64 .792
04946>
04947> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04948> CN* = 86.0 Ia = Dep. Storage (Above)
04949> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04950> THAN THE STORAGE COEFFICIENT.
04951> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04952>
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04953>

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04954> 100:0022-----
04955>
04956> | CALIB STANDHYD | Area (ha)= 3.22
04957> | 02:401 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04958>
04959>
04960> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
04961> Dep. Storage (mm)= 2.00 5.00
04962> Average Slope (%)= 1.00 1.00
04963> Length (m)= 250.00 40.00
04964> Mannings n = .013 .240
04965>
04966> Max.eff.Inten.(mm/hr)= 232.24 148.53
04967> over (min)= 3.00 10.00
04968> Storage Coeff. (min)= 3.16 (ii) 10.40 (ii)
04969> Unit Hyd. Tpeak (min)= 3.00 10.00
04970> Unit Hyd. peak (cms)= .36 .11
04971>
04972> PEAK FLOW (cms)= .77 .36 *TOTALS*
04973> TIME TO PEAK (hrs)= 1.02 1.17 1.033
04974> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
04975> TOTAL RAINFALL (mm)= 75.83 48.75 75.831
04976> RUNOFF COEFFICIENT = .97 .64 .792
04977>
04978> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
04979> CN* = 86.0 Ia = Dep. Storage (Above)
04980> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04981> THAN THE STORAGE COEFFICIENT.
04982> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04983>
-----
04984> 100:0023-----
04985>
04986>
04987> | CALIB STANDHYD | Area (ha)= 5.25
04988> | 03:400 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
04989>
04990>
04991> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
04992> Dep. Storage (mm)= 2.00 5.00
04993> Average Slope (%)= 1.00 1.00
04994> Length (m)= 250.00 40.00
04995> Mannings n = .013 .240
04996>
04997> Max.eff.Inten.(mm/hr)= 232.24 148.53
04998> over (min)= 3.00 10.00
04999> Storage Coeff. (min)= 3.16 (ii) 10.40 (ii)
05000> Unit Hyd. Tpeak (min)= 3.00 10.00
05001> Unit Hyd. peak (cms)= .36 .11
05002>
05003> PEAK FLOW (cms)= 1.25 .59 *TOTALS*
05004> TIME TO PEAK (hrs)= 1.02 1.17 1.515 (iii)
05005> RUNOFF VOLUME (mm)= 73.83 48.75 60.037
05006> TOTAL RAINFALL (mm)= 75.83 48.75 75.831
05007> RUNOFF COEFFICIENT = .97 .64 .792
05008>
05009> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05010> CN* = 86.0 Ia = Dep. Storage (Above)
05011> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05012> THAN THE STORAGE COEFFICIENT.
05013> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05014>
-----
05015> 100:0024-----
05016>
05017> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
05018> | ID1 01:402 10.47 2.872 1.05 60.04 .000
05019> | +ID2 02:401 3.22 .929 1.03 60.04 .000
05020> | +ID3 03:400 5.25 1.515 1.03 60.04 .000
05021>
05022>
05023>
05024> SUM 04:Pond4In 18.94 5.291 1.03 60.04 .000
05025>
05026> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05027>
-----
05028> 100:0025-----
05029>
05030> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05031> | IN<04:(Pond4I) |
05032> | OUT<06:(Pond4 ) |
05033> | ===== OUTFLOW STORAGE TABLE =====
05034> | OUTFLOW STORAGE | OUTFLOW STORAGE
05035> | (cms) (ha.m.) | (cms) (ha.m.)
05036> | .000 .0000E+00 | 1.400 .7000E+00
05037> | .310 .3000E+00 | .000 .0000E+00
05038>
05039>
05040> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05041> (ha) (cms) (hrs) (mm)
05042> INFLOW >04: (Pond4I) 18.94 5.291 1.033 60.037
05043> OUTFLOW<06: (Pond4 ) 18.94 1.290 1.600 60.036
05044>
05045> PEAK FLOW REDUCTION [Qout/Qin] (%) = 24.379
05046> TIME SHIFT OF PEAK FLOW (min) = 34.00
05047> MAXIMUM STORAGE USED (ha.m.) = 6597E+00
05048>
-----
05049> 100:0026-----
05050> *#*****
05051> *#
05052> *# Pond 5 Sizing, CAs 500, 501 and 502
05053> *#
05054> *#*****
05055>
05056> | CALIB STANDHYD | Area (ha)= 2.93
05057> | 01:501 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05058>
05059>
05060> Surface Area (ha)= IMPERVIOUS PERVIOUS (i)
05061> Dep. Storage (mm)= 1.61 1.32
05062> Average Slope (%)= 1.00 1.00
05063> Length (m)= 250.00 40.00
05064> Mannings n = .013 .240
05065>
05066> Max.eff.Inten.(mm/hr)= 232.24 148.53
05067> over (min)= 3.00 10.00
05068> Storage Coeff. (min)= 3.16 (ii) 10.40 (ii)
05069> Unit Hyd. Tpeak (min)= 3.00 10.00
05070> Unit Hyd. peak (cms)= .36 .11
05071>
05072> PEAK FLOW (cms)= .70 .33 *TOTALS*
05073> TIME TO PEAK (hrs)= 1.02 1.17 .846 (iii)
05074> RUNOFF VOLUME (mm)= 73.83 48.75 1.033
05075> TOTAL RAINFALL (mm)= 75.83 48.75 60.037
05076> RUNOFF COEFFICIENT = .97 .64 .792
05077>
05078> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05079> CN* = 86.0 Ia = Dep. Storage (Above)
05080> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

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05081>          THAN THE STORAGE COEFFICIENT.
05082>          (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05083>
05084>
-----
05085> 100:0027-----
05086>
05087> | CALIB STANDHYD | Area (ha)= 3.14
05088> | 02:500 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05089>
05090>          IMPERVIOUS      PERVIOUS (i)
05091> Surface Area (ha)= 1.73      1.41
05092> Dep. Storage (mm)= 2.00      5.00
05093> Average Slope (%)= 1.00      1.00
05094> Length (m)= 250.00      40.00
05095> Mannings n = .013      .240
05096>
05097> Max.eff.Inten.(mm/hr)= 232.24 148.53
05098> over (min) = 3.00      10.00
05099> Storage Coeff. (min)= 3.16 (ii) 10.40 (ii)
05100> Unit Hyd. Tpeak (min)= 3.00      10.00
05101> Unit Hyd. peak (cms)= .36      .11
05102>
05103>          *TOTALS*
05104> PEAK FLOW (cms)= .75      .35      .906 (iii)
05105> TIME TO PEAK (hrs)= 1.02      1.17      1.033
05106> RUNOFF VOLUME (mm)= 73.83      48.75      60.037
05107> TOTAL RAINFALL (mm)= 75.83      75.83      75.831
05108> RUNOFF COEFFICIENT = .97      .64      .792
05109>
05110>          (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05111>          CN* = 86.0 Ia = Dep. Storage (Above)
05112>          (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05113>          THAN THE STORAGE COEFFICIENT.
05114>          (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05115>
-----
05116> 100:0028-----
05117>
05118> | CALIB STANDHYD | Area (ha)= 5.45
05119> | 03:502 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05120>
05121>          IMPERVIOUS      PERVIOUS (i)
05122> Surface Area (ha)= 3.00      2.45
05123> Dep. Storage (mm)= 2.00      5.00
05124> Average Slope (%)= 1.00      1.00
05125> Length (m)= 600.00      40.00
05126> Mannings n = .013      .240
05127>
05128> Max.eff.Inten.(mm/hr)= 232.24 129.83
05129> over (min) = 5.00      13.00
05130> Storage Coeff. (min)= 5.34 (ii) 12.98 (ii)
05131> Unit Hyd. Tpeak (min)= 5.00      13.00
05132> Unit Hyd. peak (cms)= .22      .09
05133>
05134>          *TOTALS*
05135> PEAK FLOW (cms)= 1.07      .54      1.349 (iii)
05136> TIME TO PEAK (hrs)= 1.05      1.23      1.067
05137> RUNOFF VOLUME (mm)= 73.83      48.75      60.037
05138> TOTAL RAINFALL (mm)= 75.83      75.83      75.831
05139> RUNOFF COEFFICIENT = .97      .64      .792
05140>
05141>          (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05142>          CN* = 86.0 Ia = Dep. Storage (Above)
05143>          (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05144>          THAN THE STORAGE COEFFICIENT.
05145>          (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05146>
-----
05147> 100:0029-----
05148>
05149> | ADD HYD (Pond5In ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
05150> |-----|-----|-----|-----|-----|-----|
05151> | ID1 01:501 | (ha) (cms) (hrs) (mm) (cms)
05152> | +ID2 02:500 | 3.14 .906 1.03 60.04 .000
05153> | +ID3 03:502 | 5.45 1.349 1.07 60.04 .000
05154> |-----|-----|-----|-----|-----|
05155> | SUM 04:Pond5In | 11.52 3.013 1.03 60.04 .000
05156>
05157>          NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05158>
-----
05160> 100:0030-----
05161>
05162> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05163> | INP04:(Pond5I) |
05164> | OUTP05:(Pond5 ) |
05165> ----- OUTFLOW STORAGE TABLE -----
05166> OUTFLOW STORAGE | OUTFLOW STORAGE
05167> (cms) (ha.m.) | (cms) (ha.m.)
05168> .000 .0000E+00 | .850 .5000E+00
05169> .190 .2300E+00 | .000 .0000E+00
05170>
05171>          ROUTING RESULTS
05172>          AREA QPEAK TPEAK R.V.
05173>          (ha) (cms) (hrs) (mm)
05174> INFLOW >04: (Pond5I) 11.52 3.013 1.033 60.037
05175> OUTFLOW<05: (Pond5 ) 11.52 .670 1.700 60.036
05176>
05177>          PEAK FLOW REDUCTION [Qout/Qin] (%) = 22.236
05178>          TIME SHIFT OF PEAK FLOW (min) = 40.00
05179>          MAXIMUM STORAGE USED (ha.m.) = .4263E+00
05180>
-----
05181> 100:0031-----
05182> *#
05183> *# EXT3 Sizing, CAS EXT3
05184> *#
05185> *#-----
05186>
05187> | CALIB STANDHYD | Area (ha)= 9.16
05188> | 01:EXT3 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05189>
05190>          IMPERVIOUS      PERVIOUS (i)
05191> Surface Area (ha)= 5.04      4.12
05192> Dep. Storage (mm)= 2.00      5.00
05193> Average Slope (%)= 1.00      1.00
05194> Length (m)= 400.00      40.00
05195> Mannings n = .013      .240
05196>
05197> Max.eff.Inten.(mm/hr)= 232.24 134.99
05198> over (min) = 4.00      12.00
05199> Storage Coeff. (min)= 4.19 (ii) 11.71 (ii)
05200> Unit Hyd. Tpeak (min)= 4.00      12.00
05201> Unit Hyd. peak (cms)= .27      .10
05202>
05203>          *TOTALS*
05204> PEAK FLOW (cms)= 1.97      .97      2.420 (iii)
05205> TIME TO PEAK (hrs)= 1.03      1.20      1.050
05206> RUNOFF VOLUME (mm)= 73.83      48.75      60.037
05207> TOTAL RAINFALL (mm)= 75.83      75.83      75.831
05208> RUNOFF COEFFICIENT = .97      .64      .792

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05209>          (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05210>          CN* = 86.0 Ia = Dep. Storage (Above)
05211>          (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05212>          THAN THE STORAGE COEFFICIENT.
05213>          (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05214>
-----
05215> 100:0032-----
05216>
05217>          COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
05218> TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
05219> Total minor system capacity = .150 (cms)
05220> Total major system storage [TMJSTO] = 5000.(cu.m.)
05221>
05222>
05223>          ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
05224> (ha) (cms) (hrs) (mm) (cms)
05225> TOTAL HYD. 01:EXT3 9.16 2.420 1.050 60.037 .000
05226>
05227> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
05228> MINOR SYST 03:MinorE 9.16 .150 .667 60.102 .000
05229>
05230>          NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05231>
05232>          Maximum MAJOR SYSTEM storage used = 4098.(cu.m.)
05233>
-----
05234> 100:0033-----
05235> *#
05236> *#-----
05237> *# Flow Totals and Channel Runoff
05238> *#
05239> *#-----
05240> *#-----
05241>
05242> | ADD HYD (Control ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
05243> (ha) (cms) (hrs) (mm) (cms)
05244> ID1 02:noFlow .00 .000 .00 .00 .000
05245> +ID2 03:MinorEXT3 9.16 .150 .67 60.10 .000
05246> +ID3 05:Pond5 11.52 .670 1.70 60.04 .000
05247> +ID4 06:Pond4 18.94 1.290 1.60 60.04 .000
05248> +ID5 07:Pond3 18.88 1.216 1.68 53.83 .000
05249> +ID6 08:Pond2 7.53 .475 1.68 60.04 .000
05250> +ID7 09:Pond1 4.08 .217 1.72 60.04 .000
05251> +ID8 10:ExtPond 32.50 2.176 1.68 60.04 .000
05252>
05253> SUM 01:Control 102.61 6.187 1.67 58.90 .000
05254>
05255>          NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05256>
-----
05257> 100:0034-----
05258>
05259>
05260> | CALIB NASHYD | Area (ha)= .99 Curve Number (CN)=68.00
05261> | 02:600 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
05262> | U.H. Tp(hrs)= .350
05263>
05264>          Unit Hyd Qpeak (cms)= .108
05265>
05266>          PEAK FLOW (cms)= .066 (i)
05267>          TIME TO PEAK (hrs)= 1.467
05268>          RUNOFF VOLUME (mm)= 26.355
05269>          TOTAL RAINFALL (mm)= 75.831
05270>          RUNOFF COEFFICIENT = .348
05271>
05272>          (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05273>
-----
05274> 100:0035-----
05275>
05276>
05277> | CALIB NASHYD | Area (ha)= 3.54 Curve Number (CN)=68.00
05278> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
05279> | U.H. Tp(hrs)= .590
05280>
05281>          Unit Hyd Qpeak (cms)= .229
05282>
05283>          PEAK FLOW (cms)= .166 (i)
05284>          TIME TO PEAK (hrs)= 1.783
05285>          RUNOFF VOLUME (mm)= 26.355
05286>          TOTAL RAINFALL (mm)= 75.831
05287>          RUNOFF COEFFICIENT = .348
05288>
05289>          (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05290>
-----
05291> 100:0036-----
05292>
05293>
05294> | CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
05295> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
05296> | U.H. Tp(hrs)= .970
05297>
05298>          Unit Hyd Qpeak (cms)= .142
05299>
05300>          PEAK FLOW (cms)= .118 (i)
05301>          TIME TO PEAK (hrs)= 2.250
05302>          RUNOFF VOLUME (mm)= 26.355
05303>          TOTAL RAINFALL (mm)= 75.831
05304>          RUNOFF COEFFICIENT = .348
05305>
05306>          (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05307>
-----
05308> 100:0037-----
05309>
05310>
05311> | ADD HYD (PostTot ) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
05312> (ha) (cms) (hrs) (mm) (cms)
05313> ID1 01:Control 102.61 6.187 1.67 58.90 .000
05314> +ID2 02:600 .99 .066 1.47 26.36 .000
05315> +ID3 03:601 3.54 .166 1.78 26.36 .000
05316> +ID4 04:602 3.61 .118 2.25 26.36 .000
05317>
05318> SUM 05:PostTot 110.75 6.493 1.68 56.51 .000
05319>
05320>          NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05321>
-----
05322> 100:0038-----
05323>
05324>
05325> 100:0002-----
05326>
05327> 100:0002-----
05328>
05329> 100:0002-----
05330>
05331> 100:0002-----
05332>
05333> 100:0002-----
05334> ** END OF RUN : 249

