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RESIDENTIAL SUBDIVISION 1944 BRADLEY AVENUE CITY OF LONDON

FUNCTIONAL SERVICING REPORT

Prepared For:

ELITE DEVELOPMENTS

May 18, 2023

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APPENDIX A

Proposed Residential Subdivision by Weston Consulting

APPENDIX B

External Sanitary Area Plan prepared by Development Engineering Sanitary Calculation Spreadsheet for Parker Jackson Subdivision by Development Engineering Watermain modelling excerpts for Parker Jackson Subdivision by Development Engineering Conceptual Servicing Plan Conceptual Grading Plan

Figure 1 – Pre Development Storm Tributary Areas

Figure 2 – Post Development Storm Tributary Area Plan

Strom Sewer Design Sheet

1.0 BACKGROUND

The property under study is a 42.3 ha (104.5 acre) site located in the City of London, north-east of the intersection of Bradley Road and Jackson Road. The site is bound by a Parker Jackson residential subdivision to the north and west which is currently under construction, agricultural lands to the east, and Bradley Rd to the south.

Presently the site is farm land consisting of a dwelling with a barn on the southern portion and a wooded area on the northern portion. An existing hydro transmission corridor traverses the middle of the site running in south-west to north-east direction. See below Exhibit 1 for an aerial view of the existing site.



Exhibit 1 - Site Aerial Image

The proposed development by Elite Developments will consist of a mix of single detached homes, freehold townhouses and condo townhouses. Access to the site will be from a future road connection to the west from the neighbouring Parker Jackson Subdivision in Phase 4, currently denoted as Street N or Evans Blvd. The area of proposed development within the property is situated between the northerly woodlot and the existing hydro transmission corridor which has an area of 9.5 ha (23.5 acres). For further information regarding the proposed site layout please refer to drawings prepared by Weston Consulting in Appendix A. See Appendix A for aerial view and the proposed site plan.

This report will evaluate the serviceability of the site with respect to sanitary, water and stormwater services and also conceptual grading of the proposed development.

For detailed topography of the existing site conditions, as of September 2022, refer to the topographic survey prepared by A.T. McLaren Ltd.

2.0 DESIGN CONSIDERATIONS

A) SANITARY WASTE WATER DISPOSAL

Existing Site

Presently there are no existing sanitary sewers adjacent to the site. A 250mm diameter sanitary sewer located within the future Street N/Evans Blvd to the west is proposed to be stubbed to the property and has allocated capacity to service the proposed development, including lands east of the subject site. Development Engineering has prepared an external sanitary tributary area plan which shows there is a population of 2,160 that has been assigned in the downstream sewer design. Please refer to Appendix B for the external sanitary tributary area plan prepared by Development Engineering.

The sewer design spreadsheet prepared by Development Engineers shows that the downstream 250mm sanitary sewer sloped at 0.33% has a capacity of 34.18 l/s and the anticipated flow from the allocated population is 20.47 l/s. The upstream area that has been allocated is 14.84ha therefore an additional 1.48 l/s of infiltration has been allocated to the connecting sewer. Since the proposed development is only 9.5 ha, the remaining 5.34 ha has been assigned to lands east of the site. Please refer to Appendix B for the downstream sewer design calculations prepared by Development Engineering.

Based on the above allocation and construction of the downstream sanitary sewer on the neighbouring lands, the proposed development will have an outlet for sanitary services.

Proposed Developed Site

The proposed site will consist of residential units only. The unit type breakdown is shown in the following Table 1.

| Table 1 – Summary of Residential Units for Sanitary Flow Calculations | | | | | | | |
|---|--------------|--|--|--|--|--|--|
| Proposed Residential Typology | No. of Units | | | | | | |
| Single Detached | 49 | | | | | | |
| Freehold Townhomes | 144 | | | | | | |
| Condo Townhomes | 88 | | | | | | |
| Total | 281 | | | | | | |

Refer to the site statistics and the site plan by Weston Consulting in Appendix A for further details.

For calculating the population for the site the following City standards for population densities and flow rates will be used. It should be noted these densities were also used by Development Engineers in calculating the downstream receiving sewers to the west.

- 3 persons/unit for Single Detached and Freehold Townhomes
- 2.4 persons/unit for Condo Townhomes
- The per capita flow rate of 230 L/person/day for residential

Based on the above information, the peak sanitary flow from the proposed development was calculated as shown below totaling 9.08 L/s.

| Total Tributary Area Per Capita Flow (Q) Infiltration Rate (i) | 230 | ha L/cap/day L/s/ha | | SITE DES | SCRIPTION: | Residential Subdivision 1944 Bradley Rd City of London | | | |
|--|--------------------|--|----------------------------|---------------------|---------------------------------|--|----------------------|---------------------------------------|--|
| LAND USE | NUMBER OF UNITS | SITE AREA, (ha) | GROSS FLOOR AREA, m2 | TOTAL POPULATION | TOTAL DAILY FLOW (LITERS) | AVERAGE DAILY FLOW I/sec | PEAKING FACTOR, M | TOTAL FLOW FROM LAND USE, I/sec | |
| RESIDENTIAL, Freehold Townhomes/Single Detached, using 3 persons/unit | 193 | | | 579 | 133,170 | 1.54 | | | |
| RESIDENTIAL, Condo Townhomes, using 2.4 People/Unit | 88 | | | 211 | 48,576 | 0.56 | | | |
| TOTAL RESIDENTIAL | 281 | | | 790 | 181,746 | 2.10 | 3.86 | 8.13 | |
| TOTAL | | | | V1= | 181,746 | Q1 = Q (infil) = Q (total) = | | L/s L/s L/s | |
| Notes: | | | | | | | | | |
| Q = (MqP/86400) + A * I (L/sec) | | | | | | | | | |
| where : | | | | | | | | | |
| Peaking Factor (M) = 1 + [14 / (4 q = L/cap/day P = Population A = Gross site area | | V1= Total Volume from Land Use in liters Q1= Total domestic flow from Land Use (L/sec) Q (infil) = Total flow from infiltration (L/sec) Q (total) = Total flow (Land use + Infiltration) | | | | | | | |

As shown above, the total generated expected sanitary flow and population from the site is less than the allocated values assigned to the allocated sanitary sewer downstream within the future Phase 4 of Parker Jackson Subdivision. No changes to existing downstream design is required.