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05335>
05336> *****
05337>
05338>
05339>
05340>
05341>
05342>
05343> | START | Project dir.: C:\MODELL-1\14170\SWMHYMO\
05344> | TZERO = 00 hrs on | Rainfall dir.: C:\MODELL-1\14170\SWMHYMO\
05345> | METOUT= 2 (output = METRIC)
05346> | NRUN = 250
05347> | NSTORM= 1
05348> | # 1=1dn250YR.3hr
05349>
05350>
05351> 250:0002
05352> *****
05353> *# Project Name: [Col Talbot Complete Corridor] Project Number: [161414170]
05354> *# Date : 2022-11-14
05355> *# Modeller : [AKK]
05356> *# Company : Stantec Consulting Ltd. (London)
05357> *# License # : 4730904
05358> *****
05359> *#
05360> *#
05361> *# This model represents the hydrologic characteristics of the existing and
05362> *# proposed conditions in the proposed subdivision.
05363> *# Storm events modeled are:
05364> *# 2YR, 5YR, 10YR, 25YR, 50YR, 100YR and 250YR 3hr Chicago STORMS (London, ONT.
05365> *#
05366> *****
05367>
05368> 250:0002
05369>
05370> | READ STORM | Filename: 250-yr, 3hr Chicago Storm from London ID
05371> | Ptotal= 86.60 mm | Comments: 250-yr, 3hr Chicago Storm from London ID
05372>
05373>
05374>
05375>
05376>
05377>
05378>
05379>
05380>
05381>
05382>
05383>
05384>
05385>
05386> 250:0003
05387> *****
05388> *#
05389> *# Existing Conditions to determine target release rates
05390> *#
05391> *****
05392>
05393> | CALIB NASHYD | Area (ha)= 49.50 | Curve Number (CN)=84.00
05394> | 01:S101 DT= 1.00 | Ia (mm)= 5.000 | # of Linear Res. (N)= 3.00
05395> | U.H. Tp(hrs)= .840
05396>
05397> Unit Hyd Qpeak (cms)= 2.251
05398>
05399> PEAK FLOW (cms)= 3.621 (i)
05400> TIME TO PEAK (hrs)= 2.033
05401> RUNOFF VOLUME (mm)= 51.229
05402> TOTAL RAINFALL (mm)= 86.603
05403> RUNOFF COEFFICIENT = .592
05404>
05405> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05406>
05407>
05408> 250:0004
05409>
05410> | CALIB NASHYD | Area (ha)= 32.80 | Curve Number (CN)=84.00
05411> | 02:S102 DT= 1.00 | Ia (mm)= 5.000 | # of Linear Res. (N)= 3.00
05412> | U.H. Tp(hrs)= .620
05413>
05414> Unit Hyd Qpeak (cms)= 2.021
05415>
05416> PEAK FLOW (cms)= 3.028 (i)
05417> TIME TO PEAK (hrs)= 1.767
05418> RUNOFF VOLUME (mm)= 51.229
05419> TOTAL RAINFALL (mm)= 86.603
05420> RUNOFF COEFFICIENT = .592
05421>
05422> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05423>
05424>
05425> 250:0005
05426>
05427> | CALIB NASHYD | Area (ha)= 8.90 | Curve Number (CN)=84.00
05428> | 03:S103 DT= 1.00 | Ia (mm)= 5.000 | # of Linear Res. (N)= 3.00
05429> | U.H. Tp(hrs)= .480
05430>
05431> Unit Hyd Qpeak (cms)= .708
05432>
05433> PEAK FLOW (cms)= .993 (i)
05434> TIME TO PEAK (hrs)= 1.600
05435> RUNOFF VOLUME (mm)= 51.229
05436> TOTAL RAINFALL (mm)= 86.603
05437> RUNOFF COEFFICIENT = .592
05438>
05439> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05440>
05441>
05442> 250:0006
05443>
05444> | CALIB NASHYD | Area (ha)= 33.50 | Curve Number (CN)=84.00
05445> | 04:S104 DT= 1.00 | Ia (mm)= 5.000 | # of Linear Res. (N)= 3.00
05446> | U.H. Tp(hrs)= .720
05447>
05448> Unit Hyd Qpeak (cms)= 1.777
05449>
05450> PEAK FLOW (cms)= 2.760 (i)
05451> TIME TO PEAK (hrs)= 1.900
05452> RUNOFF VOLUME (mm)= 51.229
05453> TOTAL RAINFALL (mm)= 86.603
05454> RUNOFF COEFFICIENT = .592
05455>
05456> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05457>
05458>
05459>
05460>
05461> | ADD HYD (Total ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

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05462> ----- (ha) (cms) (hrs) (mm) (cms)
05463> ID1 01:S101 49.50 3.621 2.03 51.23 .000
05464> +ID2 02:S102 32.80 3.028 1.77 51.23 .000
05465> +ID3 03:S103 8.90 .993 1.60 51.23 .000
05466> +ID4 04:S104 33.50 2.760 1.90 51.23 .000
05467> =====
05468> SUM 05:Total 124.70 10.121 1.87 51.23 .000
05469>
05470> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05471>
05472>
05473> 250:0008
05474> *****
05475> *#
05476> *# External Pond Sizing, CAs EXT1 and EXT2
05477> *#
05478> *****
05479>
05480> | CALIB STANDHYD | Area (ha)= 9.50
05481> | 01:EXT2 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05482>
05483>
05484> IMPERVIOUS PERVIOUS (i)
05485> Surface Area (ha)= 5.22 4.27
05486> Dep. Storage (mm)= 2.00 5.00
05487> Average Slope (%)= 1.00 1.00
05488> Length (m)= 400.00 40.00
05489> Mannings n = .013 .240
05490>
05491> Max.eff.Inten.(mm/hr)= 274.73 174.76
05492> over (min) 4.00 11.00
05493> Storage Coeff. (min)= 3.92 (ii) 10.70 (ii)
05494> Unit Hyd. Tpeak (min)= 4.00 11.00
05495> Unit Hyd. peak (cms)= .29 .10
05496>
05497> PEAK FLOW (cms)= 2.46 1.30 3.129 (iii)
05498> TIME TO PEAK (hrs)= 1.03 1.17 1.050
05499> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05500> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05501> RUNOFF COEFFICIENT = .98 .68
05502>
05503> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05504> CN* = 86.0 Ia = Dep. Storage (Above)
05505> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05506> THAN THE STORAGE COEFFICIENT.
05507> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05508>
05509> 250:0009
05510>
05511> | CALIB STANDHYD | Area (ha)= 23.00
05512> | 02:EXT1 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05513>
05514>
05515> IMPERVIOUS PERVIOUS (i)
05516> Surface Area (ha)= 12.65 10.35
05517> Dep. Storage (mm)= 2.00 5.00
05518> Average Slope (%)= 1.00 1.00
05519> Length (m)= 750.00 40.00
05520> Mannings n = .013 .240
05521>
05522> Max.eff.Inten.(mm/hr)= 251.72 160.16
05523> over (min) 6.00 13.00
05524> Storage Coeff. (min)= 5.92 (ii) 12.94 (ii)
05525> Unit Hyd. Tpeak (min)= 6.00 13.00
05526> Unit Hyd. peak (cms)= .19 .09
05527>
05528> PEAK FLOW (cms)= 5.06 2.84 6.788 (iii)
05529> TIME TO PEAK (hrs)= 1.07 1.22 1.100
05530> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05531> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05532> RUNOFF COEFFICIENT = .98 .68
05533>
05534> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05535> CN* = 86.0 Ia = Dep. Storage (Above)
05536> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05537> THAN THE STORAGE COEFFICIENT.
05538> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05539>
05540> 250:0010
05541>
05542> | ADD HYD (ExPondIn ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
05543> ----- (ha) (cms) (hrs) (mm) (cms)
05544> ID1 01:EXT2 9.50 3.129 1.05 70.26 .000
05545> +ID2 02:EXT1 23.00 6.788 1.10 70.26 .000
05546> =====
05547> SUM 03:ExPondIn 32.50 9.823 1.08 70.26 .000
05548>
05549> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05550>
05551>
05552> 250:0011
05553>
05554> ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05555> | IN>03: (ExPond) |
05556> | OUT<10: (ExPond) | ===== OUTFLOW STORAGE TABLE =====
05557> OUTFLOW STORAGE | OUTFLOW STORAGE
05558> (cms) (ha.m.) | (cms) (ha.m.)
05559> .000 .0000E+00 | 2.420 .1200E+01
05560> .530 .4500E+00 | .000 .0000E+00
05561> *** WARNING: STORAGE-Q values were extrapolated.
05562> Increase curve or use overflow option.
05563>
05564> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05565> (ha) (cms) (hrs) (mm)
05566> INFLOW >03: (ExPond) 32.50 9.823 1.083 70.256
05567> OUTFLOW<10: (ExPond) 32.50 2.661 1.633 70.256
05568>
05569> PEAK FLOW REDUCTION [Qout/Qin] (%) = 27.084
05570> TIME SHIFT OF PEAK FLOW (min) = 33.00
05571> MAXIMUM STORAGE USED (ha.m.) = .1296E+01
05572>
05573>
05574> 250:0012
05575> *****
05576> *#
05577> *# Pond 1 Sizing, CAs 100
05578> *#
05579> *****
05580>
05581> | CALIB STANDHYD | Area (ha)= 4.08
05582> | 01:100 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05583>
05584>
05585> IMPERVIOUS PERVIOUS (i)
05586> Surface Area (ha)= 2.24 1.84
05587> Dep. Storage (mm)= 2.00 5.00
05588> Average Slope (%)= 1.00 1.00
05589> Length (m)= 300.00 40.00

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05589> Mannings n = .013 .240
05590>
05591> Max.eff.Inten.(mm/hr)= 274.73 184.31
05592> over (min) = 3.00 10.00
05593> Storage Coeff. (min)= 3.30 (ii) 9.94 (ii)
05594> Unit Hyd. Tpeak (min)= 3.00 10.00
05595> Unit Hyd. peak (cms)= .35 .11
05596>
05597> PEAK FLOW (cms)= 1.13 .58 1.408 (iii)
05598> TIME TO PEAK (hrs)= 1.02 1.15 1.033
05599> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05600> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05601> RUNOFF COEFFICIENT = .98 .68 .811
05602>
05603> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05604> CN* = 86.0 Ia = Dep. Storage (Above)
05605> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05606> THAN THE STORAGE COEFFICIENT.
05607> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05608>
05609>
05610> 250:0013-----
05611> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05612> | IN<01:(100) |
05613> | OUT<09:(Pond1) |
05614> | ===== OUTFLOW STORAGE TABLE =====
05615> | OUTFLOW STORAGE | OUTFLOW STORAGE
05616> | (cms) (ha.m.) | (cms) (ha.m.)
05617> | .000 .0000E+00 | .300 .2000E+00
05618> | .070 .7000E-01 | .000 .0000E+00
05619>
05620> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05621> (ha) (cms) (hrs) (mm)
05622> INFLOW >01: (100 ) 4.08 1.408 1.033 70.256
05623> OUTFLOW<09: (Pond1) 4.08 .265 1.667 70.256
05624>
05625> PEAK FLOW REDUCTION [Qout/Qin] (%) = 18.783
05626> TIME SHIFT OF PEAK FLOW (min)= 38.00
05627> MAXIMUM STORAGE USED (ha.m.)=.1799E+00
05628>
05629>
05630> 250:0014-----
05631> *#*****
05632> *# Pond 2 Sizing, Cas 200
05633> *#
05634> *#
05635> *#*****
05636>
05637> | CALIB STANDHYD | Area (ha)= 7.53
05638> | 01:200 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05639>
05640> IMPERVIOUS PERVIOUS (i)
05641> Surface Area (ha)= 4.14 3.39
05642> Dep. Storage (mm)= 2.00 5.00
05643> Average Slope (%)= 1.00 1.00
05644> Length (m)= 550.00 40.00
05645> Mannings n = .013 .240
05646>
05647> Max.eff.Inten.(mm/hr)= 274.73 166.83
05648> over (min) = 5.00 12.00
05649> Storage Coeff. (min)= 4.74 (ii) 11.65 (ii)
05650> Unit Hyd. Tpeak (min)= 5.00 12.00
05651> Unit Hyd. peak (cms)= .23 .10
05652>
05653> PEAK FLOW (cms)= 1.80 .98 2.359 (iii)
05654> TIME TO PEAK (hrs)= 1.05 1.20 1.067
05655> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05656> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05657> RUNOFF COEFFICIENT = .98 .68 .811
05658>
05659> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05660> CN* = 86.0 Ia = Dep. Storage (Above)
05661> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05662> THAN THE STORAGE COEFFICIENT.
05663> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05664>
05665>
05666> 250:0015-----
05667> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05668> | IN<01:(200) |
05669> | OUT<08:(Pond2) |
05670> | ===== OUTFLOW STORAGE TABLE =====
05671> | OUTFLOW STORAGE | OUTFLOW STORAGE
05672> | (cms) (ha.m.) | (cms) (ha.m.)
05673> | .000 .0000E+00 | .560 .3000E+00
05674> | .120 .1500E+00 | .000 .0000E+00
05675>
05676> *** WARNING: STORAGE-Q values were extrapolated.
05677> Increase curve or use overflow option.
05678>
05679> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05680> (ha) (cms) (hrs) (mm)
05681> INFLOW >01: (200 ) 7.53 2.359 1.067 70.256
05682> OUTFLOW<08: (Pond2) 7.53 .599 1.633 70.256
05683>
05684> PEAK FLOW REDUCTION [Qout/Qin] (%) = 25.406
05685> TIME SHIFT OF PEAK FLOW (min)= 34.00
05686> MAXIMUM STORAGE USED (ha.m.)=.3134E+00
05687>
05688>
05689> 250:0016-----
05690> *#*****
05691> *# Pond 3 Sizing, Cas 300, 301 and 302
05692> *#
05693> *#*****
05694>
05695> | CALIB STANDHYD | Area (ha)= 10.33
05696> | 01:300 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05697>
05698> IMPERVIOUS PERVIOUS (i)
05699> Surface Area (ha)= 5.69 4.65
05700> Dep. Storage (mm)= 2.00 5.00
05701> Average Slope (%)= 1.00 1.00
05702> Length (m)= 610.00 40.00
05703> Mannings n = .013 .240
05704>
05705> Max.eff.Inten.(mm/hr)= 274.73 166.83
05706> over (min) = 5.00 12.00
05707> Storage Coeff. (min)= 5.05 (ii) 11.96 (ii)
05708> Unit Hyd. Tpeak (min)= 5.00 12.00
05709> Unit Hyd. peak (cms)= .22 .09
05710>
05711> PEAK FLOW (cms)= 2.43 1.33 3.186 (iii)
05712> TIME TO PEAK (hrs)= 1.05 1.20 1.067
05713> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05714> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05715> RUNOFF COEFFICIENT = .98 .68 .811