All sanitary sewers within the development will be sized at 250mm diameter which is the minimum City of London standard. Please refer to Appendix B for the conceptual sanitary servicing layout within the subdivision showing pipe slopes and invert depths.

i = Infiltration rate

B) WATER DISTRIBUTION

The water servicing for the site will be provided by connecting to the future 300mm watermain which will be stubbed to the site at the connecting Street N/Evans Blvd.

Looping the municipal watermain through the site back to future Street L/Lyndsay Street through the proposed connector green spaces along the north and west boundary is proposed to maintain pressure and flows to the site and will also provide a secondary water source in case of temporary shut downs of watermains within the site. The connection to Street L/Lindsay Street will need to be made through the proposed Park Block within Phase 4 of Parker Jackson Subdivision denoted as Block 60. Please refer to the proposed servicing concept in Appendix B for the conceptual watermain layout for the proposed site.

A WaterCAD model was completed by Development Engineers for the proposed neighbouring Parker Jackson Subdivision (Parker Jackson Subdivision Water Servicing Design Report dated August 1, 2021) which included conceptual modelling for the subject site with consideration for looping to the 600mm watermain on Commissioners Rd to the north or the 600mm watermain on Bradeley Ave to the south, however due the distance to complete these connections the loop to Street L has been proposed as mentioned above. Further analysis of the looping requirements will be completed to confirm available flows within the proposed development.

Domestic Water Demands

The domestic water demand for the site will be calculated using City of London design standards as follows.

| a) | Average Day domestic demand - Peak day demand - | using 255 L/cap/day (790 persons) | 2.33 L/sec |
|----|--|--------------------------------------|-------------|
| b) | Peak day demand - | 3.5 x daily demand | 8.16 L/sec |
| c) | Peak hour demand - | 7.8 x daily demand | 18.17 L/sec |

Fire Protection

The required fire flow for the proposed development is typically determined by the Ontario Building Code at the building permit stage. As per City guidelines the Fire Underwriters Survey (FUS) can be used to determine preliminary fire demands however without specific dwelling unit sizes and setback requirements know at this time, demands from the City of London's Design Specification and Requirements manual are to be considered.

In modeling the site Development Engineering used a fire demand of 76 L/s for single detached dwellings and 105 L/s for townhouse units.

Fire hydrants will be distributed throughout the proposed subdivision meeting the City's hydrant spacing requirements.

Design Considerations

The unit rate and peaking factors of water consumption, minimum pipe size and allowable pressure in line will be established from the City's Water Design Standards.

The pressures and volumes must be sufficient for peak hour conditions and under fire conditions as established by the Ontario Building Code. The minimal residual pressure under fire conditions is 140 kpa (or 20.3 psi).

According to the MOE criteria the allowable pressures are as follows:

| Condition | Allowable Pres | Allowable Pressures (kpa) | | | | | |
|-------------------------|----------------|---------------------------|--|--|--|--|--|
| | min. | max. | | | | | |
| 1) Min. Hour | 275 | 700 | | | | | |
| 2) Peak Hour | 275 | 700 | | | | | |
| 3) Peak Day + Fire Flow | 140 | 700 | | | | | |

To determine the pressures that will be available to the site, the full buildout conditions were considered for the watermain connection and hydrant at the Street N/ Evans Ave connection point in Development Engineers Report. The available flow under peak day plus fire flow was determined to be 77 L/s with a pressure of 313.56 kpa (45.5 PSI) at the connection point which meets the fire flow requirement for single detached dwellings but not for townhome units. Looping options to increase flow will be further evaluated on subsequent submission upon further coordination with the neighbouring development. Please refer to excerpts of Development Engineers modelling results in Appendix B for details of the ultimate buildout conditions on the neighbouring subdivision.

C) STORMWATER SERVICING

The existing site is located within the Dingman Creek catchment area and drains toward the Thames River through the Hampton-Scott Municipal Drain. The area of development within the subject lands has been allocated to the Parker Stormwater Management Facility located to the westward, on the east side of Jackson Street between Darnley Blvd and Evans Blvd within the Parker Jackson Subdivision. The pond was constructed by the City of London in 2019 to provide quantity and quality control for 78.1 ha of land which includes the proposed subdivision denoted as area 202e in Exhibit 2 below.



Exhibit 2 - Site Aerial Image

Existing Conditions

A pre-development drainage area plan located in Appendix B has been prepared to show the detailed existing storm catchments within the proposed subdivision to confirm existing outlets surrounding the site and their contributing areas. Areas 1, 2 and 3 currently drain westward toward the neighbouring Parker Jackson Subdivision with Area 2 draining directly into the existing neighbouring woodlot. Area 4 currently drains southward toward Bradley Rd however this area has been allocated to the existing SWM pond and will be diverted in the post-development condition. No external areas are presently draining towards the proposed subdivision therefore no existing interim catchments will need to be considered in the proposed storm sewer design.

Proposed Conditions

The proposed subdivision will be serviced for storm drainage by a proposed 1350mm storm sewer stub located on future Street N/Evans Blvd. The connecting sewer has been sized to accommodate the subject development and future residential lands denoted as 202f (11.637 ha) on Exhibit 2 above.

A preliminary storm sewer design is shown on the conceptual servicing plan in Appendix B which shows the storm sewers sizing and slope requirements to service the site and the future westerly developable lands. A 1050mm storm sewer will be terminated at the west limit of the site to service future development. Storm design calculations and an associated storm tributary plan is provided in Appendix B detailing all proposed pipe lengths within the development located on municipal road allowances.