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05716>
05717> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05718> CN* = 86.0 Ia = Dep. Storage (Above)
05719> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05720> THAN THE STORAGE COEFFICIENT.
05721> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05722>
05723> -----
05724> 250:0017-----
05725>
05726> | CALIB STANDHYD | Area (ha)= 4.18
05727> | 02:302 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05728>
05729> IMPERVIOUS PERVIOUS (i)
05730> Surface Area (ha)= 2.30 1.88
05731> Dep. Storage (mm)= 2.00 5.00
05732> Average Slope (%)= 1.00 1.00
05733> Length (m)= 210.00 40.00
05734> Mannings n = .013 .240
05735>
05736> Max.eff.Inten.(mm/hr)= 274.73 189.26
05737> over (min) = 3.00 9.00
05738> Storage Coeff. (min)= 2.66 (ii) 9.23 (ii)
05739> Unit Hyd. Tpeak (min)= 3.00 9.00
05740> Unit Hyd. peak (cms)= .41 .12
05741>
05742> PEAK FLOW (cms)= 1.22 .62 1.535 (iii)
05743> TIME TO PEAK (hrs)= 1.02 1.13 1.017
05744> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05745> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05746> RUNOFF COEFFICIENT = .98 .68 .811
05747>
05748> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05749> CN* = 86.0 Ia = Dep. Storage (Above)
05750> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05751> THAN THE STORAGE COEFFICIENT.
05752> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05753>
05754>
05755> 250:0018-----
05756>
05757> | CALIB NASHYD | Area (ha)= 4.37 Curve Number (CN)=76.00
05758> | 03:301 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
05759> | U.H. Tp(hrs)= .410
05760>
05761> Unit Hyd Qpeak (cms)= .407
05762>
05763> PEAK FLOW (cms)= .428 (i)
05764> TIME TO PEAK (hrs)= 1.533
05765> RUNOFF VOLUME (mm)= 41.152
05766> TOTAL RAINFALL (mm)= 86.603
05767> RUNOFF COEFFICIENT = .475
05768>
05769> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05770>
05771>
05772> 250:0019-----
05773>
05774> | ADD HYD (Pond3In ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
05775> | (ha) (cms) (hrs) (mm) (cms)
05776> | ID1 01:300 10.33 3.186 1.07 70.26 .000
05777> | +ID2 02:302 4.18 1.535 1.02 70.26 .000
05778> | +ID3 03:301 4.37 .428 1.53 41.15 .000
05779>
05780> SUM 04:Pond3In 18.88 4.688 1.07 63.52 .000
05781>
05782> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05783>
05784>
05785> 250:0020-----
05786>
05787> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05788> | IN<04:(Pond3I) |
05789> | OUT<07:(Pond3) |
05790> | ===== OUTFLOW STORAGE TABLE =====
05791> | OUTFLOW STORAGE | OUTFLOW STORAGE
05792> | (cms) (ha.m.) | (cms) (ha.m.)
05793> | .000 .0000E+00 | 1.400 .5800E+00
05794> | .310 .2500E+00 | .000 .0000E+00
05795>
05796> *** WARNING: STORAGE-Q values were extrapolated.
05797> Increase curve or use overflow option.
05798>
05799> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05800> (ha) (cms) (hrs) (mm)
05801> INFLOW >04: (Pond3I) 18.88 4.688 1.067 63.520
05802> OUTFLOW<07: (Pond3) 18.88 1.504 1.633 63.520
05803>
05804> PEAK FLOW REDUCTION [Qout/Qin] (%) = 32.080
05805> TIME SHIFT OF PEAK FLOW (min)= 34.00
05806> MAXIMUM STORAGE USED (ha.m.)=.6115E+00
05807>
05808>
05809> 250:0021-----
05810> *#*****
05811> *# Pond 4 Sizing, Cas 400, 401 and 402
05812> *#
05813> *#*****
05814>
05815> | CALIB STANDHYD | Area (ha)= 10.47
05816> | 01:402 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05817>
05818> IMPERVIOUS PERVIOUS (i)
05819> Surface Area (ha)= 5.76 4.71
05820> Dep. Storage (mm)= 2.00 5.00
05821> Average Slope (%)= 1.00 1.00
05822> Length (m)= 350.00 40.00
05823> Mannings n = .013 .240
05824>
05825> Max.eff.Inten.(mm/hr)= 274.73 184.31
05826> over (min) = 4.00 10.00
05827> Storage Coeff. (min)= 3.62 (ii) 10.26 (ii)
05828> Unit Hyd. Tpeak (min)= 4.00 10.00
05829> Unit Hyd. peak (cms)= .30 .11
05830>
05831> PEAK FLOW (cms)= 2.77 1.47 3.591 (iii)
05832> TIME TO PEAK (hrs)= 1.03 1.17 1.050
05833> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05834> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05835> RUNOFF COEFFICIENT = .98 .68 .811
05836>
05837> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05838> CN* = 86.0 Ia = Dep. Storage (Above)
05839> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05840> THAN THE STORAGE COEFFICIENT.
05841> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05842>

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05843> 250:0022-----
05844>
05845> | CALIB STANDHYD | Area (ha)= 3.22
05846> | 02:401 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05847> -----
05848>
05849> IMPERVIOUS PERVIOUS (i)
05850> Surface Area (ha)= 1.77 1.45
05851> Dep. Storage (mm)= 2.00 5.00
05852> Average Slope (%)= 1.00 1.00
05853> Length (m)= 250.00 40.00
05854> Mannings n = .013 .240
05855>
05856> Max.eff.Inten.(mm/hr)= 274.73 184.31
05857> over (min) 3.00 10.00
05858> Storage Coeff. (min)= 2.95 (ii) 9.59 (ii)
05859> Unit Hyd. Tpeak (min)= 3.00 10.00
05860> Unit Hyd. peak (cms)= .38 .12
05861>
05862> *TOTALS*
05863> PEAK FLOW (cms)= .92 .47 1.133 (iii)
05864> TIME TO PEAK (hrs)= 1.02 1.15 1.017
05865> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05866> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05867> RUNOFF COEFFICIENT = .98 .68 .811
05868>
05869> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05870> CN* = 86.0 Ia = Dep. Storage (Above)
05871> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05872> THAN THE STORAGE COEFFICIENT.
05873> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05874> -----
05875> 250:0023-----
05876>
05877> | CALIB STANDHYD | Area (ha)= 5.25
05878> | 03:400 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05879> -----
05880>
05881> IMPERVIOUS PERVIOUS (i)
05882> Surface Area (ha)= 2.89 2.36
05883> Dep. Storage (mm)= 2.00 5.00
05884> Average Slope (%)= 1.00 1.00
05885> Length (m)= 250.00 40.00
05886> Mannings n = .013 .240
05887>
05888> Max.eff.Inten.(mm/hr)= 274.73 184.31
05889> over (min) 3.00 10.00
05890> Storage Coeff. (min)= 2.95 (ii) 9.59 (ii)
05891> Unit Hyd. Tpeak (min)= 3.00 10.00
05892> Unit Hyd. peak (cms)= .38 .12
05893>
05894> *TOTALS*
05895> PEAK FLOW (cms)= 1.50 .76 1.847 (iii)
05896> TIME TO PEAK (hrs)= 1.02 1.15 1.017
05897> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05898> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05899> RUNOFF COEFFICIENT = .98 .68 .811
05900>
05901> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
05902> CN* = 86.0 Ia = Dep. Storage (Above)
05903> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05904> THAN THE STORAGE COEFFICIENT.
05905> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05906> -----
05907> 250:0024-----
05908>
05909> | ADD HYD (Pond4In ) | ID: NHYD AREA QPEAK TPEAK R.V. DMF
05910> |-----|-----|-----|-----|-----|-----|
05911> | ID1 01:402 | (ha) (cms) (hrs) (mm) (cms)
05912> | +ID2 02:401 | 10.47 3.591 1.05 70.26 .000
05913> | +ID3 03:400 | 3.22 1.133 1.02 70.26 .000
05914> |-----|-----|-----|-----|-----|
05915> | SUM 04:Pond4In | 18.94 6.538 1.03 70.26 .000
05916>
05917> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
05918> -----
05919> 250:0025-----
05920>
05921> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
05922> | IN>04:(Pond4I) |
05923> | OUT<06:(Pond4 ) |
05924>
05925> ===== OUTFLOW STORAGE TABLE =====
05926> OUTFLOW STORAGE | OUTFLOW STORAGE
05927> (cms) (ha.m.) | (cms) (ha.m.)
05928> .000 .0000E+00 | 1.400 .7000E+00
05929> .310 .2300E+00 | .000 .0000E+00
05930>
05931> *** WARNING: STORAGE-Q values were extrapolated.
05932> Increase curve or use overflow option.
05933>
05934> ROUTING RESULTS AREA QPEAK TPEAK R.V.
05935> (ha) (cms) (hrs) (mm)
05936> INFLOW >04: (Pond4I) 18.94 6.538 1.033 70.256
05937> OUTFLOW<06: (Pond4 ) 18.94 1.592 1.567 70.256
05938>
05939> PEAK FLOW REDUCTION [Qout/Qin] (%) = 24.347
05940> TIME SHIFT OF PEAK FLOW (min)= 32.00
05941> MAXIMUM STORAGE USED (ha.m.)=.7705E+00
05942> -----
05943> 250:0026-----
05944>
05945> *#*****
05946> *# Pond 5 Sizing, Cas 500, 501 and 502
05947> *#*****
05948>
05949> | CALIB STANDHYD | Area (ha)= 2.93
05950> | 01:501 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05951> -----
05952>
05953> IMPERVIOUS PERVIOUS (i)
05954> Surface Area (ha)= 1.61 1.32
05955> Dep. Storage (mm)= 2.00 5.00
05956> Average Slope (%)= 1.00 1.00
05957> Length (m)= 250.00 40.00
05958> Mannings n = .013 .240
05959>
05960> Max.eff.Inten.(mm/hr)= 274.73 184.31
05961> over (min) 3.00 10.00
05962> Storage Coeff. (min)= 2.95 (ii) 9.59 (ii)
05963> Unit Hyd. Tpeak (min)= 3.00 10.00
05964> Unit Hyd. peak (cms)= .38 .12
05965>
05966> *TOTALS*
05967> PEAK FLOW (cms)= .84 .43 1.031 (iii)
05968> TIME TO PEAK (hrs)= 1.02 1.15 1.017
05969> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
05970> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
05971> RUNOFF COEFFICIENT = .98 .68 .811
05972>
05973> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

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05974> CN* = 86.0 Ia = Dep. Storage (Above)
05975> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
05976> THAN THE STORAGE COEFFICIENT.
05977> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
05978> -----
05979> 250:0027-----
05980>
05981> | CALIB STANDHYD | Area (ha)= 3.14
05982> | 02:500 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
05983> -----
05984>
05985> IMPERVIOUS PERVIOUS (i)
05986> Surface Area (ha)= 1.73 1.41
05987> Dep. Storage (mm)= 2.00 5.00
05988> Average Slope (%)= 1.00 1.00
05989> Length (m)= 250.00 40.00
05990> Mannings n = .013 .240
05991>
05992> Max.eff.Inten.(mm/hr)= 274.73 184.31
05993> over (min) 3.00 10.00
05994> Storage Coeff. (min)= 2.95 (ii) 9.59 (ii)
05995> Unit Hyd. Tpeak (min)= 3.00 10.00
05996> Unit Hyd. peak (cms)= .38 .12
05997>
05998> *TOTALS*
05999> PEAK FLOW (cms)= .90 .46 1.104 (iii)
06000> TIME TO PEAK (hrs)= 1.02 1.15 1.017
06001> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
06002> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
06003> RUNOFF COEFFICIENT = .98 .68 .811
06004>
06005> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
06006> CN* = 86.0 Ia = Dep. Storage (Above)
06007> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
06008> THAN THE STORAGE COEFFICIENT.
06009> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06010> -----
06011> 250:0028-----
06012>
06013> | CALIB STANDHYD | Area (ha)= 5.45
06014> | 03:502 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
06015> -----
06016>
06017> IMPERVIOUS PERVIOUS (i)
06018> Surface Area (ha)= 2.00 2.45
06019> Dep. Storage (mm)= 2.00 5.00
06020> Average Slope (%)= 1.00 1.00
06021> Length (m)= 600.00 40.00
06022> Mannings n = .013 .240
06023>
06024> Max.eff.Inten.(mm/hr)= 274.73 166.83
06025> over (min) 5.00 12.00
06026> Storage Coeff. (min)= 5.00 (ii) 11.91 (ii)
06027> Unit Hyd. Tpeak (min)= 5.00 12.00
06028> Unit Hyd. peak (cms)= .23 .09
06029>
06030> *TOTALS*
06031> PEAK FLOW (cms)= 1.28 .70 1.685 (iii)
06032> TIME TO PEAK (hrs)= 1.05 1.20 1.067
06033> RUNOFF VOLUME (mm)= 84.60 58.52 70.256
06034> TOTAL RAINFALL (mm)= 86.60 86.60 86.603
06035> RUNOFF COEFFICIENT = .98 .68 .811
06036>
06037> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
06038> CN* = 86.0 Ia = Dep. Storage (Above)
06039> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
06040> THAN THE STORAGE COEFFICIENT.
06041> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06042> -----
06043> 250:0029-----
06044>
06045> | ADD HYD (Pond5In ) | ID: NHYD AREA QPEAK TPEAK R.V. DMF
06046> |-----|-----|-----|-----|-----|
06047> | ID1 01:501 | (ha) (cms) (hrs) (mm) (cms)
06048> | +ID2 02:500 | 2.93 1.031 1.02 70.26 .000
06049> | +ID3 03:502 | 3.14 1.104 1.02 70.26 .000
06050> |-----|-----|-----|-----|-----|
06051> | SUM 04:Pond5In | 11.52 3.710 1.03 70.26 .000
06052>
06053> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
06054> -----
06055> 250:0030-----
06056>
06057> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
06058> | IN>04:(Pond5I) |
06059> | OUT<05:(Pond5 ) |
06060>
06061> ===== OUTFLOW STORAGE TABLE =====
06062> OUTFLOW STORAGE | OUTFLOW STORAGE
06063> (cms) (ha.m.) | (cms) (ha.m.)
06064> .000 .0000E+00 | .850 .5000E+00
06065> .190 .2300E+00 | .000 .0000E+00
06066>
06067> ROUTING RESULTS AREA QPEAK TPEAK R.V.
06068> (ha) (cms) (hrs) (mm)
06069> INFLOW >04: (Pond5I) 11.52 3.710 1.033 70.256
06070> OUTFLOW<05: (Pond5 ) 11.52 .837 1.633 70.256
06071>
06072> PEAK FLOW REDUCTION [Qout/Qin] (%) = 22.571
06073> TIME SHIFT OF PEAK FLOW (min)= 36.00
06074> MAXIMUM STORAGE USED (ha.m.)=.4949E+00
06075> -----
06076> 250:0031-----
06077>
06078> *#*****
06079> *# EXT3 Sizing, Cas EXT3
06080> *#*****
06081>
06082> | CALIB STANDHYD | Area (ha)= 9.16
06083> | 01:EXT3 DT= 1.00 | Total Imp(%)= 55.00 Dir. Conn.(%)= 45.00
06084> -----
06085>
06086> IMPERVIOUS PERVIOUS (i)
06087> Surface Area (ha)= 5.04 4.12
06088> Dep. Storage (mm)= 2.00 5.00
06089> Average Slope (%)= 1.00 1.00
06090> Length (m)= 400.00 40.00
06091> Mannings n = .013 .240
06092>
06093> Max.eff.Inten.(mm/hr)= 274.73 174.76
06094> over (min) 4.00 11.00
06095> Storage Coeff. (min)= 3.92 (ii) 10.70 (ii)
06096> Unit Hyd. Tpeak (min)= 4.00 11.00
06097> Unit Hyd. peak (cms)= .29 .10
06098>
06099> *TOTALS*
06100> PEAK FLOW (cms)= 2.37 1.25 3.017 (iii)
06101> TIME TO PEAK (hrs)= 1.03 1.17 1.050
06102> RUNOFF VOLUME (mm)= 84.60 58.52 70.256

```