The open space areas of the development between the woodlot and the proposed residential lots will remain as per existing conditions and will drain according to the existing topography. Areas draining toward the residential units will drain to proposed rear yard catchbasins whereas areas draining toward the northerly and westerly woodlot will continue to drain to their respective outlets.

The internal private condo townhouse block will be serviced with one storm outlet west of the block. Internal sewers within the block have not been detailed at this stage as the sewers will be privately owned and the block will be subject to a Site Plan Application which will detail the sewer design within the block. This block will not require any quantity or quality stormwater control as this is being managed within the downstream Parker SWM facility.

Grading Consideration

Grading for the proposed site will be such that major overland flow will be directed westward through the proposed internal road network toward the connecting Street N/Evans Blvd. Overland flow beyond the property is proposed to be directed overland to the Parker SWM facility via the proposed road network.

A conceptual grading design can be found in Appendix B showing how the site will tie into existing surrounding sites and direct overland runoff to westerly lands.

Erosion Control

Erosion and sediment controls for the site will be implemented according to The Ministry of Natural Resources Guidelines on Erosion and Sediment Control for Urban Construction Sites. A detailed erosion control plan will be prepared upon final design.

3.0 **CONCLUSIONS**

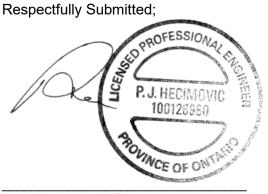
From our investigation the site is serviceable utilizing the future allocated sanitary, storm and watermain infrastructure that will be constructed in Phase 4 of the westerly Parker Jackson Subdivision.

A 250mm sanitary stub at the connecting Street N/Evans Blvd has an allocated population of 2,160 people of which 790 are within the proposed development, thereby providing sufficient capacity for the site.

A 300mm watermain stub has been proposed at the connecting Street N/Evans Blvd which provides sufficient flow to meet the water demand for single family dwellings however will require looping to a second watermain source to accommodate water demand for the proposed townhouse units within the development. Watermain looping options will be explored through further watermain analysis.

A 1350mm storm sewer stub at the connecting Street N/Evans Blvd will provide sufficient stormwater drainage capacity to drain stormwater from the subject development and future developable lands to the east. The existing downstream Parker SWM facility located west of the site within Parker Jackson Subdivison has allocated quantity and quality control to service the site for stormwater management purposes.

Respectfully Submitted;

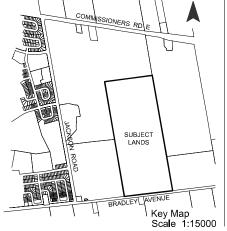


Paul Hecimovic, P.Eng



Proposed Residential Subdivision by Weston Consulting





| DEVELOPMENT STATISTICS | : | | |
|-------------------------------|--------------------|-----------|-----------|
| Land Use | Lots/Blocks | Units | Area |
| Single Detached Residential | Lots 1-49 | 49 units | 2.246 ha |
| Street Townhouses | Blks 50-72 | 144 units | 2.748 ha |
| Condo Townhouse Block | Blk 73 | | 1.862 ha |
| Greenspace Connector | Blk 74 | | 0.232 ha |
| Future Development | B l k 75,76 | | 17.635 ha |
| Hydro Easement | B l k 77,78 | | 2.518 ha |
| 30 m Buffer | B i k 79 | | 1.909 ha |
| Environmental Protection Area | B i k 80 | | 9.449 ha |
| 0.3m Reserves | Blk 81,82 | | 0.001 ha |
| Roads | | | 3.517 ha |
| TOTAL | | 193 units | 42.117 ha |

ADDITIONAL INFORMATION:

[Section 51(17) of the Planning Act, R.S.O. 1990, c. P.13], as amended to February 09, 2023.
a), b), e), f), g), & j) - on plan.
c) - on key plan
d) - see statistics

a) - see statistics
 h) - piped municipal water supply
 i) - silty clay and gravel
 k) - piped communal sewage disposal
 l) - easements as in instruments

ELITE BRADLEY DEVELOPMENTS INC.
SAM SAKHI
102-3410 SOUTH SERVICE ROAD
BURLINGTON, ONTARIO L7N 3T2
PHONE (289) 816-1024 EMAIL: s.sakhi@eli

SURVEYOR'S CERTIFICATE:

I hereby certify that the boundaries of the lands being subdivided and their correct relationship to the adjacent lands are accurately and correctly shown on this plan.

A.T. McLAREN LIMITED
LEGAL AND ENGINEERING SURVEYS
69 JOHN STREET SOUTH, SUITE 230
HAMILTON, ONTARIO, LBN 289
PHONE (905) 527–8559 FAX (905) 527–0032