```

06099> TOTAL RAINFALL (mm) = 86.60 86.60 86.603
06098> RUNOFF COEFFICIENT = .98 .68 .811
06099>
06100> (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
06101> CN* = 86.0 Ia = Dep. Storage (Above)
06102> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
06103> THAN THE STORAGE COEFFICIENT.
06104> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06105>
-----
06107> 250:0032-----
06108>
06109> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .150 (cms)
06110> | TotalHyd 01:EXT3 | Number of inlets in system [NINLET] = 1
06111> | | Total minor system capacity = .150 (cms)
06112> | | Total major system storage [TMJSTO] = 5000. (cu.m.)
06113>
06114> ID: NHYD AREA QPEAK TPEAK R.V. DWF
06115> (ha) (cms) (hrs) (mm) (cms)
06116> TOTAL HYD. 01:EXT3 9.16 3.017 1.050 70.256 .000
06117>
06118> MAJOR SYST 02:noFlow .00 .000 .000 .000 .000
06119> MINOR SYST 03:MinorE 9.16 .150 .633 70.328 .000
06120>
06121> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
06122>
06123> Maximum MAJOR SYSTEM storage used = 4998. (cu.m.)
06124>
-----
06125> 250:0033-----
06126>
06127> *#*****
06128> *#
06129> *# Flow Totals and Channel Runoff
06130> *#
06131> *#*****
06132>
06133> | ADD HYD (Control ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
06134> (ha) (cms) (hrs) (mm) (cms)
06135> ID1 02:noFlow .00 .000 .00 .00 .000
06136> +ID2 03:MinorEXT3 9.16 .150 .63 70.33 .000
06137> +ID3 05:Pond5 11.52 .837 1.63 70.26 .000
06138> +ID4 06:Pond4 18.94 1.592 1.57 70.26 .000
06139> +ID5 07:Pond3 18.88 1.504 1.63 63.52 .000
06140> +ID6 08:Pond2 7.53 .599 1.63 70.26 .000
06141> +ID7 09:Pond1 4.08 .265 1.67 70.26 .000
06142> +ID8 10:ExPond 32.50 2.661 1.63 70.26 .000
06143>
06144> SUM 01:Control 102.61 7.599 1.62 69.02 .000
06145>
06146> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
06147>
06148>
-----
06149> 250:0034-----
06150>
06151> | CALIB NASHYD | Area (ha)= .99 Curve Number (CN)=68.00
06152> | 02:600 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
06153> | U.H. Tp (hrs)= .350
06154>
06155> Unit Hyd Qpeak (cms)= .108
06156>
06157> PEAK FLOW (cms)= .085 (i)
06158> TIME TO PEAK (hrs)= 1.467
06159> RUNOFF VOLUME (mm)= 33.107
06160> TOTAL RAINFALL (mm)= 86.603
06161> RUNOFF COEFFICIENT = .382
06162>
06163> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06164>
-----
06165> 250:0035-----
06166>
06167>
06168> | CALIB NASHYD | Area (ha)= 3.54 Curve Number (CN)=68.00
06169> | 03:601 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
06170> | U.H. Tp (hrs)= .590
06171>
06172> Unit Hyd Qpeak (cms)= .229
06173>
06174> PEAK FLOW (cms)= .212 (i)
06175> TIME TO PEAK (hrs)= 1.767
06176> RUNOFF VOLUME (mm)= 33.108
06177> TOTAL RAINFALL (mm)= 86.603
06178> RUNOFF COEFFICIENT = .382
06179>
06180> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06181>
-----
06182> 250:0036-----
06183>
06184>
06185> | CALIB NASHYD | Area (ha)= 3.61 Curve Number (CN)=68.00
06186> | 04:602 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res. (N)= 3.00
06187> | U.H. Tp (hrs)= .970
06188>
06189> Unit Hyd Qpeak (cms)= .142
06190>
06191> PEAK FLOW (cms)= .149 (i)
06192> TIME TO PEAK (hrs)= 2.233
06193> RUNOFF VOLUME (mm)= 33.108
06194> TOTAL RAINFALL (mm)= 86.603
06195> RUNOFF COEFFICIENT = .382
06196>
06197> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
06198>
-----
06199> 250:0037-----
06200>
06201>
06202> | ADD HYD (PostTot ) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
06203> (ha) (cms) (hrs) (mm) (cms)
06204> ID1 01:Control 102.61 7.599 1.62 69.02 .000
06205> +ID2 02:600 .99 .085 1.47 33.11 .000
06206> +ID3 03:601 3.54 .212 1.77 33.11 .000
06207> +ID4 04:602 3.61 .149 2.23 33.11 .000
06208>
06209> SUM 05:PostTot 110.75 7.983 1.63 66.38 .000
06210>
06211> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
06212>
06213>
06214> 250:0038-----
06215>
06216> 250:0002-----
06217>
06218> 250:0002-----
06219>
06220> 250:0002-----
06221>
06222> 250:0002-----
06223>

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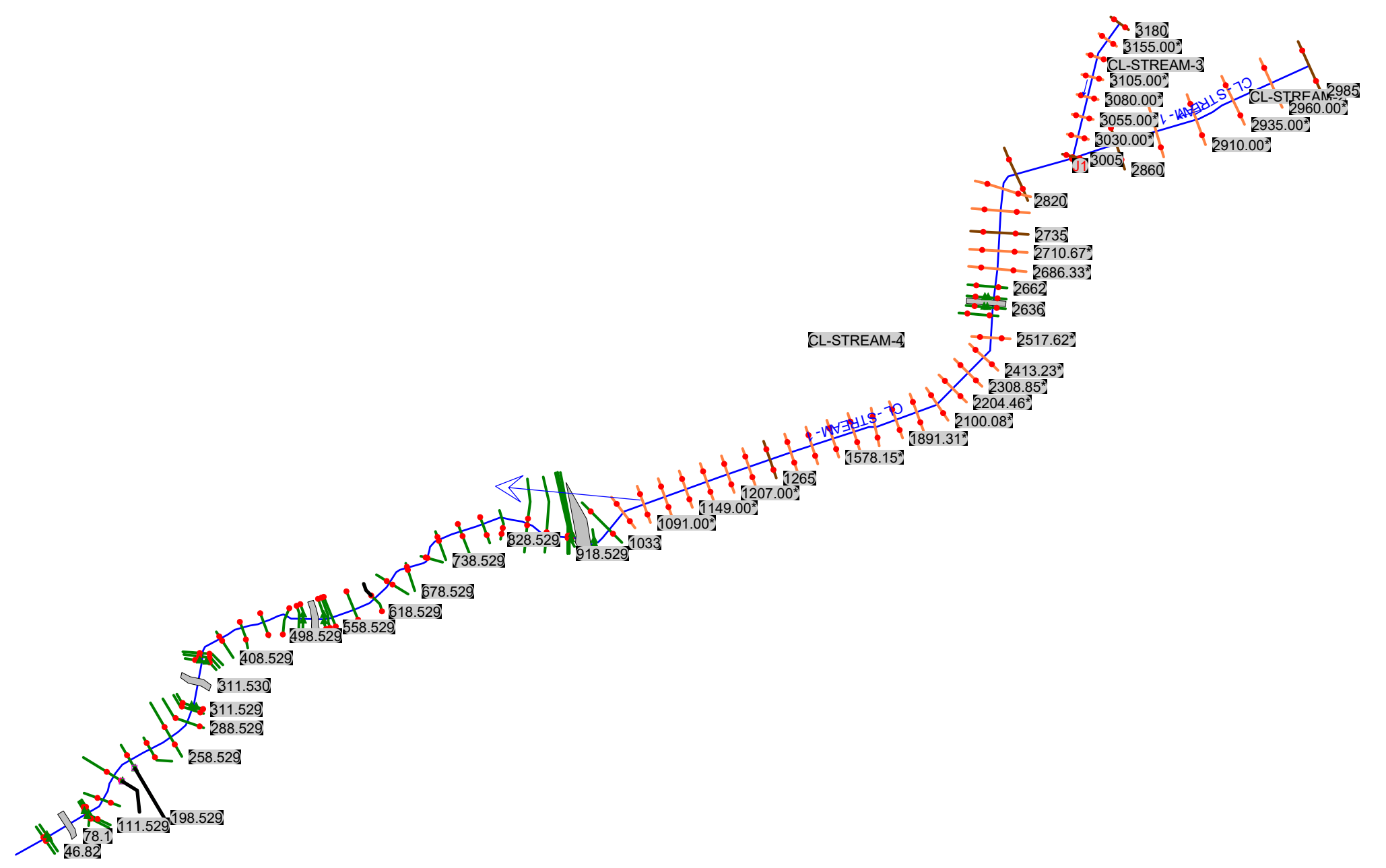
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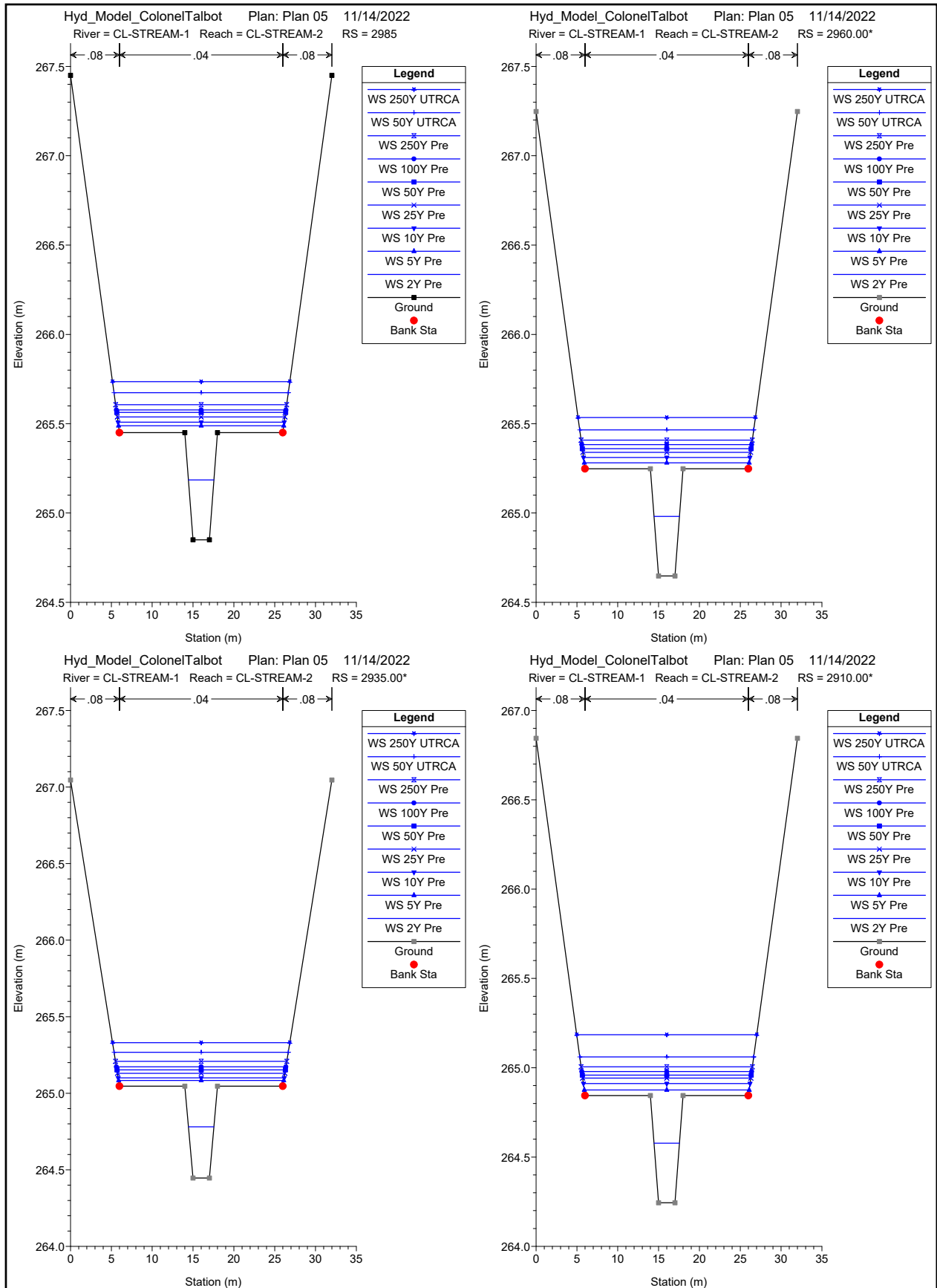
06224> 250:0002-----
06225>
06226> 250:0002-----
06227> FINISH
06228>
06229> *****
06230> WARNINGS / ERRORS / NOTES
06231>
06232> 250:0011 ROUTE RESERVOIR
06233> *** WARNING: STORAGE-Q values were extrapolated.
06234> Increase curve or use overflow option.
06235> 250:0015 ROUTE RESERVOIR
06236> *** WARNING: STORAGE-Q values were extrapolated.
06237> Increase curve or use overflow option.
06238> 250:0020 ROUTE RESERVOIR
06239> *** WARNING: STORAGE-Q values were extrapolated.
06240> Increase curve or use overflow option.
06241> 250:0025 ROUTE RESERVOIR
06242> *** WARNING: STORAGE-Q values were extrapolated.
06243> Increase curve or use overflow option.
06244> Simulation ended on 2022-11-14 at 16:30:53
06245>
06246>

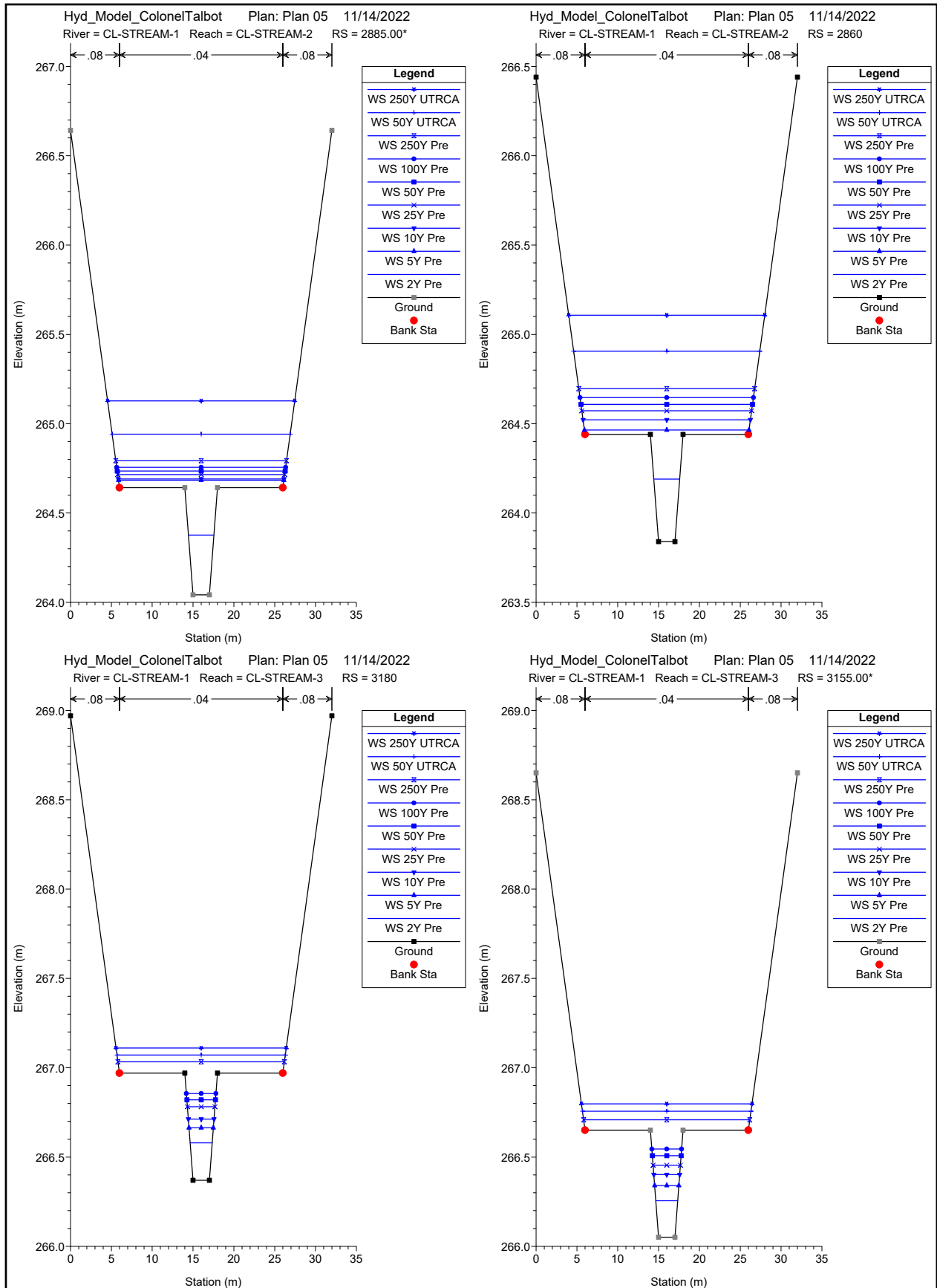
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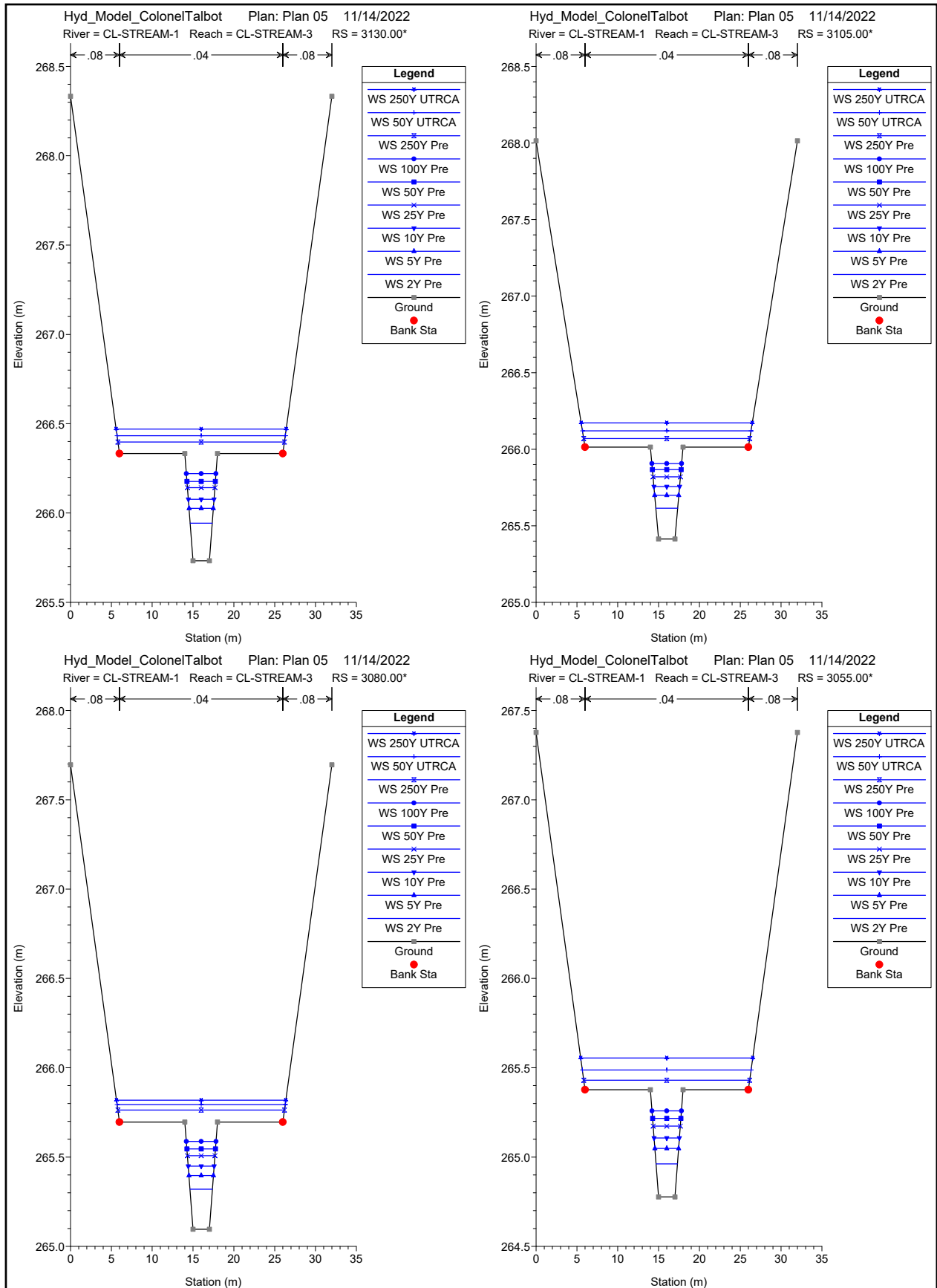
APPENDIX B: Hydraulic Analysis Results