SCALE

25 50 75 100m **WESTON**

File Numbe

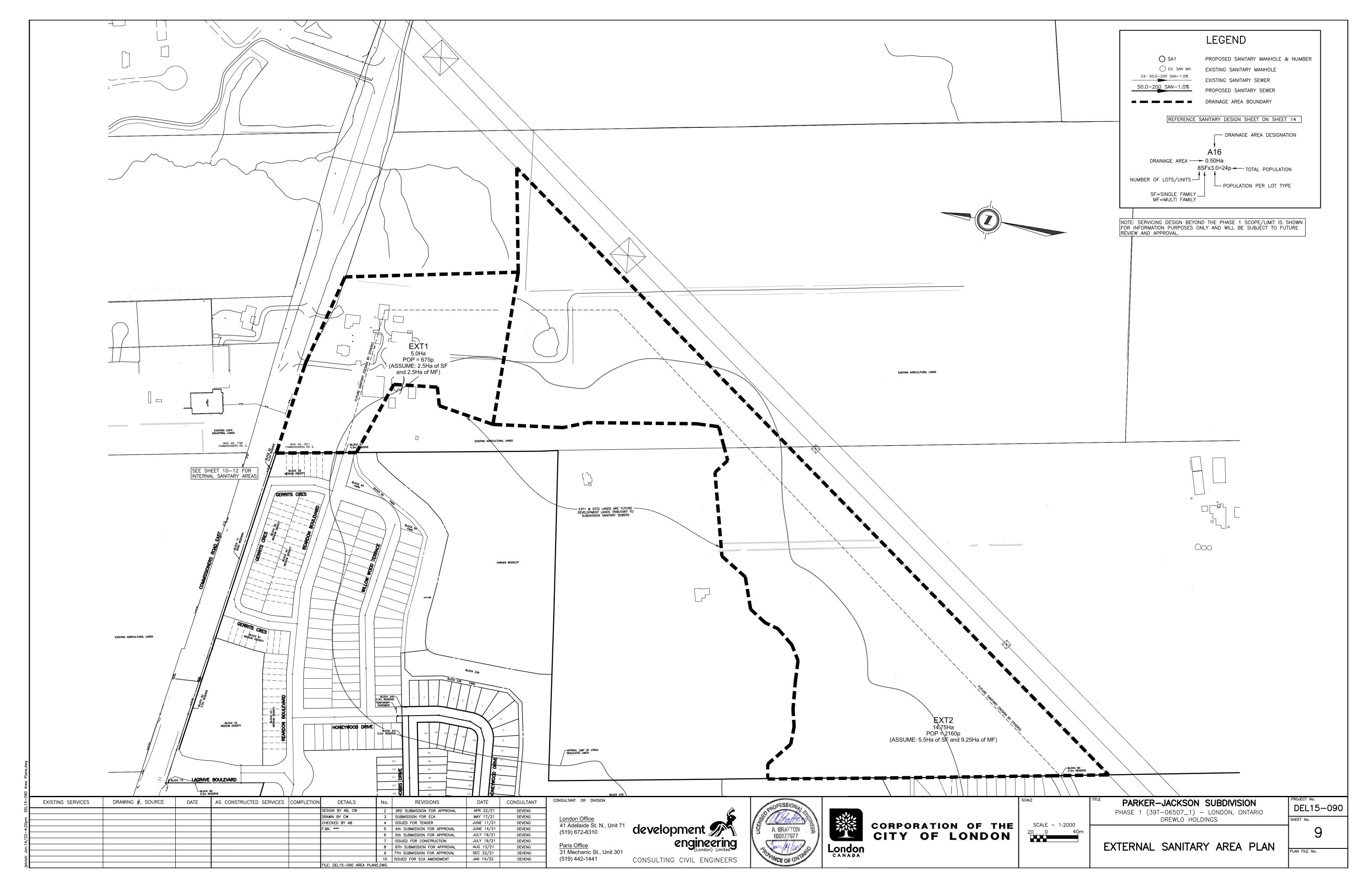


REVISIONS LIST 21 FEB 2023 First Draft

D1 see scale bar 10574/draft plans/D1.dgn

APPENDIX B

External Sanitary Area Plan prepared by Development Engineering
Sanitary Calculation Spreadsheet for Parker Jackson Subdivision by Development Engineering
Watermain modelling excerpts for Parker Jackson Subdivision by Development Engineering
Conceptual Servicing Plan
Conceptual Grading Plan
Figure 1 – Pre Development Storm Tributary Areas
Figure 2 – Post Development Storm Tributary Area Plan
Strom Sewer Design Sheet