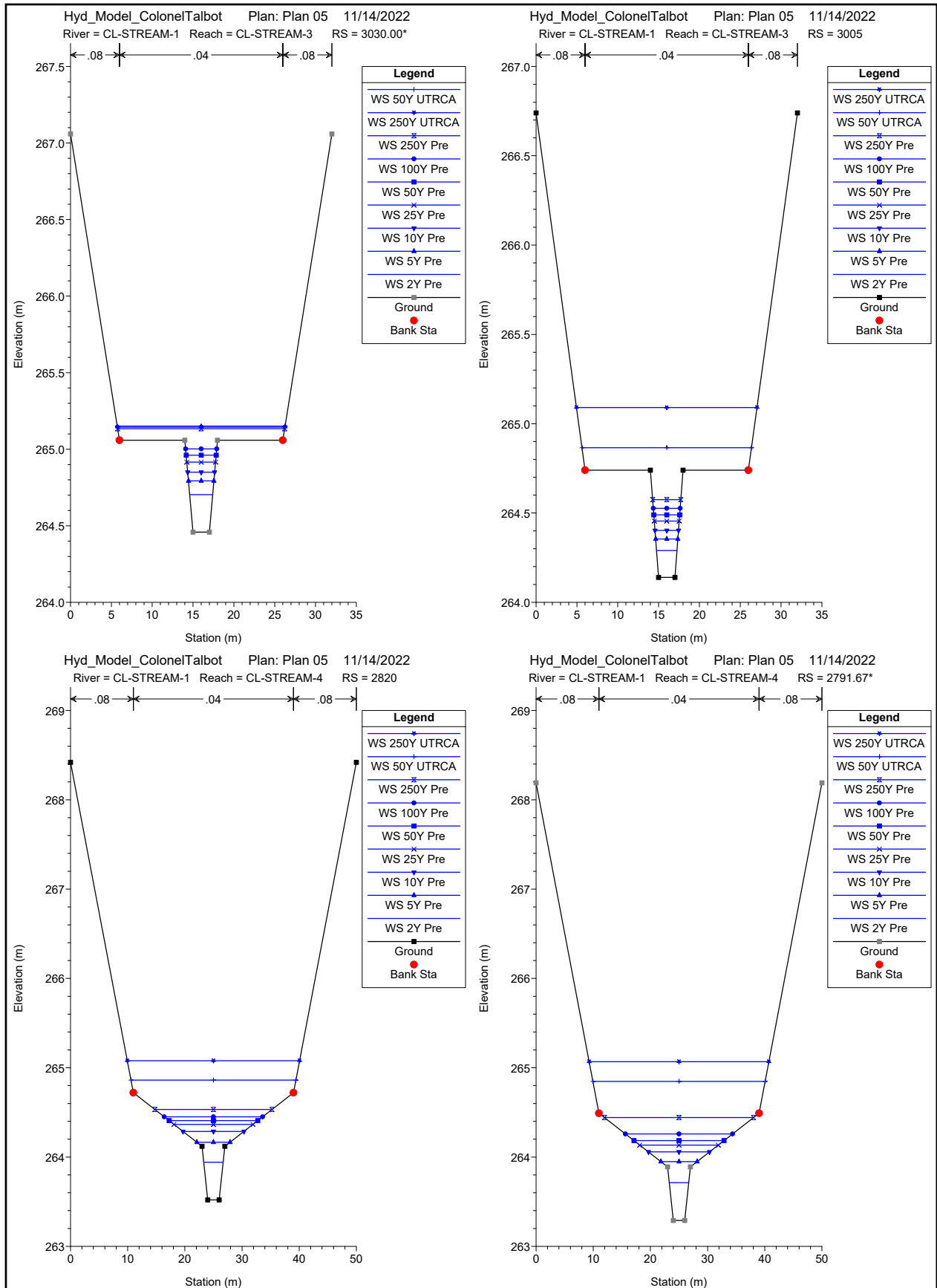


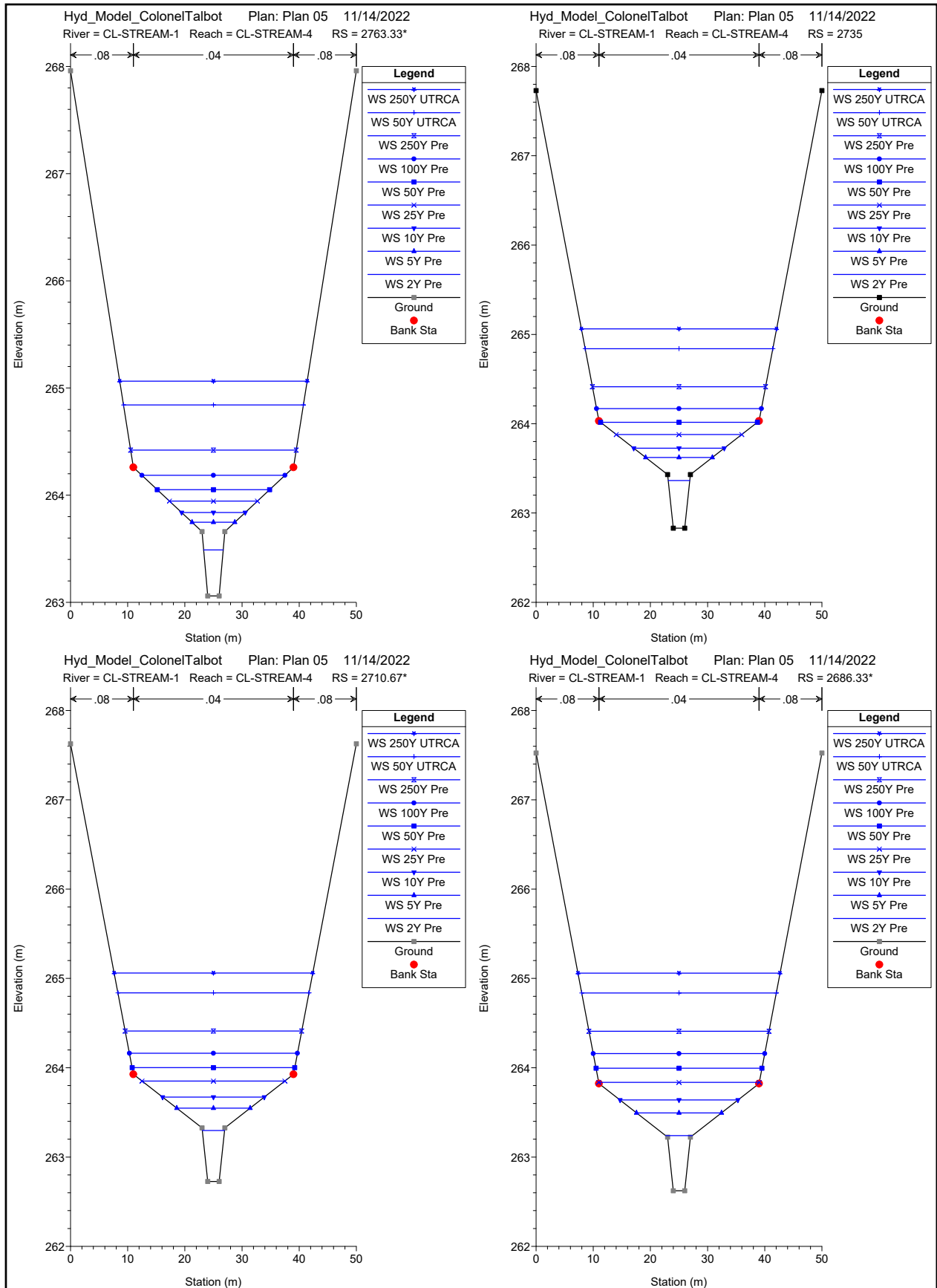


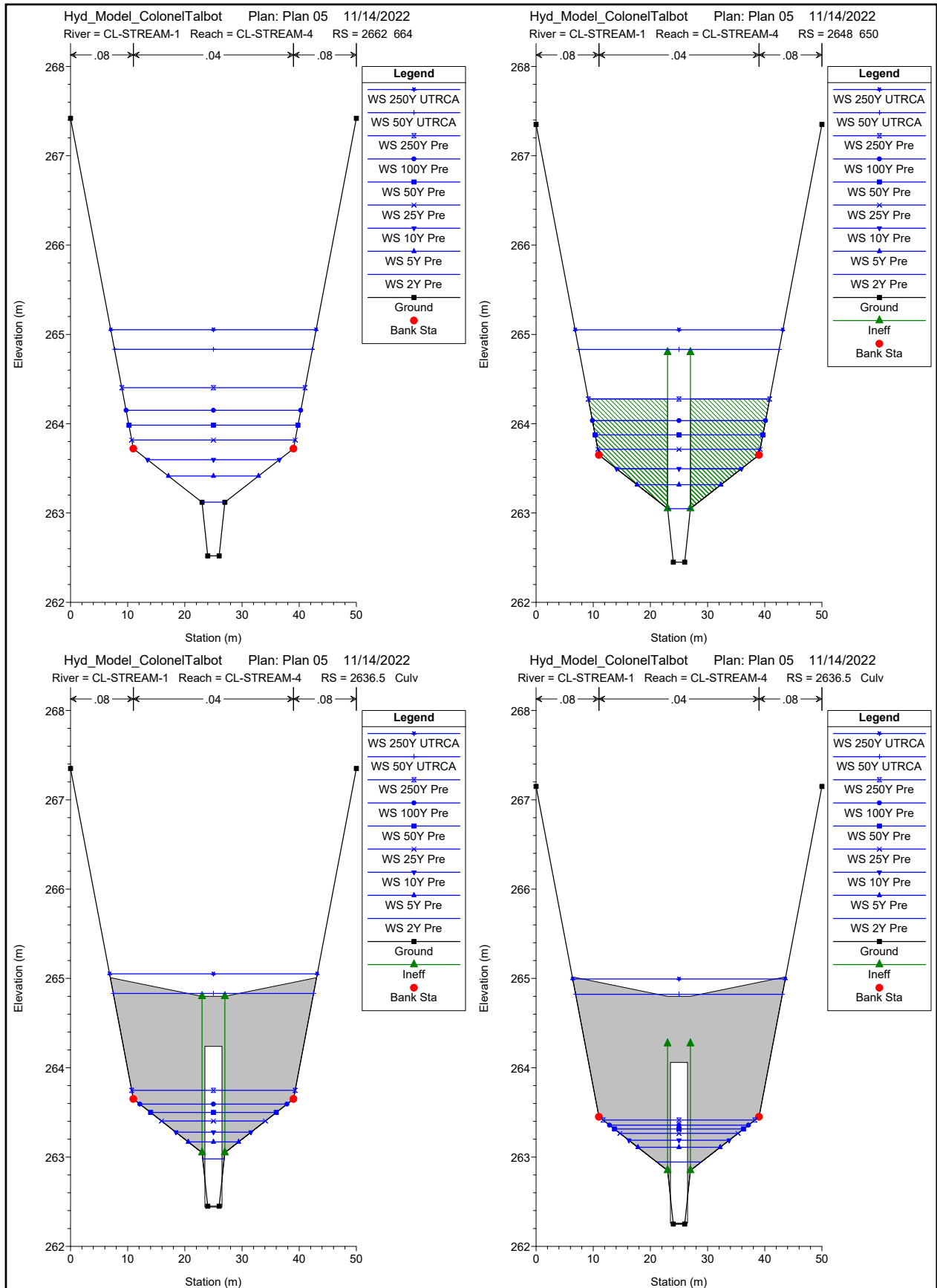


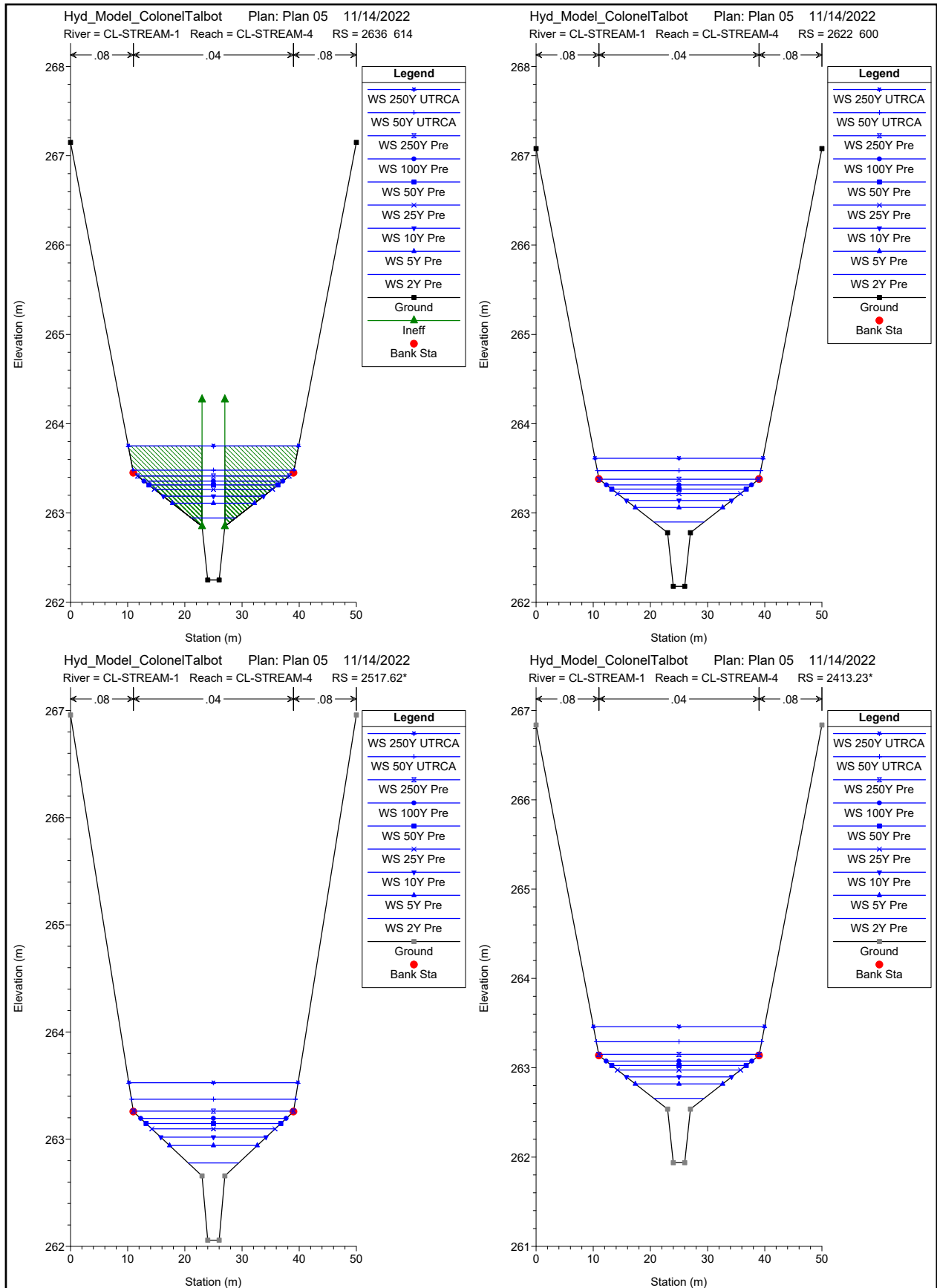


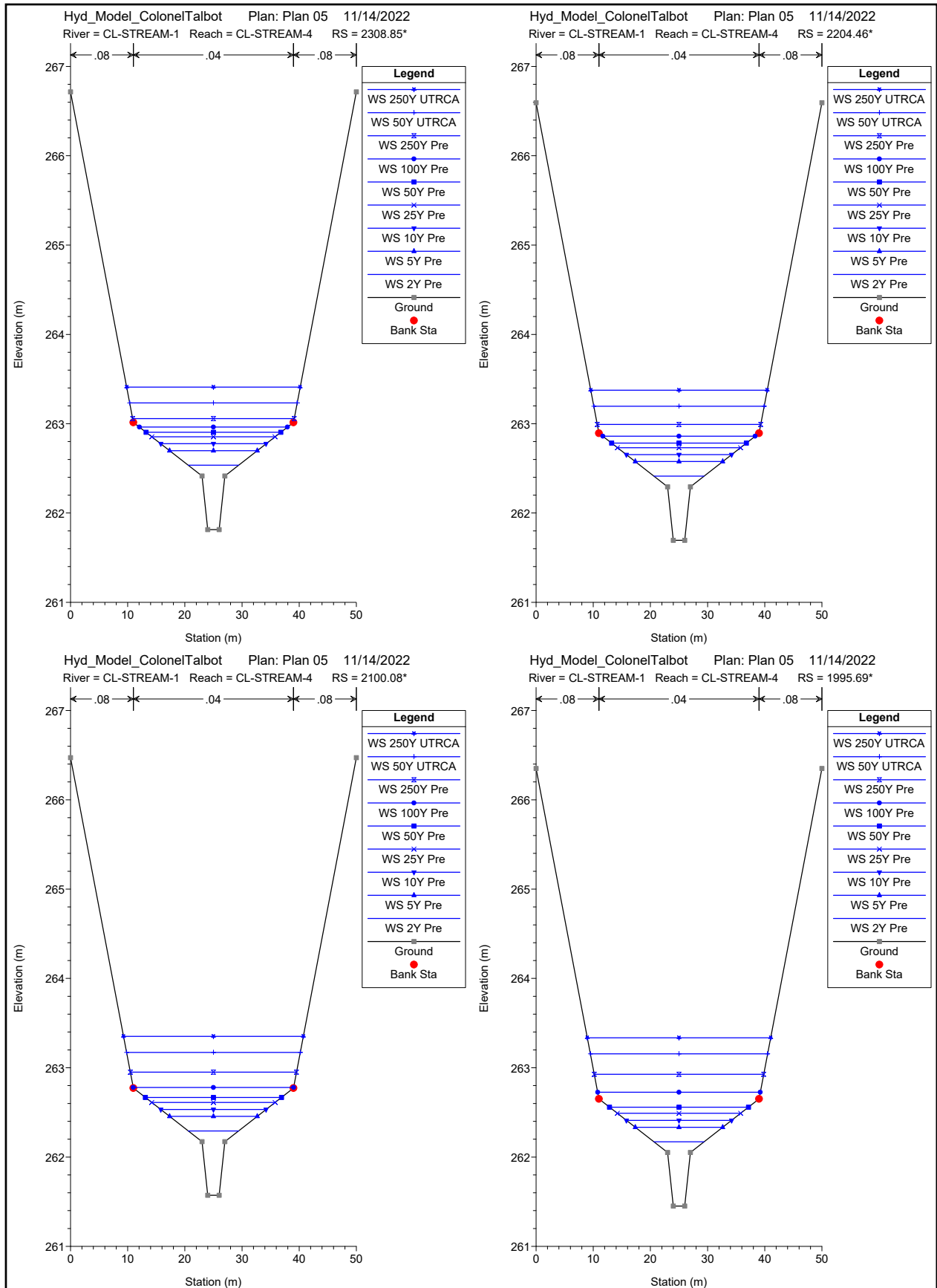


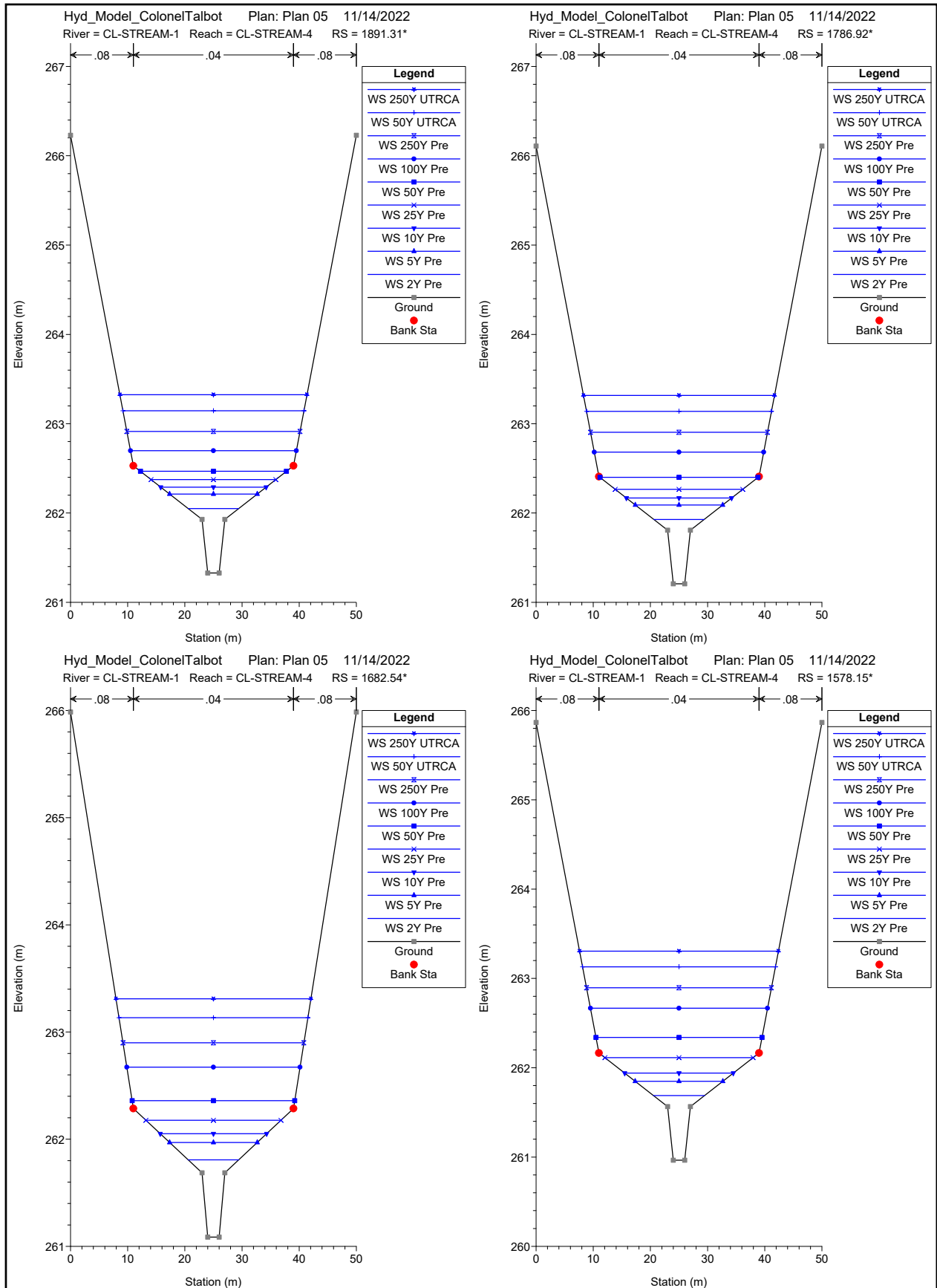


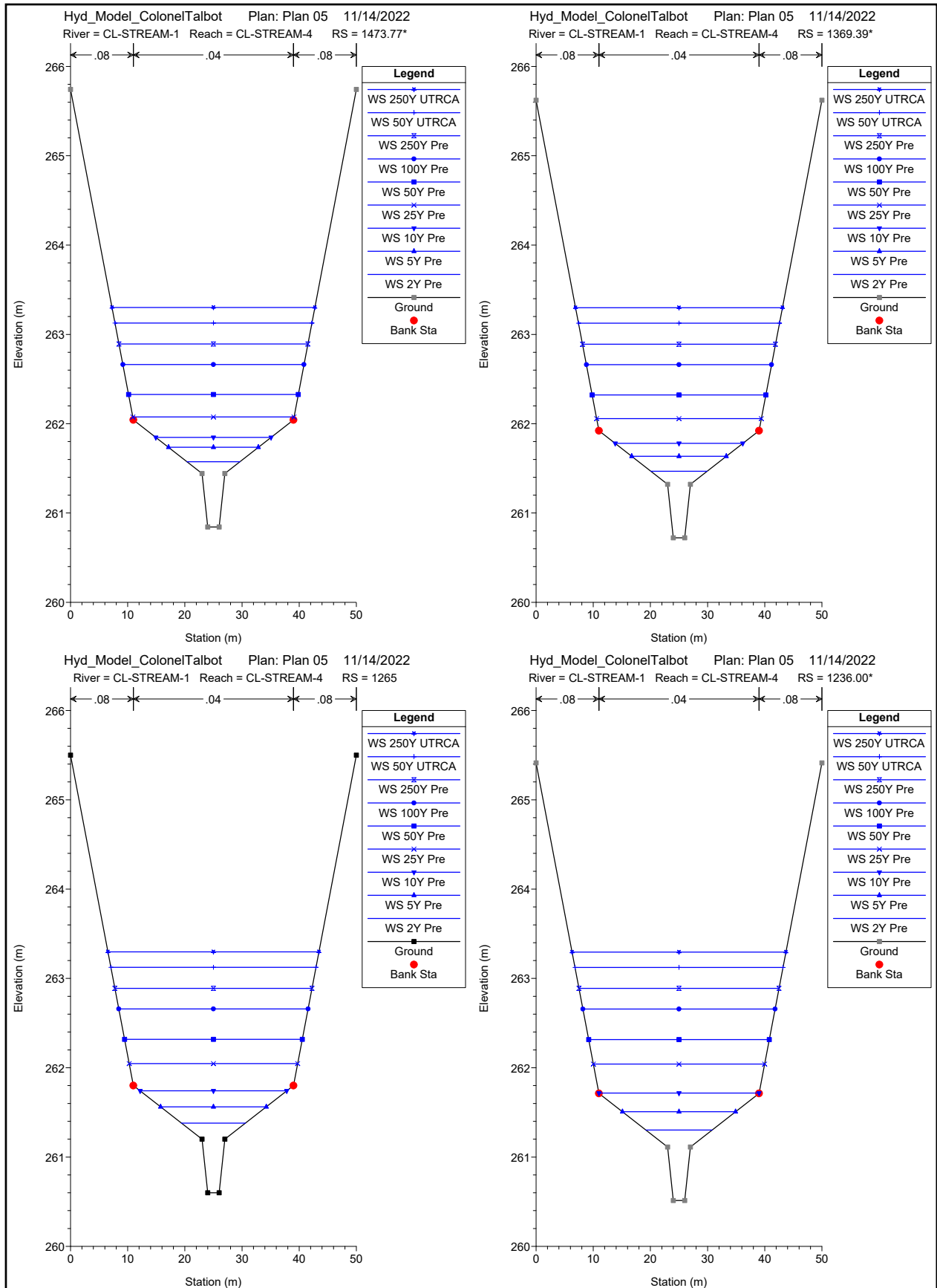


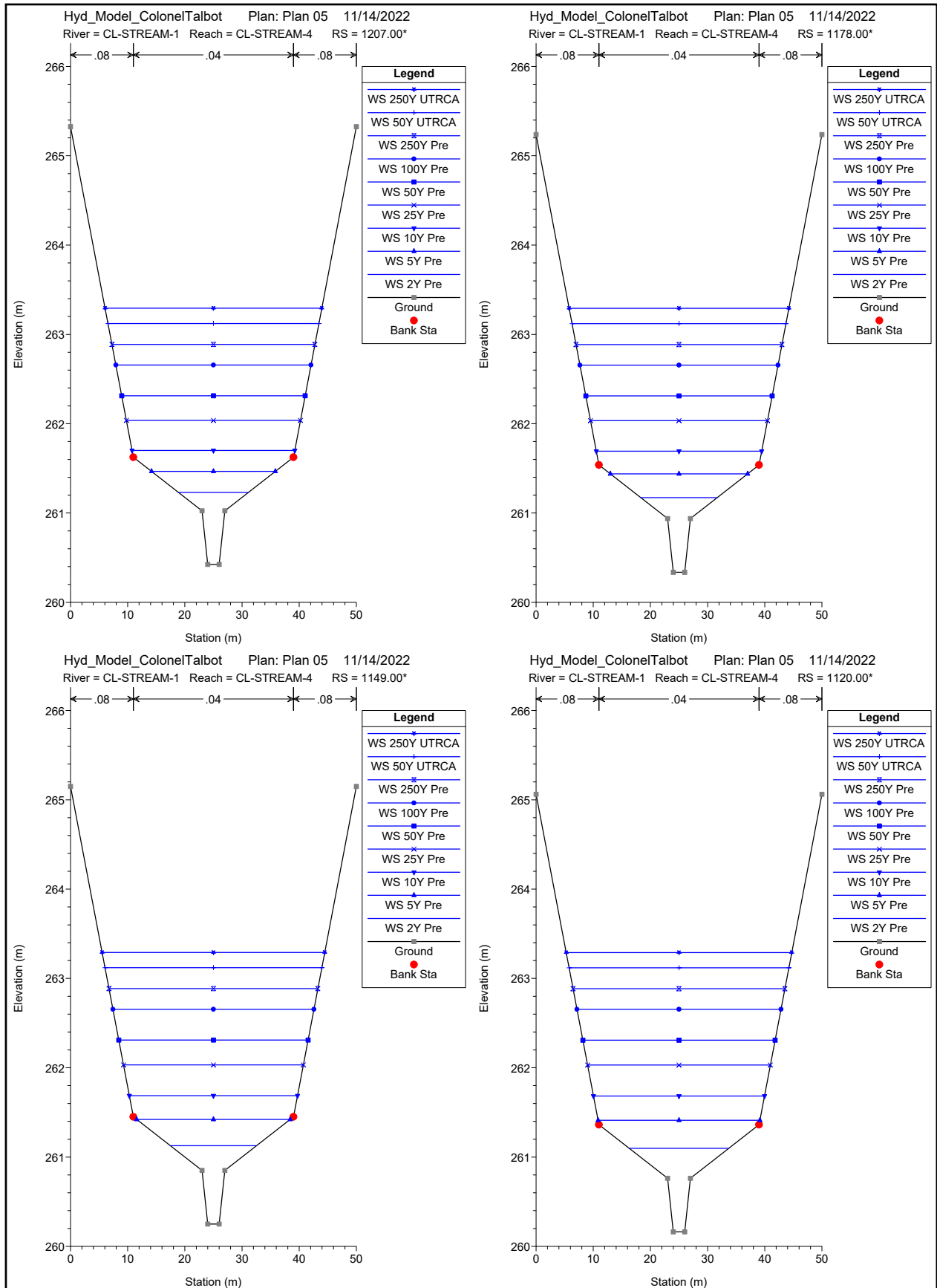


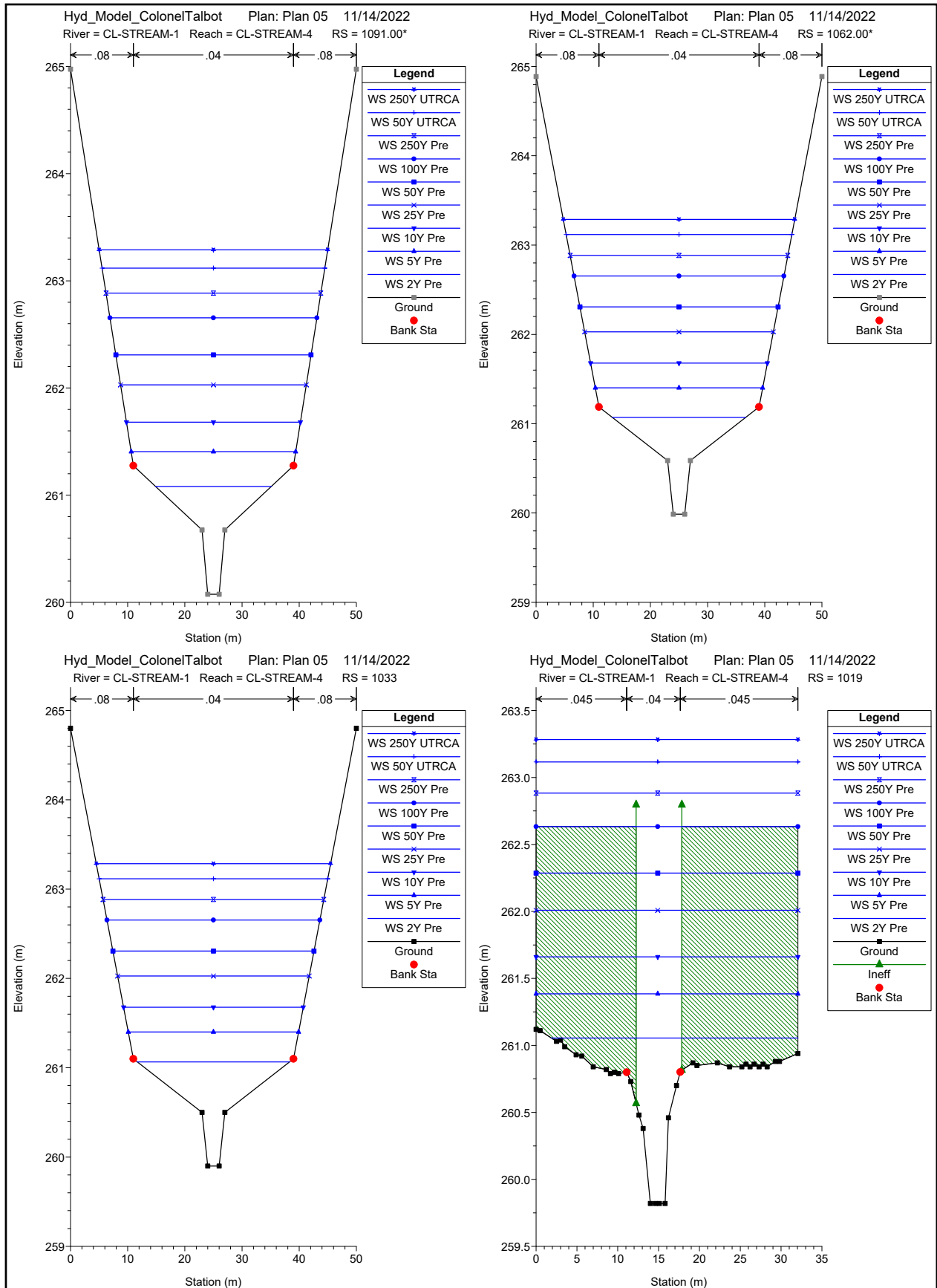


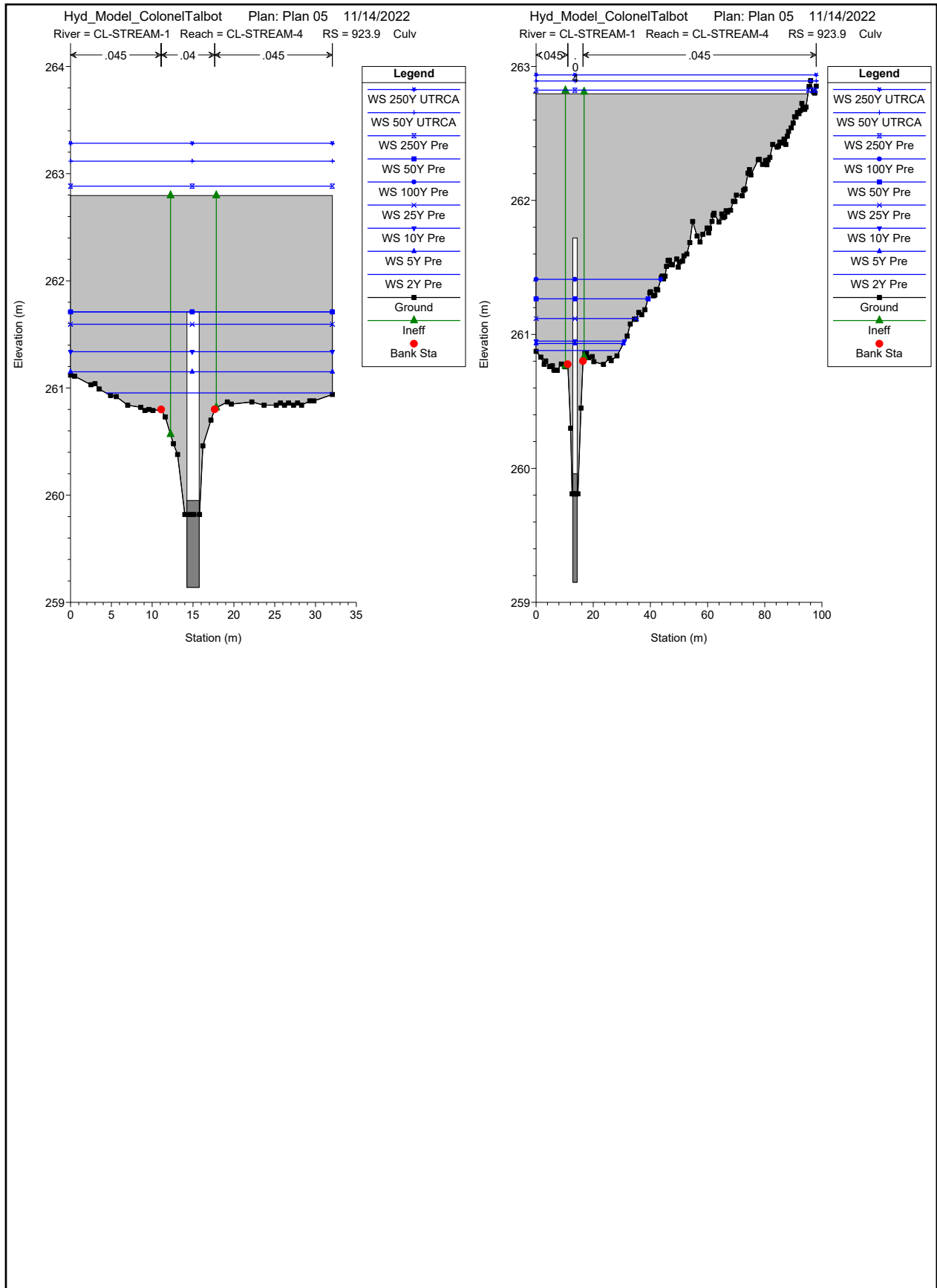












**APPENDIX C:
Fluvial Geomorphology and
Meander Belt Assessment**





**Fluvial Geomorphology and
Meander Belt Assessment,
Dingman Creek Tributary B1,
London, Ontario**

November 21, 2019

Prepared for:

York Development Group and
Sifton Properties Ltd.

Prepared by:

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Waterloo, ON N2L 0A4
Tel.: (519) 579-4410

161413835



**FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY
B1, LONDON, ONTARIO**

This document entitled Fluvial Geomorphology and Meander Belt Assessment, Dingman Creek Tributary B1, London, Ontario was prepared by Stantec Consulting Ltd. ("Stantec") for the account of York Development Group and Sifton Properties Ltd. (the "Client") to support the Client's application for Draft Plan Approval (the "Application") for the Future Development Lands in the Colonel Talbot Area (the "Project"). In connection thereto, this document may be reviewed and used by the provincial and municipal government agencies participating in the permitting process in the normal course of their duties. Except as set forth in the previous sentence, any reliance on this document by any third party for any other purpose is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

Prepared by _____

(signature)

Amber Garrett, B.Eng.
Water Resources Engineering Intern

Reviewed by _____

(signature)

Scott Cowan, P.Geo., C.Tech.
Fluvial Geomorphologist



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FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY B1, LONDON, ONTARIO

Introduction

1.0 INTRODUCTION

Stantec Consulting Ltd. was retained by York Developments and Sifton to provide a major drainage and flow routing assessment in support of their proposed subdivisions located on Colonel Talbot Road in the City of London, Ontario. As part of this work plan, a meander belt assessment was recommended for Dingman Creek Tributary B1 (the Tributary). The results of the meander belt assessment support the development by delineating the Tributary's meander belt and confirming the proposed channel corridor. The location of the Study Area and the Tributary are presented in Figure 1.