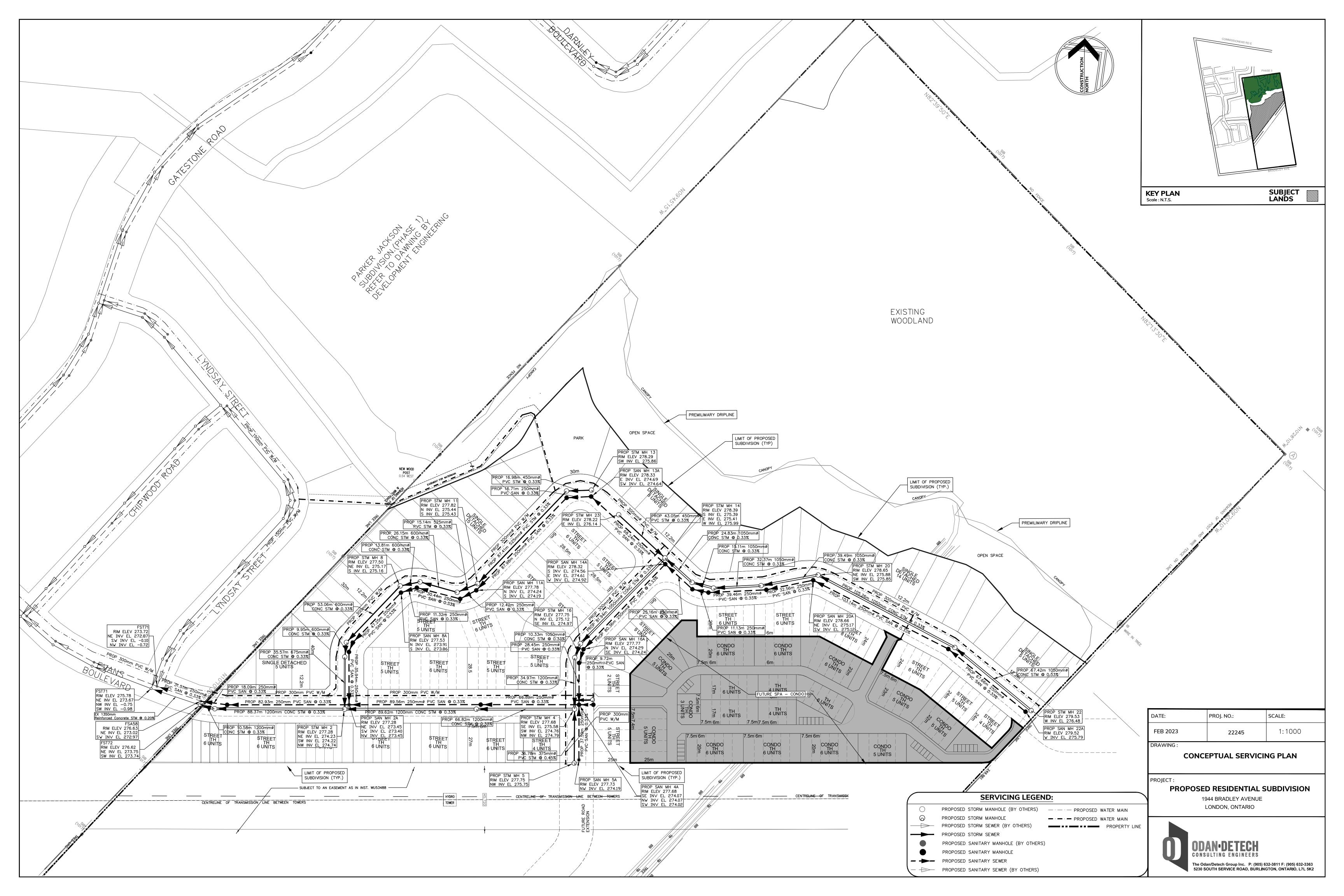


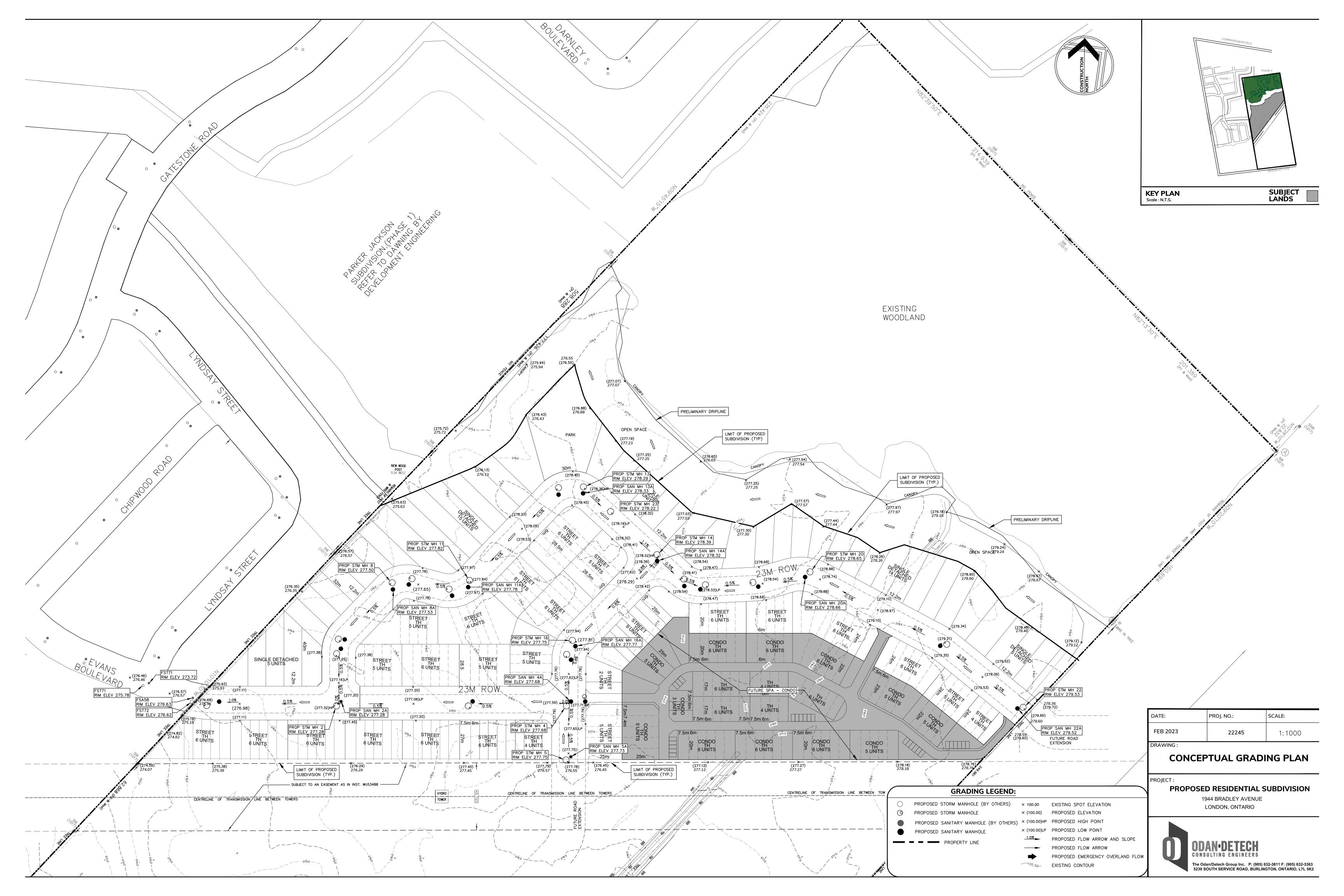
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Max Day + FF - Ultimate

Fire Flow Report - Time: 0.00 hours

| Label | Satisfies Fire Flow | Flow (Total Needed) | Flow (Total Available) | Pressure (Calculated | Pressure (Calculated | Junction w/ | Pipe w/ Maximu | Velocity of |
|-------|------------------------|------------------------|--|-------------------------|-------------------------|----------------|-------------------|----------------|
| | Constraint | (L/s) | (L/s) | Residual) | Zone Lower | Minimum | m | Maximum |
| | s? | | 77 | (kPa) | Limit) | Pressure | Velocity | Pipe |
| | Caspet 15. | | A. A | | (kPa) | (Zone) | | (m/s) |
| H-1 | True | 76.000 | 77.000 | 331.32 | 321.56 | J-47 | P34 | 1.34 |
| H-2 | True | 76.000 | 77.000 | 342.28 | 321.56 | J-47 | P34 | 1.34 |
| H-3 | True | 76.000 | 77.000 | 338.79 | 318.23 | J-47 | P34 | 1.34 |
| H-4 | True | 76.000 | 77.000 | 330.79 | 313.56 | J-47 | P34 | 1.34 |
| H-5 | True | 76.000 | 77.000 | 224.61 | 242.24 | J-47 | P18 | 2.31 |
| H-7 | True | 76.000 | 77.000 | 351.90 | 327.10 | J-47 | P34 | 1.34 |
| H-8 | True | 76.000 | 77.000 | 372.00 | 336.48 | J-24 | P34 | 1.34 |
| H-9 | True | 76.000 | 77.000 | 393.77 | 336.48 | J-24 | P33 | 1.34 |
| H-10 | True | 105.000 | 106.000 | 397.15 | 337,20 | J-24 | P91 | 1.37 |
| H-11 | True | 76.000 | 77.000 | 358.18 | 333.71 | J-24 | P35 | 1.83 |
| H-13 | True | 76.000 | 77.000 | 376.65 | 335.24 | J-24 | P100 | 0.89 |
| H-14 | True | 105.000 | 106.000 | 295.02 | 300.58 | J-37 | P13 | 2.40 |
| H-15 | True | 76.000 | 77.000 | 346.88 | 334.87 | J-24 | P11 | 1.58 |
| H-16 | True | 76.000 | 77.000 | 349.45 | 330.81 | J-24 | P45 | 1.73 |
| H-17 | True | 76.000 | 77.000 | 312.54 | 325.19 | H-19 | P48 | 1.38 |
| H-18 | True | 76.000 | 77.000 | 317.01 | 321.21 | H-19 | P50 | 1.45 |
| H-19 | True | 76.000 | 77.000 | 304.29 | 307.04 | J-24 | P51 | 1.28 |
| H-20 | True | 76.000 | 77.000 | 315.97 | 316.03 | J-22 | P102 | 1.67 |
| H-21 | True | 76.000 | 77.000 | 329.14 | 321.79 | J-21 | P53 | 1.62 |
| H-22 | True | 76.000 | 77.000 | 343.12 | 329.89 | J-21 | P55 | 1.35 |
| H-23 | True | 76.000 | 77.000 | 341.35 | 334.79 | J-24 | P12 | 1.84 |
| H-25 | True | 76.000 | 77.000 | 348.96 | 332.26 | J-21 | P61 | 1.37 |
| H-26 | True | 76.000 | 77.000 | 346.60 | 329.13 | J-21 | P64 | 1.40 |
| H-27 | True | 76.000 | 77.000 | 305.42 | 311.10 | J-12 | P66 | 1.54 |
| H-28 | True | 76.000 | 77.000 | 305.53 | 302.83 | J-12 | P68 | 1.40 |
| H-29 | True | 105.000 | 106.000 | 308.36 | 299.29 | J-12 | P100 | 1.26 |
| H-30 | True | 105.000 | 106.000 | 286.48 | 287.23 | J-11 | P100 | 1.26 |
| H-31 | True | 105.000 | 106.000 | 317.06 | 303.78 | J-12 | P100 | 1.26 |
| H-32 | True | 105.000 | 106.000 | 331.77 | 312.10 | J-12 | P100 | 1.27 |
| H-33 | True | 105.000 | 106.000 | 348.78 | 321.21 | J-12 | P100 | 1.28 |
| H-35 | True | 76.000 | 77.000 | 371.17 | 334.72 | J-22 | P100 | 1.04 |
| H-36 | True | 105.000 | 106.000 | 368.72 | 329.50 | J-21 | P100 | 1.27 |
| H-38 | True | 105,000 | 106.000 | 372.42 | 338.15 | J-22 | P100 | 1.51 |
| H-39 | True | 76.000 | 77.000 | 354.05 | 338.14 | J-22 | P87 | 1,32 |
| H-47 | True | 105.000 | 106.000 | 369.08 | 331.14 | J-21 | P100 | 1.32 |
| H-49 | True | 76.000 | 77.000 | 375.67 | 334.64 | J-21 | P100 | 0.95 |
| H-50 | True | 76.000 | 77.000 | 352.56 | 340.28 | J-22 | P104 | 1.52 |
| H-51 | True | 105.000 | 106.000 | 392.52 | 331.12 | J-24 | P91 | 1.15 |
| H-52 | True | 76.000 | 77.000 | 328.21 | 326.80 | J-31 | P36(1) | 1.48 |
| H-53 | True | 76.000 | 77.000 | 327,24 | 322.64 | J-11 | P3(1) | 1.03 |
| H-54 | True | 76.000 | 77.000 | 319.53 | 322.43 | J-22 | P4(1) | 3.13 |
| H-55 | True | 76.000 | 77.000 | 350.68 | 329.10 | J-47 | P17(2) | 2.13 |
| H-56 | True | 76.000 | 77.000 | 313.95 | 313.35 | J-45 | P17(1) | 1.58 |
| H-57 | True | 76.000 | 77.000 | 271.35 | 273.74 | J-44 | P15(1) | 2 . 35 |