1.1 SCOPE OF WORK

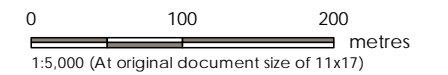
The scope of this assessment involved various desktop and field components. The goal of these components was to determine a meander belt for the Tributary within the Study Area. The tasks completed for this study included:

1. review background information including topographic mapping, geologic mapping, and aerial photographs;
2. reach delineation and field observations; and
3. meander belt width delineation

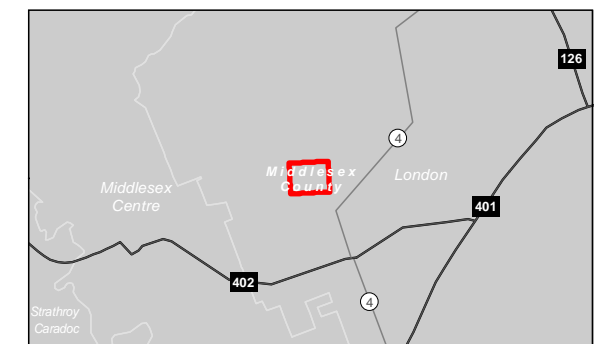


Legend

- Study Area
- Reach Break
- Dingman Creek Tributary (Centerline - 2015)
- Dingman Creek Tributary (Estimated Centerline - 2015)
- Meander Belt
- 1 m Contour
- Expressway / Highway
- Major Road
- Minor Road



- Notes
1. Coordinate System: NAD 1983 UTM Zone 17N
 2. Base features produced under license with the Ontario Ministry of Natural Resources and Forestry © Queen's Printer for Ontario, 2019.
 3. Orthoimagery © First Base Solutions. Imagery Date, 2019.



Project Location: City of London
 Prepared by AMW on 2019-11-21
 Technical Review by SC on 2019-11-21
 161413835 REVA

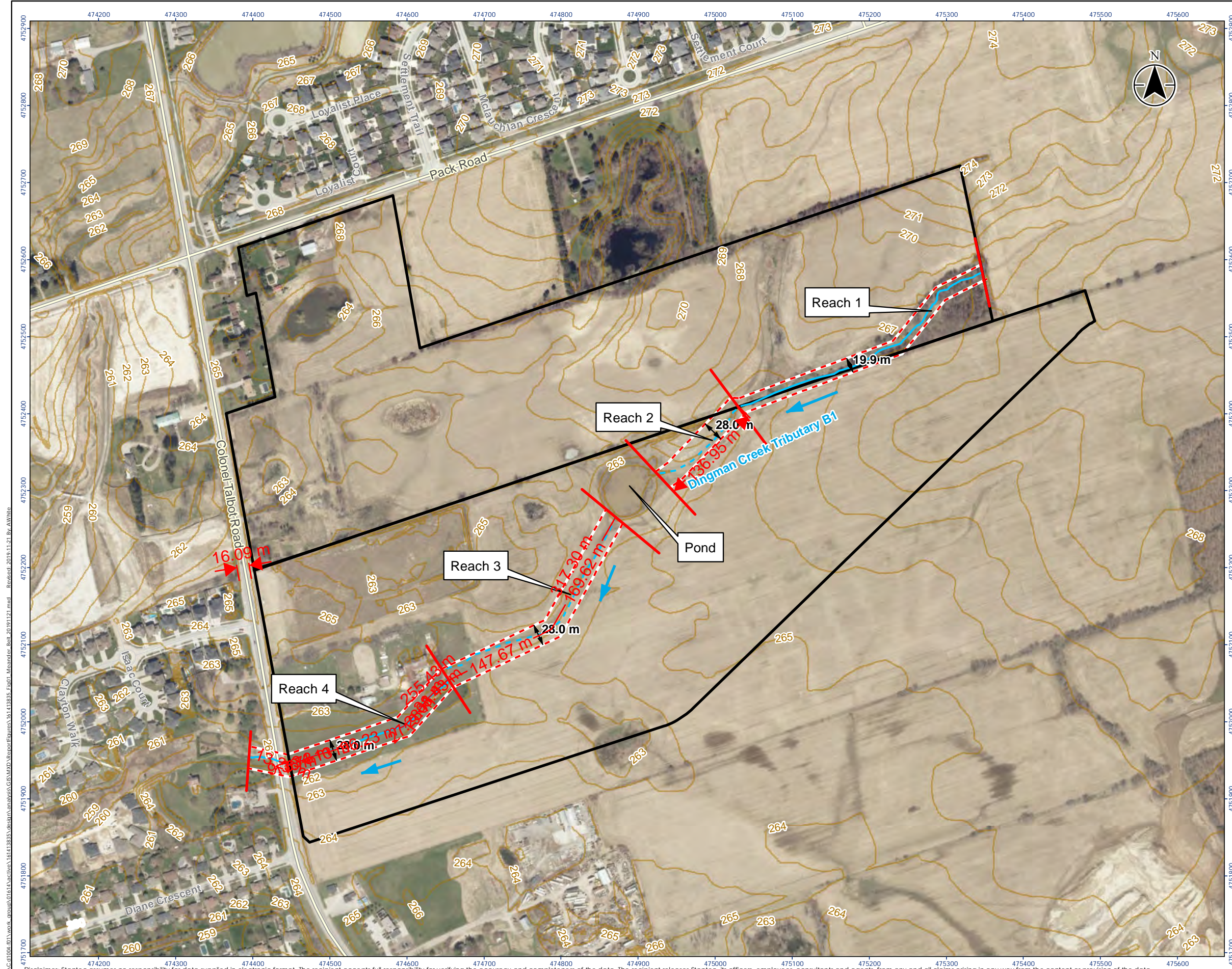
Client/Project: 731675 ONTARIO LIMITED
 COLONEL TALBOT AREA MAJOR DRAINAGE

Figure No.

1

Title

Colonel Talbot Meander Belt



\\C:\d\001\work_group\0161413835\subpara_analysis\GIS\KOD\Report\Figures\161413835_Fig01_Meander Belt_20191121.mxd Revised: 2019-11-21 By: AWhite

FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY B1, LONDON, ONTARIO

Background Review

2.0 BACKGROUND REVIEW

2.1 GEOLOGY

Surficial and bedrock geology maps published by the Ontario Geological Service (OGS) indicated the predominant physiographic region within the Study Area is the Mount Elgin Ridges (Chapman and Putnam, 1984). The Mount Elgin Ridges physiographic region contains a series of moraines that are oriented generally parallel to Lake Erie and consist of mainly clay-silt till.

2.2 THE DINGMAN CREEK WATERSHED

The Dingman Creek watershed is located at the southern boundary of the City of London and drains 176 km² of the Upper Thames River watershed. Dingman Creek flows east to west from its headwaters in Thames Center to the Thames River just west of London. Within the Study Area, the Tributary, is a constructed drain and is classified as an intermittent system by Land Information Ontario (LIO) mapping (Ministry of Natural Resources and Forestry (MNRF), 2011). This tributary drains an area approximately 2 km² from its northern boundary at Southdale Road West to its outlet into Dingman Creek.

2.3 HISTORICAL ANALYSIS

A sequence of historic aerial photographs (1955, 1995, 2007, and 2015) and detailed topographic mapping (1 m contours) were reviewed to gain insight into channel form, surrounding land use/cover, and to identify any changes that have occurred during the period of record. The predominant land use within the watershed is agricultural with a growing proportion of residential in more recent years. Within the area of the proposed development, the Tributary has been straightened within an agricultural field and has remained in that orientation throughout the period of record (since 1955). This type of channel modification is common within the rural areas surrounding the City of London. The riparian corridor consists of short herbaceous vegetation consistent with a pasture. Riparian vegetation within the Study Area has not changed through the period of record.



3.0 REACH DELINEATION AND FIELD OBSERVATIONS

3.1 REACH DELINEATION

Reaches are lengths of channel that have physical constraints (e.g. geology, slope, discharge, vegetation, sediment input) that remain nearly constant along their length and subsequently exhibit similar physical geomorphic characteristics (e.g. channel form, sinuosity, physical dimensions). As a result, the controlling and modifying influences of channel form in a reach are similar (TRCA, 2004). This partitioning of a channel into reaches guides the desktop and field analyses, in that it considers the influence of localized channel patterns and processes. Based on the information available, the Tributary within the Study Area was partitioned into four reaches (Figure 1).

3.2 REACH DESCRIPTION

Existing site conditions were observed during a site visit completed by Stantec on November 1, 2019. Reach 1 exhibited a mostly straightened planform with a low degree of confinement and a narrow, low width/depth ratio channel. Banks appeared almost vertical with some scour but were mostly stable throughout the reach. Vegetation within this reach consisted of herbaceous vegetation on stream banks with shrubs and mature trees in the riparian corridor and floodplain. Reaches 2 and 3 were enclosed in a tile flowing subsurface. Reach 4 consisted of a straight planform within an unconfined valley setting. Channel banks were shallow sloping and vegetated with short grasses typical of a lawn or field. Vegetation in the riparian corridor and floodplain was similar to the channel banks. The physical attributes of the channels within each reach are summarized in Table 1 below. A photographic inventory of Reach 1 and Reach 4 is presented in Appendix A.



FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY B1, LONDON, ONTARIO

Reach Delineation and Field Observations

Table 1 - Summary of Existing Conditions Along Dingman Creek Tributary B1

Reach	Reach 1	Reach 2	Reach 3	Reach 4
Length (m)	383	142	332	298
Channel Slope (m/m)	0.0088	Not Applicable - Enclosed	Not Applicable - Enclosed	0.0042
Valley Form	Unconfined			Unconfined
Bankfull Width (m)	1.2			3.8
Substrate	Soft clay loam			Soft clay loam
Bank Material	Soft sandy clay loam. Lower banks were bare and undercut, upper banks vegetated with grasses.			Soft sandy clay loam. Banks well vegetated with grasses.
Sinuosity	1.05 (historically straightened)			1.02 (historically straightened)
Riparian Vegetation	Well vegetated with grasses and shrubs. Mature trees outside of bankfull channel			Banks, bed, and riparian corridor, and floodplain exclusively vegetated with short grasses.



FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY B1, LONDON, ONTARIO

Meander Belt Width Determination

4.0 MEANDER BELT WIDTH DETERMINATION

The meander belt is a term used to quantify the lateral extent of a river's occupation of its floodplain (TRCA, 2004). Meander belts are inherently variable and their extent is dependent on a number of controlling factors. These include, among other things, hydrology, stormwater flows, bank erosion rates, channel slope, and the degree of channel confinement by the valley walls.

The Tributary within the Study Area was straightened prior to the available historic air photo record. As a result, channel mapping procedures could not be implemented to delineate the meander belt width. In such situations, a surrogate approach can be used wherein the meander pattern of a similar system is measured and the results are applied to the straightened channel. However, no such suitable surrogate reach could be located as most of the watercourses of this size and slope within this region have also been straightened or altered.

Since there is no available evidence of what this historical meander belt would have been, and with no suitable surrogate reach available, the specific methodology applied to the study area was the Empirical Approach (TRCA Procedure 5). The empirical approach used in this analysis implements a suite of empirical relationships. These models are based on a variety of physical variables and represent a reasonable range of values. As such, calculated averages for each reach are considered appropriate to estimate existing condition meander belt widths. The empirical relations considered suitable for the Study Area include the following:

4.1 TRCA (2004)

The empirical relation developed for this method requires calculating stream power during a 2-year flow event, defined as the product of the specific weight of water, discharge, and channel slope, using the following equation:

$$SP = \gamma Qs, \text{ where}$$

SP = Stream power (watts/m²)

γ = Specific weight of water (9806 kg/m² s²)

Q = 2-year flow, (m³/s)

s = Channel slope (m/m)

The empirical relationship used to account for a potential change in hydrology was calculated as follows:

$$W_b = -14.827 + 8.319 \ln (SP * DA) \text{ where}$$

W_b = Meander belt width (m)

DA = Drainage area (km²)



FLUVIAL GEOMORPHOLOGY AND MEANDER BELT ASSESSMENT, DINGMAN CREEK TRIBUTARY B1, LONDON, ONTARIO

Meander Belt Width Determination

4.2 WILLIAMS (1986)

This empirical relationship is based on the bankfull width of the channel and calculated as follows:

$$W_b = 4.3w^{1.12}, \text{ where}$$

W_b = Meander belt width (m)

w = Bankfull width, (m)

4.3 ANNABLE (1996)

This empirical relationship was developed based on streams in southern Ontario. The All Types analysis used in this report is calculated as follows:

$$W_b = 35.20Q_{bkf}^{0.53}, \text{ where}$$

W_b = Meander belt width (m)

Q_{bkf} = Bankfull Discharge, (m³/s)

Results from the empirical analysis are reported in Table 2. Based on a variety of physical variables, these results represent a reasonable range of values. As such, calculated averages for each subject reach are considered appropriate for existing meander belt widths. Given that Reach 2 and 3 were historically tile drained, Reach 4 was used as a surrogate reach in order to recommend a meander belt dimension for these reaches. Meander belt limits are illustrated in Figure 1.

Table 2 - Summary of Existing and Final Meander Belt Widths

Reach	Reach 1	Reach 2	Reach 3	Reach 4
Discharge, Q_2 (m ³ /s)	1.1	-	-	2.0
Reach Drainage Area, DA (km ²)	0.82	-	-	1.25
Existing Meander Belt Width – TRCA, 2004 (m)	21.4	-	-	23.7
Existing Meander Belt Width – Williams, 1986 (m)	5.3	-	-	19.2
Existing Meander Belt Width – Annable, 1996 (m)	23.0	-	-	27.2
Existing Meander Belt Width (Average) (m)	16.6	-	-	23.4
Final Meander Belt Width (including factor of safety) (m)	19.9	28.0*	28.0*	28.0

* Reach 4 Meander Belt Width Applied

4.4 FACTOR OF SAFETY

The TRCA (2004) mapping protocol requires that meander belt delineation is augmented by incorporating an additional and appropriate margin of safety to allow for future lateral migration. An evaluation of the historic air photo record indicates that the realigned channel has remained relatively stable over the



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Meander Belt Width Determination

period of record. However, because of poor aerial photograph resolution, a quantification of the rate of channel shifting is not possible. As a result, the margin of safety for this study is dependent on a safety factor of 1.2 applied to the existing belt width. This margin of safety is considered conservative, and suitable to account for typical rates of channel adjustment (erosion and migration) and the potential for underprediction within the empirical methods. The final meander belt widths were estimated to be 19.9 m for Reach 1 and 28.0 m for Reaches 2, 3, and 4. Although these belt widths represent the maximum lateral expression of the watercourse within its geomorphically active corridor, it is understood that during detailed design, measures will be implemented that reduce channel erosion within the active corridor.



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Summary

5.0 SUMMARY

The purpose of this assessment was to delineate a meander belt width for the Tributary within the Study Area. The results of this assessment support the development by estimating a meander belt that provides adequate width to address potential migration associated with the watercourse in its current location. The meander belt widths for the Study Area are 19.9 m for Reach 1 and 28.0 m for Reach 2, 3, and 4. Although these belt widths represent the maximum lateral expression of the watercourse within its geomorphically active corridor, it is understood that during detailed design, measures will be implemented that reduce channel erosion within the active corridor. As a result, the proposed channel corridor of 30.0 m is considered to be conservative and adequate to support the natural function of the Tributary.



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6.0 REFERENCES

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APPENDIX A

Photographic Inventory



Photo 1: Looking upstream at Reach 1 from left bank (November 1, 2019).



Photo 2: Looking downstream in Reach 1 (November 1, 2019).



Photo 3: Looking downstream at Reach 4 from Colonel Talbot Road (November 1, 2019).



Photo 4: Looking upstream at Reach 4 from Colonel Talbot Road (November 1, 2019).

Appendix A: Photographic Inventory of Tributary to Dingman Creek B1 Existing Conditions

PREPARED FOR:
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