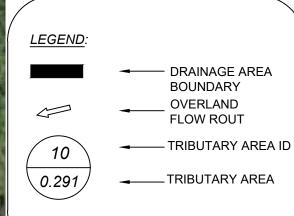


FIGURE 1

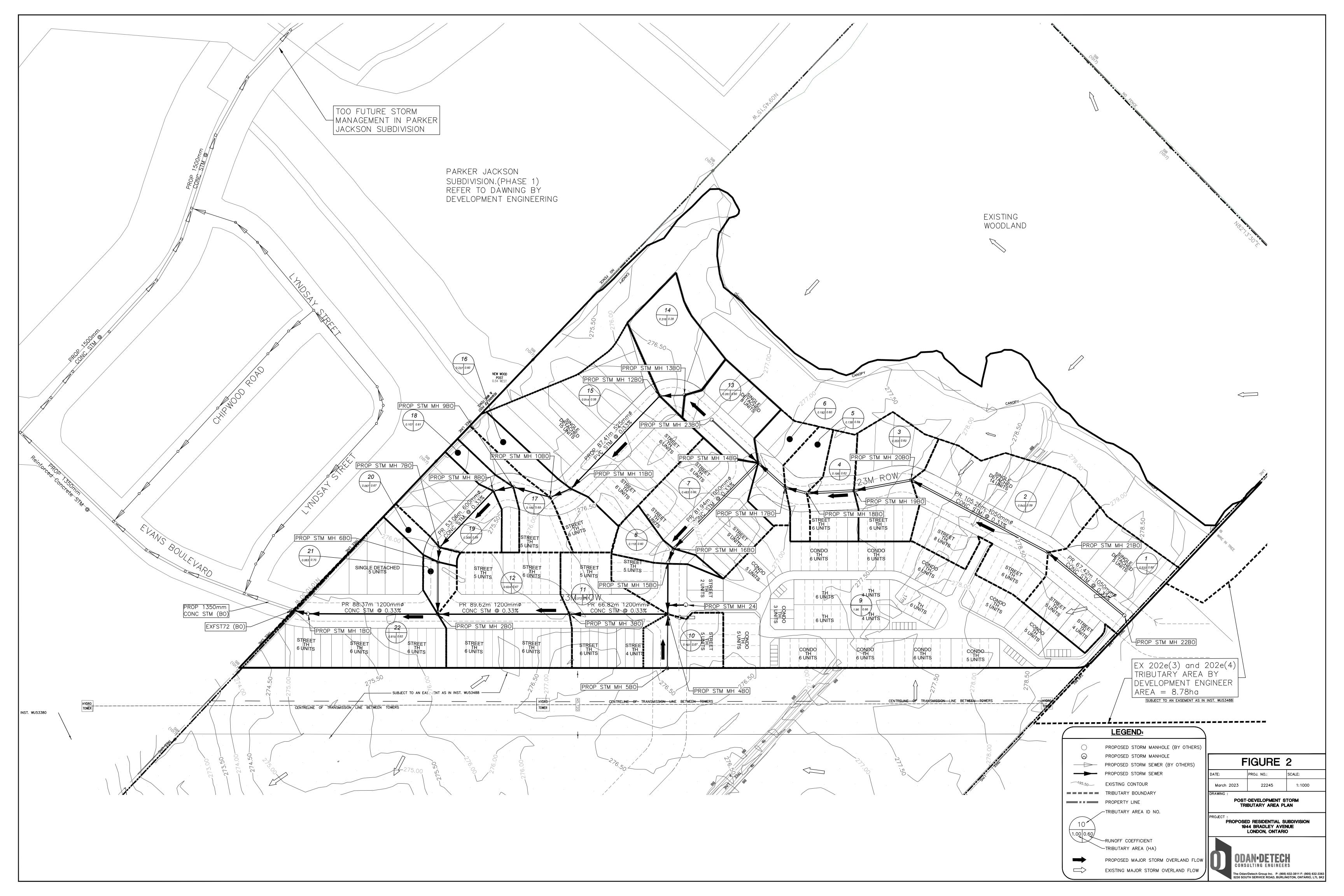
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PRE DEVELOPMENT STORM TRIBUTARY AREAS

PROPOSED RESIDENTIAL SUBDIVISION

1944 BRADLEY AVENUE LONDON, ONTARIO





STORM SEWER DESIGN SHEET

Project No.: 22245

Location: 1944 BRADLEY AVENUE

Project: Proposed Residential Subdivision

DESIGNED BY: M.A.A. DATE: Feb. 24-2023 RAINFALL Return Period 2-years

CHECKED BY

1290/ (Tc+8.5)0.86

PIPE ROUGHNESS: n = 0.013 For Manning's Equation

Vmin = 1.0 m/s

Vmax = 4.5 m/s, for <= 825 mm $V_{max} = 6.0 \text{ m/s for} >= 900 \text{ mm}$

ODAN-DETECH

| Municipality: City of London | | | E | | | | | | | | | | n = 0.013 For Manning's Equation $vmax = 4.5 m/s, fPeak Flow / Full Flow Capacity vmax = 6.0 \text{ m/s}, \text{ f}$ | | | | |
|------------------------------|--------------------------|--|-----------------|-----------------------|-------|-----------------|-----------------------------|-----------------------|----------------------------------|--------------------|-----------------------|-------------------|--|--|--|--|--|
| Municipanty | | idon | | | | | | % 01 Full F | iow: | Peak Flow / | ruii riow C | араспу | | | m/s, for >= | 900 mm | |
| Tributary ID No. | From Manhole | To Manhole | A Area ha | C Runoff Coeff. | A*C | Accumulated A*C | Time of Concentration (min) | Flow Time (min) | Rainfall Intensity (mm/hr) | Peak Flow (l/s) | Pipe Length (m) | Pipe Size (mm) | Pipe Slope (%) | Pipe Full Flow Capacity (I/s) | Pipe Full Flow Velocity (m/s) | Percent of Full Flow Capacity (% | |
| External | | | 8.78 | 0.60 | 5.268 | 5.268 | 20.30 | | 71.70 | 1050 | | 1050 | 0.33 | 1569 | 1.81 | 67 | |
| | | | | | | | | | | | | | | | | | |
| 1 | Pr. MH 22 | | 0.533 | 0.60 | 0.320 | 5.588 | 20.30 | 0.62 | 71.70 | 1114 | 67.42 | 1050 | 0.33 | 1569 | 1.81 | 71 | |
| 2 | the New York Assessed to | Pr. MH 20 | 0.843 | 0.59 | 0.497 | 6.085 | 20.92 | 0.97 | 70.40 | 1191 | 105.26 | 1050 | 0.33 | 1569 | 1.81 | 76 | |
| 3 | THE ROLL SERVICE STREET | Pr. MH 19 | 0.353 | 0.60 | 0.212 | 6.297 | 21.89 | 0.36 | 68.46 | 1198 | 39.49 | 1050 | 0.33 | 1569 | 1.81 | 76 | |
| 4 | | Pr. MH 18 | 0.196 | 0.62 | 0.122 | 6.418 | 22.25 | 0.30 | 67.77 | 1209 | 32.4 | 1050 | 0.33 | 1569 | 1.81 | 77 | |
| 5 | Pr. MH 18 | | 0.138 | 0.59 | 0.081 | 6.500 | 22.55 | 0.14 | 67.21 | 1214 | 15.1 | 1050 | 0.33 | 1569 | 1.81 | 77 | |
| 6 | Pr. MH 17 | Pr. MH 14 | 0.182 | 0.60 | 0.109 | 6.609 | 22.69 | 0.23 | 66.95 | 1230 | 24.8 | 1050 | 0.33 | 1569 | 1.81 | 78 | |
| | | 20 W VIII WOOD | | | | | 22.92 | | | | | | | | | | |
| 13 | Pr. MH 23 | Pr. MH 14 | 0.261 | 0.60 | 0.216 | 0.216 | 10.00 | 0.70 | 104.91 | 63 | 43 | 450 | 0.33 | 164 | 1.03 | 38 | |
| | | | | | | | 10.70 | | | | | | | | | | |
| 7 | D- 141144 | D- 141146 | 0.483 | 0.60 | 0.290 | 7.116 | 22.92 | 0.75 | 66.53 | 1316 | 01.04 | 1050 | 0.22 | 1500 | 1.01 | 0.4 | |
| 8 | Pr. MH 14 | Pr. MH 16 | 0.483 | 0.60 | 0.290 | 7.115 7.186 | 23.67 | 0.75 | 65.19 | 1316 | 81.94 10.33 | 1050 1050 | 0.33 | 1569 1569 | 1.81 | 84 83 | |
| 9 | Pr. MH 15 | | 1.96 | 0.66 | 1.294 | 8.409 | 23.07 | 0.10 | 65.02 | 1520 | 45.3 | 1200 | 0.33 | 2240 | 1.81 | 68 | |
| 9 | Pr. IVIT 15 | Pr. IVIT 4 | 1.90 | 0.00 | 1.294 | 8.409 | 24.15 | 0.38 | 03.02 | 1320 | 43.3 | 1200 | 0.55 | 2240 | 1.98 | 08 | |
| 10 | Pr. MH 5 | Pr. MH 4 | 0.191 | 0.67 | 0.128 | 0.128 | 10.00 | 0.58 | 104.91 | 37 | 36.8 | 375 | 0.45 | 118 | 1.06 | 32 | |
| 10 | PI. IVIN 3 | PI.IVIT 4 | 0.191 | 0.07 | 0.128 | 0.128 | 10.58 | 0.38 | 104.91 | 31 | 30.8 | 3/3 | 0.43 | 118 | 1.00 | 32 | |
| | | | | | | | 10.58 | 1 | | | | | | | | | |
| 11 | Pr. MH 4 | Pr. MH3 | 0.372 | 0.67 | 0.249 | 8.786 | 24.15 | 0.56 | 64.37 | 1572 | 66.82 | 1200 | 0.33 | 2240 | 1.98 | 70 | |
| 12 | Pr. MH3 | Pr. MH2 | 0.624 | 0.67 | 0.418 | 9.204 | 24.71 | 0.75 | 63.43 | 1623 | 89.62 | 1200 | 0.33 | 2240 | 1.98 | 72 | |
| | | | 0.02 | 0.07 | 0.110 | 7.201 | 25.46 | 0.75 | 05.15 | 1023 | 07.02 | 1200 | 0.55 | 2210 | 1.50 | 1-1- | |
| | | | | | | | | | | | | | | | | | |
| 14 | Pr. MH 13 | Pr. MH 12 | 0.316 | 0.28 | 0.088 | 0.088 | 10.00 | 0.28 | 104.91 | 26 | 17 | 450 | 0.33 | 164 | 1.03 | 16 | |
| 15 | Pr. MH 12 | CONTROL OF THE PARTY OF THE PAR | 0.914 | 0.58 | 0.530 | 0.619 | 10.28 | 1.28 | 103.59 | 178 | 87.4 | 525 | 0.33 | 247 | 1.14 | 72 | |
| 16 | Pr. MH 11 | | 0.237 | 0.60 | 0.142 | 0.761 | 11.55 | 0.22 | 97.89 | 207 | 15.14 | 525 | 0.33 | 247 | 1.14 | 84 | |
| 17 | Pr. MH 10 | | 0.189 | 0.63 | 0.119 | 0.880 | 11.77 | 0.35 | 96.97 | 237 | 26.15 | 600 | 0.33 | 353 | 1.25 | 67 | |
| 18 | Pr. MH 9 | Pr. MH8 | 0.107 | 0.61 | 0.065 | 0.945 | 12.12 | 0.18 | 95.56 | 251 | 13.8 | 600 | 0.33 | 353 | 1.25 | 71 | |
| 19 | Pr. MH8 | Pr. MH7 | 0.308 | 0.59 | 0.182 | 1.127 | 12.31 | 0.71 | 94.83 | 297 | 53 | 600 | 0.33 | 353 | 1.25 | 84 | |
| 20 | Pr. MH7 | Pr. MH6 | 0.067 | 0.67 | 0.045 | 1.172 | 13.01 | 0.13 | 92.14 | 300 | 10 | 600 | 0.33 | 353 | 1.25 | 85 | |
| 21 | Pr. MH6 | Pr. MH2 | 0.063 | 0.70 | 0.044 | 1.216 | 13.15 | 0.44 | 91.65 | 310 | 35.6 | 675 | 0.33 | 483 | 1.35 | 64 | |
| | | | | | | | 13.59 | | | | | | | | | | |
| 22 | Pr. MH2 | FST 72 | 0.815 | 0.62 | 0.505 | 10.925 | 25.46 | 0.83 | 62.22 | 1890 | 99 | 1200 | 0.33 | 2240 | 1.98 | 84 | |